

A New Meshless Interpolation Scheme for MLPG_R Method

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Abstract: In the MLPG_R (Meshless Local Petrove-Galerkin based on Rankine source solution) method, one needs a meshless interpolation scheme for an unknown function to discretise the governing equation. The MLS (moving least square) method has been used for this purpose so far. The MLS method requires inverse of matrix or solution of a linear algebraic system and so is quite time-consuming. In this paper, a new scheme, called simplified finite difference interpolation (SFDI), is devised. This scheme is generally as accurate as the MLS method but does not need matrix inverse and consume less CPU time to evaluate. Although this scheme is purposely developed for the MLPG_R method, it may also be used for other meshless methods.

Keyword: Simplified finite difference interpolation (SFDI), MLPG, MLPG_R, nonlinear water waves.

1 Introduction

A meshless method, called Meshless Local Petrove-Galerkin (MLPG) method, has been invented by Atluri and Zhu (1998) and Atluri and Shen (2002) and has been developed into many forms as summarised in Atluri, Liu and Han (2006). This method is based on a local weak form over local sub-domains (circles for two dimensional problems and spheres for three dimensional ones). The success of the MLPG method has been reported in solving fracture mechanics problems [Batra and Ching (2002)], beam and plate bending problems [Atluri and Zhu (2000)], three dimensional elasto-static and -dynamic problems [Han and Atluri (2004a,b)]

and some fluid dynamic problems, such as steady flow around a cylinder [Atluri and Zhu (1998)], steady convection and diffusion flow [Lin and Atluri (2000)] in one and two dimensions and lid-driven cavity flow in a two dimensional box [Lin and Atluri (2001)].

In Ma (2005a), the MLPG method was extended to simulating nonlinear water waves and produced some encouraging results. In that paper, the simple Heaviside step function was adopted as the test function to formulate the weak form over local sub-domains, resulting in one in terms of pressure gradient.

In Ma (2005b), the MLPG method was developed into a new form called the MLPG_R method, suitable for modelling nonlinear water waves. In the MLPG_R method, the solution for Rankine sources rather than the Heaviside step function was taken as the test function. Based on this test function, a weak form of governing equations was derived, which did not contain the gradients of unknown functions, therefore made numerical discretisation of the governing equation relatively easier and more efficient. A semi-analytical technique was also developed to evaluate the domain integral involved in this method, which dramatically reduce the CPU time spent on the numerical evaluation of the integral. Numerical tests showed that the MLPG_R method could be twice as fast as the MLPG method for modelling nonlinear water wave problems.

In the MLPG_R method, the water wave problems are solved using a time-step marching procedure. This starts from a particular instant when the velocity and the geometry of fluid flow are known and then evolves to next time step, at which all physical quantities are updated by solving the governing equations. During each time step, the problem is formulated using a well-

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known time-split procedure, in which the velocities of particles are updated by

$$\vec{u}^{(n+1)} = \vec{u}^{(*)} - \frac{\Delta t}{\rho} \nabla p^{(n+1)} \quad (1)$$

where $\vec{u}^{(n+1)}$ is the velocity at time t_{n+1} , $\vec{u}^{(*)}$ is the intermediate velocity evaluated by the velocity and external forces in previous time step and $p^{(n+1)}$ is the pressure at time t_{n+1} . The pressure is found by solving

$$\frac{1}{2\pi\alpha R_I^\alpha} \int_{\partial\Omega_I} p dS - p_I = G(\vec{u}^{(*)}) \quad (2a)$$

where R_I is the radius of integration domain Ω_I , $\alpha=1$ for 2D cases, $\alpha=2$ for 3D cases and $G(\vec{u}^{(*)})$ is defined as

$$G(\vec{u}^{(*)}) = \begin{cases} \frac{\rho}{2\pi\Delta t} \int_0^{R_I} \int_0^{2\pi} u_r^{(*)}(r, \theta) dr d\theta & \text{for 2D cases} \\ \frac{\rho}{2\pi\alpha\Delta t} \int_0^{R_I} \int_0^{2\pi} \int_0^\pi u_r^{(*)} \sin\theta dr d\theta d\beta & \text{for 3D cases} \end{cases} \quad (2b)$$

where $u_r^{(*)}$ is the radial component of the intermediate velocity $\vec{u}^{(*)}$.

In order to discretise Eq. (2) and to evolve the velocity in Eq. (1), one needs a meshless interpolation scheme for evaluating the pressure and its gradient in terms of discrete values of pressure at nodes. Computational costs spent on them are considerable. Reducing these costs can make the method more efficient. The main contribution of this paper is to develop a new meshless interpolation scheme, requiring less computational efforts, and thus to further enhance the overall efficiency of the MLPG_R method.

2 Brief review on meshless interpolation schemes for MLPG methods

Various available meshless interpolation schemes have been reviewed by Atluri and Shen (2002) and also by Atluri (2005). They include the Shepard function (SF), the partition of unity (PU), the reproducing kernel particle interpolation

(RKPM), radial basis function (RBF) and moving least square (MLS) methods. The simplest one among them is the SF method, which is the same as the interpolation of an unknown function used in a moving particle semi-implicit method (MPS) and can suffer a problem of large errors as discussed below. The PU method is more computational expensive and so is not good choice for the family of MLPG methods. The RKPM is equivalent to the MLS method if the basis and weight functions used in them are the same. Atluri and Shen (2002) carried out numerical investigations and demonstrated that the RBFs was not as accurate as the MLS method for the same number of nodes or needed more nodes to achieve the same accuracy. Therefore, the MLS method is more popular than other interpolation schemes for the MLPG methods. It is also the reason why it was utilised by the author in Ma (2005a and 2005b).

For the sake of completeness and convenience of discussions below, the MLS method is outlined here. To be more general, the unknown function is represented by $f(\vec{r})$ with \vec{r} denoting the position vector of a point, which may also be the pressure (p) in the MLPG_R method. With the MLS method, the unknown function $f(\vec{r})$ can be written as

$$f(\vec{r}) \approx \sum_{J=1}^N \Phi_J(\vec{r}) \hat{f}_J \quad (3a)$$

where N is the number of nodes that affect the function at point \vec{r} ; \hat{f}_J are nodal variables but not necessarily equal to the nodal values of $f(\vec{r})$. In the equation, $\Phi_J(\vec{r})$ is called the interpolation or shape function and is given as

$$\begin{aligned} \Phi_J(\vec{r}) &= \sum_{l=1}^m \psi_l(\vec{r}) [\mathbf{A}^{-1}(\vec{r}) \mathbf{B}(\vec{r})]_{lJ} \\ &= \boldsymbol{\psi}^T(\vec{r}) \mathbf{A}^{-1}(\vec{r}) \mathbf{B}_J(\vec{r}) \end{aligned} \quad (3b)$$

with the basis function, assuming to be linear, being

$$\boldsymbol{\psi}^T(\vec{r}) = [\psi_1, \psi_2, \psi_3] = [1, x, y] \quad (m=3) \text{ for 2D cases}$$

and

$$\boldsymbol{\psi}^T(\vec{r}) = [\psi_1, \psi_2, \psi_3, \psi_4] = [1, x, y, z] \quad (m=4) \text{ for 3D cases;}$$

and with the matrixes $\mathbf{B}(\bar{x})$ and $\mathbf{A}(\bar{x})$ being defined as

$$\begin{aligned} \mathbf{B}(\vec{r}) &= \Psi^T \mathbf{W}(\vec{r}) \\ &= [w_1(\vec{r} - \vec{r}_1) \Psi(\vec{r}_1), w_2(\vec{r} - \vec{r}_2) \Psi(\vec{r}_2), \dots] \end{aligned} \quad (3c)$$

and

$$\mathbf{A}(\vec{r}) = \Psi^T \mathbf{W}(\vec{r}) \Psi = \mathbf{B}(\vec{r}) \Psi,$$

where $\mathbf{W}(\vec{r})$ and Ψ are, respectively, expressed by

$$\mathbf{W}(\vec{r} - \vec{r}_J) = \begin{bmatrix} w(|\vec{r} - \vec{r}_J|) & 0 & \dots & 0 \\ 0 & & & \\ \dots & & & \\ 0 & & & w(|\vec{r} - \vec{r}_J|) \end{bmatrix} \quad (3d)$$

and

$$\Psi^T = [\Psi(\vec{r}_1), \Psi(\vec{r}_2), \dots, \Psi(\vec{r}_N)], \quad (3e)$$

which shows each column of the matrix Ψ^T is the value of the basis function Ψ at a particular point. $w(|\vec{r} - \vec{r}_J|)$ in Eq. (3d) is a weight function. Its specific form will be given later. The gradient of the unknown function is estimated by

$$\nabla f(\vec{r}) \approx \sum_{J=1}^N \nabla \Phi_J(\vec{r}) \hat{f}_J \quad (3f)$$

The partial derivatives (or the gradient) of the shape function with respect to y are found by directly differentiating Eq. (3b), that is,

$$\Phi_{J,y} = \Psi_{,y}^T \mathbf{A}^{-1} \mathbf{B}_J + \Psi^T \mathbf{A}_{,y}^{-1} \mathbf{B}_J + \Psi^T \mathbf{A}^{-1} \mathbf{B}_{J,y} \quad (3g)$$

where $\mathbf{A}_{,y}^{-1}$ is the partial derivative of \mathbf{A}^{-1} (the inverse of $\mathbf{A}(\vec{r})$), with respect to y (x or z) and is evaluated by $\mathbf{A}_{,y}^{-1} = -\mathbf{A}^{-1} \mathbf{A}_{,y} \mathbf{A}^{-1}$ and \mathbf{B}_J is J -th column of Matrix \mathbf{B} whose partial derivative is estimated by

$$\mathbf{B}_{J,y} = \frac{\partial w_J(\vec{r} - \vec{r}_J)}{\partial y} \Psi(\vec{r}_J).$$

The interpolations given by Eqs. (3a) and (3f) are accurate for a linear function independent on the node distribution. This is a good feature particularly for the problems, such as about non-linear water waves, involving large deformation

of computational domain. Nevertheless, they do have some drawbacks. (1) The interpolation function will not be well defined if the number of nodes (N) affecting the concerned point is not large enough. This implies that it may not always work properly when modelling the problems associated with fragment phenomena, such as breaking waves. Although this may be overcome by enlarging the support domain, the larger support domain may lead to over-smoothing and so degrade the accuracy. (2) Interpolation of the function in Eq. (3a) needs the inverse of matrix \mathbf{A} , which is the order of $m \times m$. Although m may be only 3 for 2D case and only 4 for 3D cases, the computational cost spent on it is not negligible due to the fact that the number of points at which the function $f(\vec{r})$ needs to be estimated is much larger (at least 8 times for 2D and 16 times for 3D) than the total number of nodes when discretising Eq. (2a) and that the computational cost for the inverse of the matrix is proportional to m^3 . (3) The evaluation of the gradient by direct differentiation as shown in Eqs. (3f) and (3g) is even more expensive due not only to the inverse of matrix but also to the successive multiplication of several matrixes. To avoid the direct differentiation on the interpolation function, Prof. Atluri and his research group suggested a mixed approach in their several recent publications. In particular, Atluri, Liu and Han (2006) describe the following new formulation. The unknown function is still evaluated using Eq. (3a) but its gradient is estimated by a finite difference method. In this method, the components of the gradient are determined by minimising the norm of the unknown function with respect to the gradient components (similar to a least square method) and are expressed (different symbols used in this paper to avoid some confusion with other equations) as

$$f_{,y}^I(\vec{r}_I) = \sum_{J=1}^N H_y^J f(\vec{r}_I + \zeta \Delta \vec{r}_{IJ}) - \bar{H}_y f(\vec{r}_I) \quad (4)$$

$$\bar{H}_y = \sum_{J=1}^N H_y^J$$

where $f_{,y}^I(\vec{r}_I)$ is the y -component (y can be changed into x or z to give other components) of the gradient of $f(\vec{r})$ at Node I , $\mathbf{H} =$

$(\mathbf{h}^T \mathbf{W} \mathbf{h})^{-1} \mathbf{h}^T \mathbf{W}$, $\mathbf{h}^T = \zeta [\Delta \vec{r}_{I1}, \Delta \vec{r}_{I2}, \Delta \vec{r}_{I3}, \dots, \Delta \vec{r}_{IN}]$, $\Delta \vec{r}_{IJ} = \vec{r}_J - \vec{r}_I$, \mathbf{W} is the same matrix as in Eq. (3d) and ζ is a shrink factor, controlling the position of sample points that are not necessarily the nodes. If the shrink factor is not equal 1, the value of $f(\vec{r}_I + \zeta \Delta \vec{r}_{IJ})$ must be found by Eq. (3a) before estimating the gradient.

Another relevant meshless interpolation is the one used in the moving particle semi-implicit method (MPS) developed by Koshizuka and Oka (1996) and adopted by others [e.g. Koshizuka, Ikeda and Oka, (1999), Heo, Koshizuka and Oka, (2002)]. In the MPS method, a function and its gradient are modelled by

$$f(\vec{r}_0) = \frac{\sum_J f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J w(|\vec{r}_J - \vec{r}_0|)} \quad (5a)$$

$$(f_{,y})_{\vec{r}_0} = \frac{d}{\sum_J w(|\vec{r}_J - \vec{r}_0|)} \sum_J [f(\vec{r}_J) - f(\vec{r}_0)] \cdot \frac{(\vec{r}_{J,y} - \vec{r}_{0,y})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|) \quad (5b)$$

where J represents the neighbour nodes of Point \vec{r}_0 , $w(|\vec{r}_J - \vec{r}_0|)$ is a weight function as mentioned above, $f_{,y}$ is the partial derivative with respect to y (changeable to x or z), $\vec{r}_{J,y}$ is the component of the position vector in y (x or z) direction and d is a number of spatial dimensions, equal to 2 in 2D cases and 3 in 3D cases. Although these expressions are very easy to evaluate, they are only rough approximations. This can be seen by the following fact. Eq. (5a) is accurate for any distribution of nodes only if the function is a constant or accurate for a linear function only when the nodes are symmetrical about Point \vec{r}_0 . The condition of symmetry is not met even if all nodes are located at intersection points of a rectangular grid unless Point \vec{r}_0 is also a node, not arbitrary. Eq. (5b) is even worse. In order to give accurate value of the gradient for a linear function, it does not only require that the point (\vec{r}_0) must be a node and all nodes lie on intersection points of rectangular grid but also require that the grid must be square. To remove the restriction to the square

grid, Yoon, Koshizuka and Oka (2001) suggested another expression for the gradient, i.e.

$$(f_{,y})_{\vec{r}_0} = \frac{1}{n_{0,y}} \sum_J [f(\vec{r}_J) - f(\vec{r}_0)] \frac{(\vec{r}_{J,y} - \vec{r}_{0,y})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|) \quad (5c)$$

where

$$n_{0,y} = \sum_J \frac{(\vec{r}_{J,y} - \vec{r}_{0,y})^2}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|).$$

Similarly, this one is not accurate either for a linear function unless Point \vec{r}_0 and all the nodes lie on the intersection points of a rectangular (not necessarily being square) grid. Nevertheless, if the linear function is one dimensional, Eq. (5c) does not depend on the nodes distribution to give accurate results but this feature is rarely useful because problems we consider are generally two or three directional. If Eq. (5b) or (5c) is used to evolve the velocity in Eq. (1) for an irregular distribution of nodes, large errors may be caused.

Based on the discussions above, it could be seen that interpolations used in the MPS method are not as good as the corresponding expressions in the MLS formulation in terms of accuracy. The problems with Eq. (5a) and Eq. (5b) or (5c) may become severe if they are used to model the violent water waves, in which it is impossible to keep all the nodes at the intersection points of rectangular grids. If they are really used in such cases, much more number of nodes must be required to achieve the same accuracy, compared with the MLS formulation. However, they are cheaper to compute than those in the MLS scheme mainly because matrix inverse is not involved.

3 Simplified finite difference interpolation (SFDI) scheme

In this section, a new scheme for interpolating an unknown function will be developed, which is in the same order of accuracy as Eq. (3a) in the MLS using a linear basis function but does not need inverse of matrix and so needs less CPU time to evaluate. This scheme will be particularly useful

for the MLPG_R method, in which the values of unknown pressure have to be evaluated at a large number of points when discretising Eq. (2a), as indicated above.

To achieve this, a general function $f(\vec{r})$ is expanded into a Taylor series near Point \vec{r}_0 :

$$f(\vec{r}) = f(\vec{r}_0) + (\nabla f)_{\vec{r}_0} \cdot (\vec{r} - \vec{r}_0) + O(|\vec{r} - \vec{r}_0|^2) \quad (6)$$

Applying the above expression to a set of nodes (J) around \vec{r}_0 , multiplying a weight function $w(|\vec{r}_J - \vec{r}_0|)$ on both sides and taking the sum of equations at all relevant nodes yields:

$$\begin{aligned} & \sum_J^N f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|) \\ &= \sum_J^N f(\vec{r}_0) w(|\vec{r}_J - \vec{r}_0|) \\ &+ (\nabla f)_{\vec{r}_0} \cdot \sum_J^N (\vec{r}_J - \vec{r}_0) w(|\vec{r}_J - \vec{r}_0|) \\ &+ O\left(\sum_J^N |\vec{r}_J - \vec{r}_0|^2 w(|\vec{r}_J - \vec{r}_0|)\right) \end{aligned} \quad (7)$$

where N is the total number of nodes and $(\nabla f)_{\vec{r}_0}$ is the gradient of $f(\vec{r})$ at Point \vec{r}_0 . This gives

$$\begin{aligned} f(\vec{r}_0) &= \frac{\sum_J^N f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)} \\ &- (\nabla f)_{\vec{r}_0} \cdot \frac{\sum_J^N (\vec{r}_J - \vec{r}_0) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)} \\ &- O\left(\frac{\sum_J^N |\vec{r}_J - \vec{r}_0|^2 w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)}\right). \end{aligned} \quad (8)$$

Defining

$$\vec{R}_0 = \frac{\sum_J^N (\vec{r}_J - \vec{r}_0) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)}$$

and

$$\varepsilon_{\vec{r}_0} = O\left(\frac{\sum_J^N |\vec{r}_J - \vec{r}_0|^2 w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)}\right),$$

one can write the above equation as

$$f(\vec{r}_0) = \frac{\sum_J^N f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)} - (\nabla f)_{\vec{r}_0} \cdot \vec{R}_0 - \varepsilon_{\vec{r}_0} \quad (9)$$

Omitting the error term ($\varepsilon_{\vec{r}_0}$), the value of the function at Point \vec{r}_0 is approximated by

$$f(\vec{r}_0) \approx \frac{\sum_J^N f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)} - (\nabla f)_{\vec{r}_0} \cdot \vec{R}_0 \quad (10)$$

It is obvious that the error of the approximation is

$$\varepsilon_{\vec{r}_0} < O(\max(|\vec{r}_J - \vec{r}_0|^2)).$$

In other words, if $f(\vec{r})$ is a linear function and $(\nabla f)_{\vec{r}_0}$ is its accurate gradient, the expression for $f(\vec{r}_0)$ is accurate. On the other hand, if $f(\vec{r})$ is a general function, the expression has a second order of accuracy. This is similar to the approximation of the MLS using a linear basis. Nevertheless, the gradient $(\nabla f)_{\vec{r}_0}$ is generally unknown. Although we may derive another set of equations for $(\nabla f)_{\vec{r}_0}$ and solve them together with Eq. (10) as in Liszka, Duarte and Tworzydlo (1996), it conflicts with our purpose to derive a shape function that does not require matrix inverse or solution of linear algebraic equations. To circumvent the difficulty, it is suggested that $(\nabla f)_{\vec{r}_0}$ is replaced by $(\nabla f)_{\vec{r}_I}$, where \vec{r}_I is one of nodes among \vec{r}_J ($J = 1, 2, \dots$), that is,

$$f(\vec{r}_0) \approx \frac{\sum_J^N f(\vec{r}_J) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)} - (\nabla f)_{\vec{r}_I} \cdot \vec{R}_0 \quad (11)$$

The alternation to the gradient in the above equation is a key point of the new scheme. Because of this, it is called as ‘simplified’ finite difference interpolation (SFDI). It is noted that this alternation does not affect the accuracy of the expression if $f(\vec{r}_0)$ is a linear function because $(\nabla f)_{\vec{r}_0} = (\nabla f)_{\vec{r}_I}$ for such a function. In other words, it does not affect the order of accuracy for a general function.

It is also noted that \vec{r}_I may be the nearest node to Point \vec{r}_0 but not necessary. Of course, the gradient $(\nabla f)_{\vec{r}_I}$ must be evaluated to obtain the final form of the shape function. There are variety ways to do so. For example, the method described in the next section may be used but it again needs the solution of a linear algebraic system. In this paper we choose to estimate it by using Eq. (5d), i.e., the components of $(\nabla f)_{\vec{r}_I}$ is approximated by

$$(f_y)_{\vec{r}_I} = \frac{1}{n_{I,y}} \sum_{J \neq I}^N [f(\vec{r}_J) - f(\vec{r}_I)] \frac{(\vec{r}_{J,y} - \vec{r}_{I,y})}{|\vec{r}_J - \vec{r}_I|^2} w(|\vec{r}_J - \vec{r}_I|) \quad (12)$$

where

$$n_{I,y} = \sum_{J \neq I}^N \frac{(\vec{r}_{J,y} - \vec{r}_{I,y})^2}{|\vec{r}_J - \vec{r}_I|^2} w(|\vec{r}_J - \vec{r}_I|)$$

with y changed into x or z to give other components of the gradient. As already noted for Eq. (5), the gradient expressed by Eq. (12) is not accurate to the order of $O(\max(|\vec{r}_J - \vec{r}_0|^2))$ unless all the nodes are uniformly distributed around Point \vec{r}_0 and thus may not be used for estimating the velocity directly. However, in Eq. (11), the term $(\nabla f)_{\vec{r}_I} \cdot \vec{R}_0$ has higher order than the first term and so the error in the estimation of $(\nabla f)_{\vec{r}_I}$ may not significantly degrade the accuracy of $f(\vec{r}_0)$. This will be confirmed by the numerical tests in later sections. Substituting Eq. (12) into (11), it follows that

$$f(\vec{r}_0) = \sum_{J=1}^N \Phi_J(\vec{r}_0; \vec{r}_I) f(\vec{r}_J) \quad (13)$$

where $\Phi_J(\vec{r}_0; \vec{r}_I)$ is the shape function in the SFDI interpolation and is defined by

$$\Phi_J(\vec{r}_0; \vec{r}_I) = \frac{w(|\vec{r}_J - \vec{r}_0|)}{\sum_J w(|\vec{r}_J - \vec{r}_0|)} - (1 - \delta_{IJ}) B_{0,J}(\vec{r}_I) + \delta_{IJ} \sum_{J \neq I}^N B_{0,J}(\vec{r}_I)$$

Where

$$\delta_{IJ} = \begin{cases} 1 & I = J \\ 0 & I \neq J \end{cases}$$

$$B_{0,J}(\vec{r}_I) = \frac{w(|\vec{r}_J - \vec{r}_I|)}{|\vec{r}_J - \vec{r}_I|^2} \sum_{k=1}^d \frac{\vec{R}_{0,x_k}}{n_{I,x_k}} (\vec{r}_{J,x_k} - \vec{r}_{I,x_k}),$$

and

$$\vec{R}_{0,x_k} = \frac{\sum_J^N (\vec{r}_{J,x_k} - \vec{r}_{0,x_k}) w(|\vec{r}_J - \vec{r}_0|)}{\sum_J^N w(|\vec{r}_J - \vec{r}_0|)},$$

where d is still the number of spatial dimensions as defined above and x_k for $k=1, 2$ and 3 is x, y and z , respectively. It may be noted that the methodology to formulate the above interpolation function is some what similar to that for formulating the consistent SPH approximation [Chen and Beraun (2000)]. However there are three differences. (1) Eq. (6) is integrated over a domain in SPH approximation rather than taken as the weighted sum. (2) The integration must be performed on a mesh while Eq. (7) is based only on the weight function. (3) Therefore, the consistent SPH approximation relies on a background mesh. Comparatively, Eq. (13) is a truly meshless expression. (4) The consistent SPH approximation for a function did not have the second term, i.e., similar to the form used in the MPS method.

4 Gradient interpolation

As pointed out before, the velocity evolvment of particles in Eq. (1) for the MLPG_R method requires the evaluation of pressure gradient. In this section, the interpolation for the gradient is developed by using the similar method to the above in order to replace Eq. (3f) with the new one eliminating the necessity of multiplications of several matrixes. For this purpose, Eq. (6) is rewritten as

$$f(\vec{r}_J) - f(\vec{r}_0) = (\nabla f)_{\vec{r}_0} \cdot (\vec{r}_J - \vec{r}_0) + O(|\vec{r}_J - \vec{r}_0|^2)$$

Multiplying $\frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|)$ on both sides, taking the sum of equations at all the relevant

nodes and ignoring the error term, it follows that

$$\begin{aligned} & \sum_J^N [f(\vec{r}_J) - f(\vec{r}_0)] \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|) \\ &= \sum_J^N \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})^2}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|) (f_{,x_m})_{\vec{r}_0} \\ &+ \sum_J^N \sum_{k=1, k \neq m}^d (\vec{r}_{J,x_k} - \vec{r}_{0,k}) (f_{,x_k})_{\vec{r}_0} \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})}{|\vec{r}_J - \vec{r}_0|^2} \\ &\quad \cdot w(|\vec{r}_J - \vec{r}_0|) \end{aligned}$$

Alternatively, we have

$$(f_{,x_m})_{\vec{r}_0} + \sum_{k=1, k \neq m}^d a_{0,mk} (f_{,x_k})_{\vec{r}_0} = C_{0,m} \quad (m = 1, 2, \dots, d) \quad (14)$$

where

$$C_{0,m} = \frac{1}{n_{0,x_m}} \sum_J^N [f(\vec{r}_J) - f(\vec{r}_0)] \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|)$$

and

$$a_{0,mk} = \frac{1}{n_{0,x_m}} \sum_J^N \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})(\vec{r}_{J,x_k} - \vec{r}_{0,x_k})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|).$$

Solving the system in Eq. (14), one can find the gradient components. For example, in 2D cases, they are

$$(f_{,x})_{\vec{r}_0} = \frac{C_{0,1} - a_{0,12}C_{0,2}}{1 - a_{0,12}a_{0,21}}$$

and

$$(f_{,y})_{\vec{r}_0} = \frac{C_{0,2} - a_{0,21}C_{0,1}}{1 - a_{0,12}a_{0,21}}.$$

In 3D cases, Eq. (14) can be generally written as

$$[A]\{F\} = [C]\{\delta F\}$$

where

$$\{F\} = \left[(f_{,x})_{\vec{r}_0}, (f_{,y})_{\vec{r}_0}, (f_{,z})_{\vec{r}_0} \right]^T,$$

$$\{\delta f\} = [f(\vec{r}_1) - f(\vec{r}_0), f(\vec{r}_2) - f(\vec{r}_0), \dots, f(\vec{r}_J) - f(\vec{r}_0), \dots]^T,$$

[C] is an $3 \times N$ matrix with its components defined as

$$C_{mJ} = \frac{1}{n_{0,x_m}} \frac{(\vec{r}_{J,x_m} - \vec{r}_{0,x_m})}{|\vec{r}_J - \vec{r}_0|^2} w(|\vec{r}_J - \vec{r}_0|),$$

[A] is an 3×3 matrix with its entries given by

$$A_{mk} = a_{0,mk} \quad (m \neq k) \text{ and } A_{mm} = 1.$$

At last, the gradient components may be written as

$$(f_{,x_m})_{\vec{r}_0} = \sum_{J=1}^N \tilde{\Gamma}_{mJ}(\vec{r}_0) [f(\vec{r}_J) - f(\vec{r}_0)] \quad (15)$$

with

$$\tilde{\Gamma}_{mJ}(\vec{r}_0) = \sum_{k=1}^d \tilde{A}_{mk} C_{kJ} \quad J = 1, 2, 3 \dots, \quad (16)$$

where $[\tilde{A}]$ is the inverse matrix of [A], i.e. $[\tilde{A}] = [A]^{-1}$. $\tilde{\Gamma}_{mJ}(\vec{r}_0)$ is the shape function for gradient components. Compared with Eqs. (3f) and (3g) in the MLS method, the expressions in Eq. (15) needs to solve a smaller number of equations, to evaluate the multiplication of a smaller number of matrixes, and therefore require less CPU time, making the method more efficient particularly in 3D cases.

It is easy to deduce that if $f(\vec{r})$ is linear Eq. (15) gives exact value of gradient components, independent of the distribution of nodes. This equation may be used in Eq. (11) to formulate the shape function for the interpolation of the unknown function with sacrifice to CPU time and with slight improvement to the accuracy. Another point is worthy to be pointed out is that Eq. (15) become equivalent to Eq. (4) if the shrink factor is taken as 1. Therefore the same expression of the gradient is obtained by using two different methods. In addition, for some special cases, such as all neighbour nodes lying on a special line in 2D cases or in a special plane in 3D cases, $[A]^{-1}$ may not exist. This difficulty may be overcome simply by making $a_{0,mk} = 0$ (the SFDI is reduced

to Eq. (5c)) for the node concerned. It should be noted that this difficulty is not only with the SFDI method but also with schemes such as Eq. (4) or the MLS method. The real reason is that for such a special distribution of neighbour nodes, one actually attempts to model the gradient in a low-dimensional space (e.g. 2D) using a function defined in a high-dimensional space (e.g. 3D).

5 Convergent rate

In this section, investigations will be made into the convergent rate of the new shape functions in Eqs. (13) and (15) by comparing with their counterparts in other two methods through numerical tests on assumed functions. Although they can be used for any problem, the numerical tests will be carried out on 2D problems.

The computational domain for the tests is chosen as a square with the length of sides being 1. The nodes, at which the nodal values $f(\vec{r}_J)$ are defined, are irregularly distributed by using quasi-random number [see for example, Faure, H. (1990)]. A typical node distribution is illustrated in Fig 1.

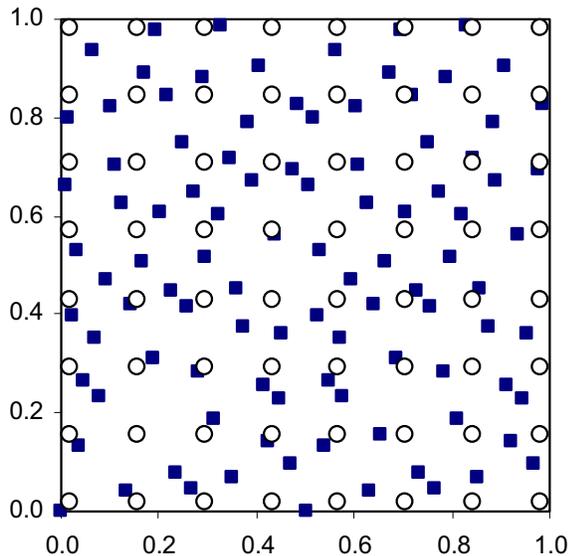


Figure 1: Example of distributions of nodes and interpolation points (Hollow circles: interpolation points; Solid squares: nodes)

Generally, as noted before, Eq. (13) is used in

the MLPG_R method to discretise Eq. (2), giving the relationship between a function value at any point and nodal values of the same function at nodes. On the other hand, Eq. (15) is employed to estimate the pressure gradient of the same function at nodes by using its nodal values for evolving the velocity in Eq. (1). Therefore, different approaches should be adopted when investigating the convergent rate of Eq. (13) and Eq. (15).

To investigate the convergent rate of Eq. (13), the assumed functions are interpolated by the equation at a set of points. These interpolation points are not necessarily coincided with any node and the number of the points is not necessary the same as the number of nodes. In fact, the number of points in the following tests is fixed as 64 except for Section 5.3. For clarity, these points are denoted by \vec{r}_{0k} while nodes are still denoted by \vec{r}_J as above. The distribution of the points is illustrated in Fig. 1. The error of the results of interpolation is defined as

$$E_{mean} = \frac{1}{K} \sum_k^K |f(\vec{r}_{0k}) - \bar{f}(\vec{r}_{0k})| \quad (17)$$

where E_{mean} is the mean error, $f(\vec{r}_{0k})$ is the interpolated value at the interpolation points and $\bar{f}(\vec{r}_{0k})$ is the values computed by the formula defining a function at the same point; K is the number of interpolation points.

For investigating the convergent rate of Eq. (15), the gradient of the function is estimated at the nodes by the equation and the error is found by the following expression

$$E_{gmean,y} = \frac{1}{M} \sum_J^M |f_{,y}(\vec{r}_J) - \bar{f}_{,y}(\vec{r}_J)| \quad (18)$$

where $E_{gmean,y}$ represents the mean error of the y-component of the gradient, $f_{,y}(\vec{r}_J)$ is the approximate value of the y-component of the gradient obtained by interpolation, $\bar{f}_{,y}(\vec{r}_J)$ is its counterpart computed by the formula defining the function and M is the total number of nodes. The mean error of the x-component of the gradient can be estimated in the same way by replacing y with x.

There are many options for the weight function. It is not necessary to use the same one for estimating

unknown functions and for estimating their gradients. In this paper, however, we mainly concern about the convergent rate of different formulations rather than the best weight function. Therefore, the spline function is employed in all the cases, i.e.,

$$w(|\Delta\vec{r}|) = \begin{cases} 1 - 6\left(\frac{|\Delta\vec{r}|}{h_I}\right)^2 + 8\left(\frac{|\Delta\vec{r}|}{h_I}\right)^3 - 3\left(\frac{|\Delta\vec{r}|}{h_I}\right)^4 & 0 \leq \frac{|\Delta\vec{r}|}{h_I} \leq 1 \\ 0 & \frac{|\Delta\vec{r}|}{h_I} > 1 \end{cases}$$

where $|\Delta\vec{r}|$ is the distance of two points as defined before and h_I is the size of the support domain of the weight function which is given by $h_I = kh_{4I}$ with h_{4I} being the distance between Node I and the fourth nearest neighbour and with k being a scale factor.

5.1 Case 1 – second order polynomial function

The first considered is a polynomial function of second order expressed by $f = 1 + 2x^2 + 3y^2$. Its gradient components are easy to find and is not written out here. The total number (M) of nodes in the square domain described above is selected as 25, 100, 400, 900 or 1600, respectively, in different runs. The convergent rates for interpolation of the function at 64 points by using three methods are shown in Fig. 2, where the scale factors for the SFDI and MLS are 2.5 and for the MPS two curves are shown corresponding to the scale factors of 2.5 and 5, respectively. The convergent rates are denoted by the decrease of mean errors defined in Eq. (17) with the increase in the total number of nodes. The figure demonstrates that the errors of all three methods are reduced if more nodes are distributed in the same domain. The rates of reduction in errors of the SFDI and MLS methods are similar while the rate of the MPS is considerably slow compared with other two methods. This obviously indicates that the SFDI and MLS can achieve the similar level of accuracy while the MPS is not as robust as other two when nodes are irregularly distributed.

Fig. 3 shows the convergent rates of the three methods for estimating the gradient components

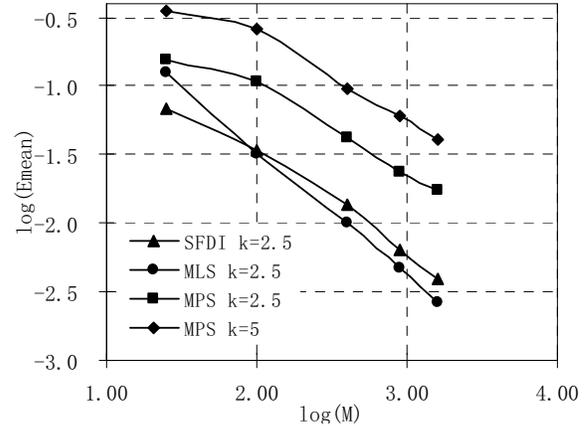


Figure 2: Convergent rates of three methods for interpolating the polynomial function

or partial derivative of the polynomial function. The value of $f_{,y}$ ($f_{,x}$ is similar and is not necessary to show) is computed by using Eq. (15), (3f) and (5c), respectively, and the error is yielded by Eq. (18). It can be seen that the errors of both the SFDI and MLS methods are almost the same and decrease with increase in the number of nodes while the MPS loses its reasonableness for the scale factor of 2.5 for the irregular distribution of nodes. The results of the MPS corresponding to the scale factor of 5 seem to be more reasonable but still far worse than those of other two methods. This example demonstrates that Eq. (5c) from the MPS is not always reliable to estimate the gradient and should not be considered as an option for problems with a large deformation where original regular distribution of nodes may become irregular.

One may notice from the figures that the scale factor may affect the convergent property of these methods. Investigations are then made by selecting different scale factors. The results of the SFDI for the different scale factors of 1.8, 2.1, 2.5 and 3.0 are shown in Fig 4 and Fig. 5. It is interesting to see that convergent rate of these methods are not very sensitive to the scale factors. This may be considered as another advantage of the SFDI because people may not always know the optimised values of the scale factor.

The convergent rate of the MLS method corresponding to the scale factors of 1.8, 2.1, 2.5 and

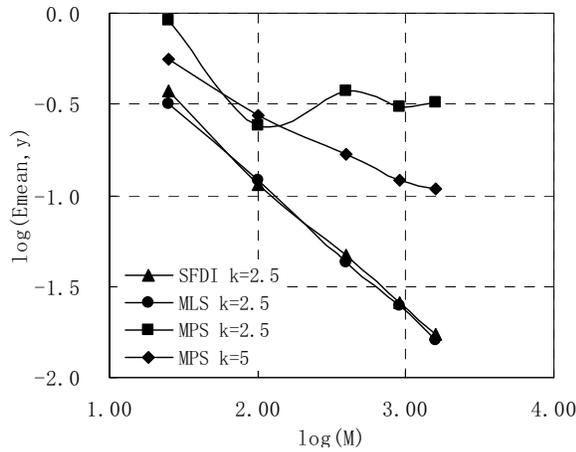


Figure 3: The convergent rate of three methods for estimating the gradients

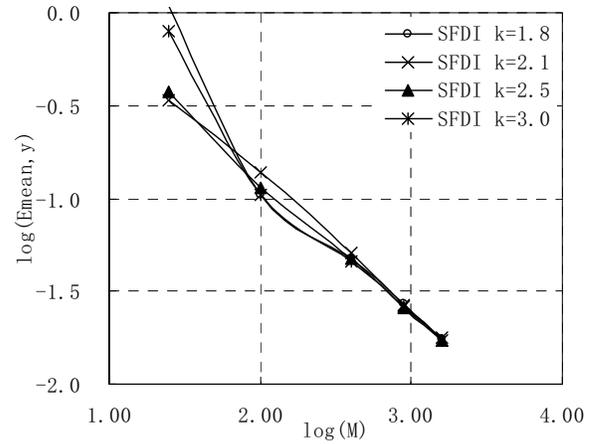


Figure 5: Convergent rate of the SFDI for estimating the gradients (Eq. (15))

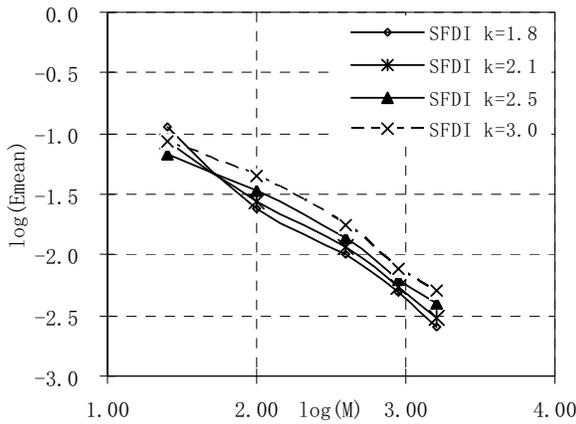


Figure 4: Convergent rate of the SFDI for interpolating the polynomial function (Eq. (13))

3.0 are depicted in Fig. 6 and Fig. 7. Compared with the results in Figs. 4 and 5, the reduction in the errors for interpolating the polynomial function seems to be faster here with the decrease of the scale factor and the reduction in the errors for estimating the gradients for different scale factors seem to be the same when the total number of nodes is large enough. However, when the scale factor is small and the total number of nodes is not big enough, the results of the MLS is not as good as those of the SFDI. This is clearly illustrated by the cases with the scale factor being 2.1 or less. That is because the number of neighbour nodes at some points is not large enough when the scale factor and so support domain is small. One

may deduce from this fact that the MLS scheme may not work well in some sub-areas where nodes are thinly scattered even though total number of nodes in the whole domain may be large enough. Such circumstances may happen to simulating violent flow of fluids, e.g. breaking waves. At the beginning, one may distribute enough number of nodes in the whole domain. However when waves become breaking, nodes in the front area of the breaking waves may become very fragmentary. The investigation in this subsection seems to show that the SFDI may yields better results than the MLS when modelling such waves.

The results obtained by the MPS method are de-

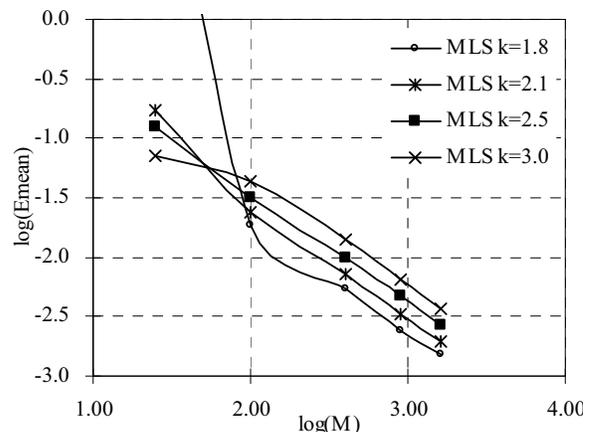


Figure 6: Convergent rate of the MLS for interpolating the polynomial function (Eq. (3a))

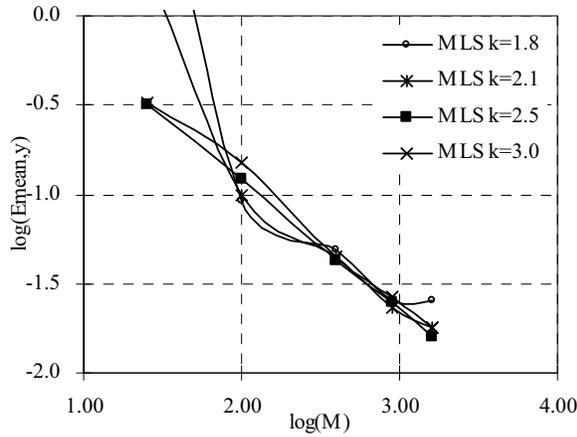


Figure 7: Convergent rate of the MLS for estimating the gradients (Eq. (3f))

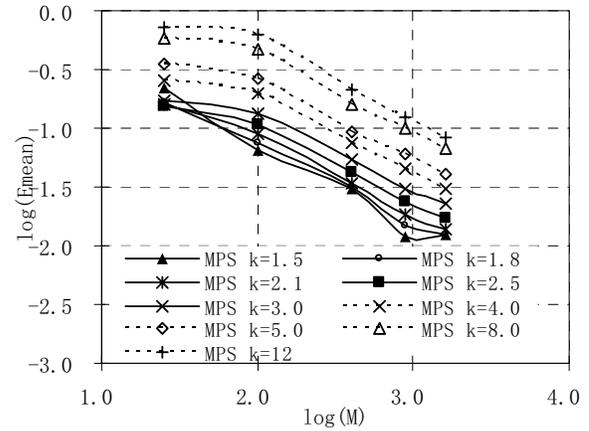


Figure 8: Convergent rate of the MPS for interpolating the polynomial function (Eq.(5a))

pictured in Fig. 8 and Fig. 9. As the convergent property of this method seems to be sensitive to the scale factor as illustrated in Figs. 2 and 3, a larger range of the factor, from 1.5 to 12, is investigated. These figures show that the results of the MPS can be very different if the scale factor is not properly selected. They also show that the best scale factor for interpolation of the function is different from that for estimating the gradients. The former is near 1.5 and the latter near 5 for the second-order polynomial. The requirement of a large scale factor by the MPS method means that a large number of neighbour nodes are involved in the evaluation of the gradients. That does not only increase the computational costs but also degrade the accuracy in the region where the gradient varies rapidly. Therefore, a great care must be taken when choosing the scale factor for the MPS method.

5.2 Case 2 – cosine function

The second function considered is defined by $f = \cos(0.5\pi x)\cos(0.5\pi y)$. The same investigations as for the polynomial function are made for this cosine function, i.e. the computational domain, the number of nodes and the values of the scale factor are all the same. The convergent rates for interpolating the cosine function and for estimating its derivative by the three methods are plotted in Fig. 10 and Fig. 11, respectively. Compared Fig. 10 with Fig. 2 and Fig. 11 with Fig. 3, it can

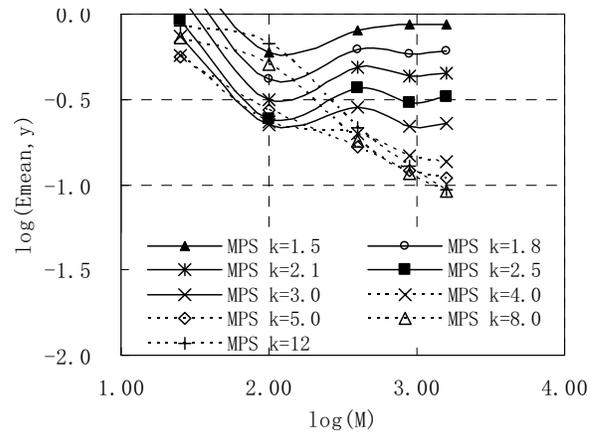


Figure 9: Convergent rate of the MPS for estimating the gradients (Eq. (5c))

be seen that the curves in the corresponding figures are largely similar, though specific values are not the same due to different functions concerned with.

The effects of the scale factors on the convergent rates for the cosine function are also looked at. All the results are presented in Fig. 12 to Fig. 17. These figures seem to support the following conclusions obtained by using the polynomial function. 1) The results of the SFDI are not sensitive to the scale factors. 2) The MLS method generally works well but may not be as good as the SFDI when the scale factor has a small value and when the total number of nodes is not large enough. 3) The results of the MPS method do not converge

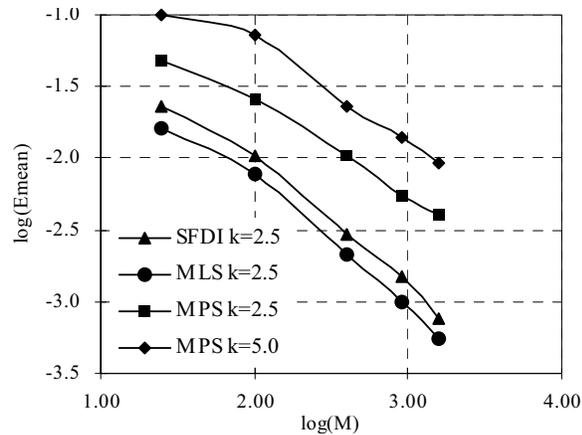


Figure 10: Convergent rates of three methods for interpolating the cosine function

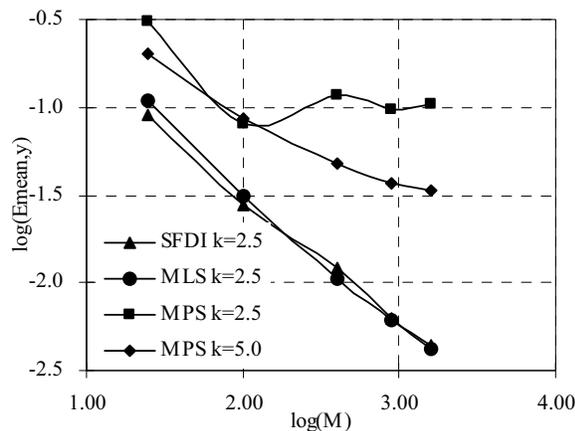


Figure 11: Convergent rates of three methods for estimating the gradient of cosine function

as fast as those of other two methods and are sensitive to the scale factors. The best scale factors are different for interpolating the function and for estimating the gradient (1.5 for the former and 8 for the later in this case).

5.3 CPU time

As has been seen, the SFDI can be as accurate as the MLS method. Based on the discussions in Sections 3 and 4, one has known that the SFDI should need less CPU time than the MLS method for a same problem. In this section, the ratio of CPU time required by the SFDI to that by the MLS method will be quantified. For this purpose, calculations of interpolating the polynomial func-

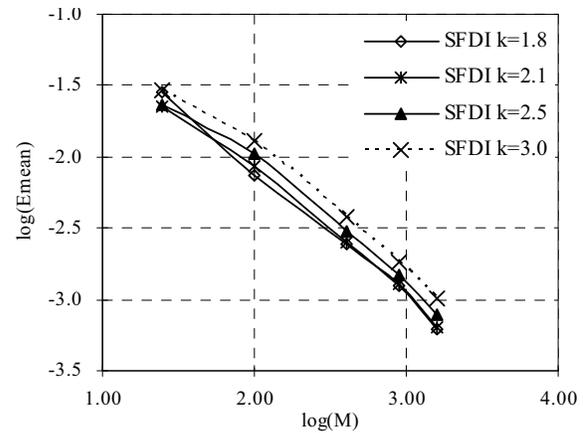


Figure 12: Convergent rate of the SFDI for interpolating the cosine function (Eq. (13))

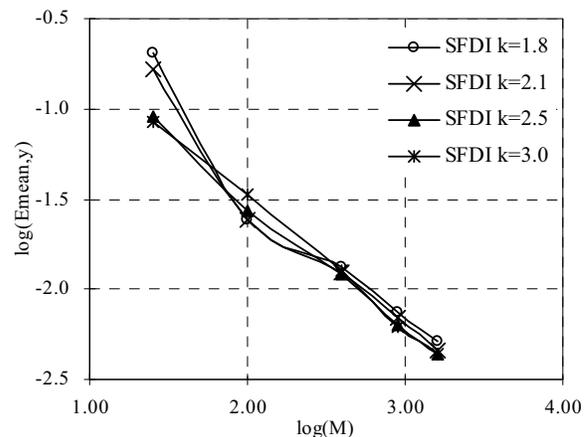


Figure 13: Convergent rate of the SFDI for estimating the gradient of cosine function (Eq. (15))

tion and estimating its gradient are performed 100 times on the same computer (a Laptop with 1 GB RAM and 1.8 GHz processor) by using the two methods with the scale factor of 2.5. To find the ratio of CPU time for interpolating the function, the total number (M) of nodes is selected as 1600 but the number of interpolation points (K) varies from 64 to 6400. To find the ratio of CPU time for estimating the gradient at nodes, the total number of nodes varies from 400 to 1600. Fig. 18 shows the ratio of CPU time for interpolating the function used by the SFDI to that by the MLS method while Fig. 19 gives the ratio of CPU time for estimating the gradient used by the SFDI to that by the MLS method. It can be seen that the ratio in

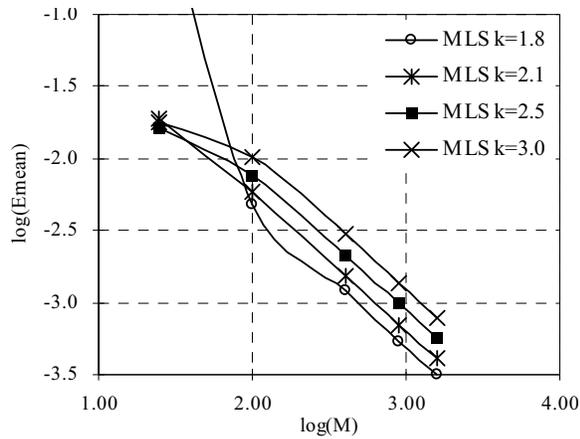


Figure 14: Convergent rate of the MLS for interpolating the cosine function (Eq. (3a))

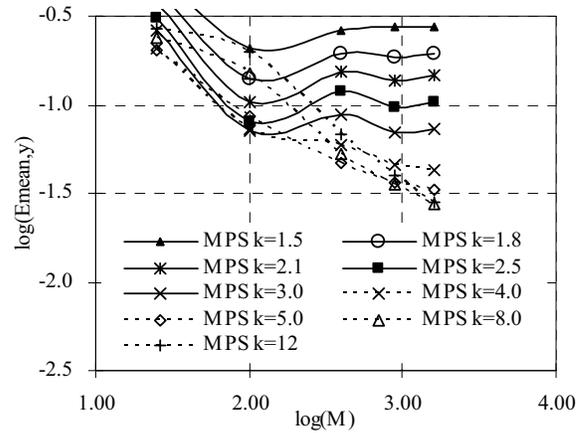


Figure 17: Convergent rate of the MPS for estimating the gradient of cosine function (Eq.(5c))

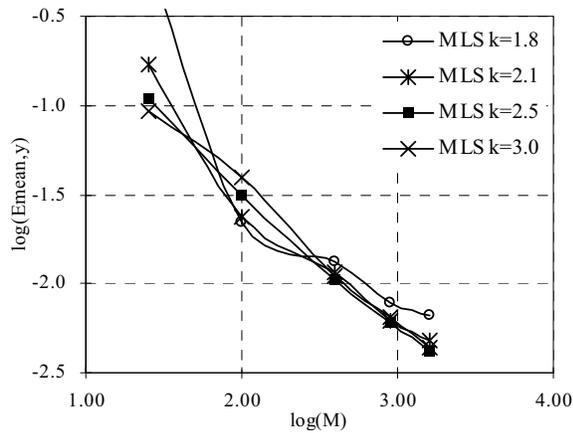


Figure 15: Convergent rate of MLS for estimating the gradient of cosine function (Eq. (3f))

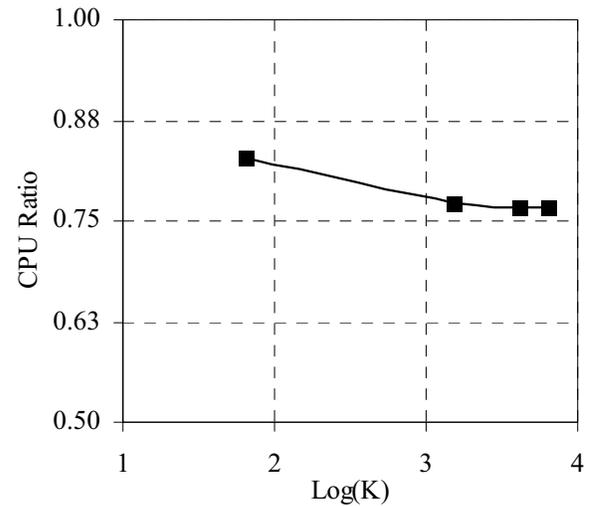


Figure 18: Ratio of CPU time used by the SFDI to that by the MLS for interpolating the function

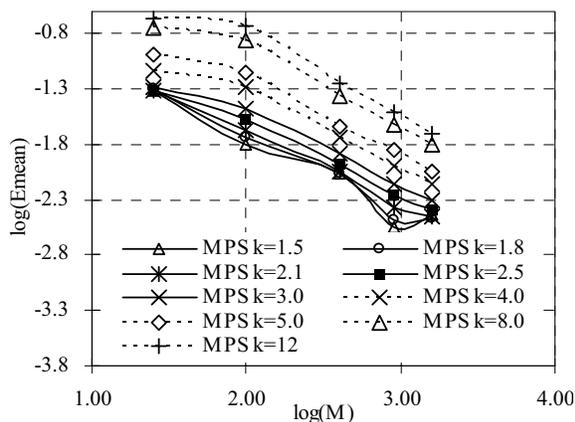


Figure 16: Convergent rate of the MPS for interpolating the cosine function (Eq.(5a))

Fig. 18 is about 0.76 while the ratio is only 0.16 in Fig. 19. In addition to this, the ratio seems not to vary significantly with the change in the number of interpolation points or nodes. It is noted that the specific values of the ratios may depend on the scale factor. However, according to numerical tests (not given here), it is found that reduction in the scale factor tends to decrease the ratios. It is also noted that both ratios should be smaller for 3D cases based on discussions in Sections 3 and 4.

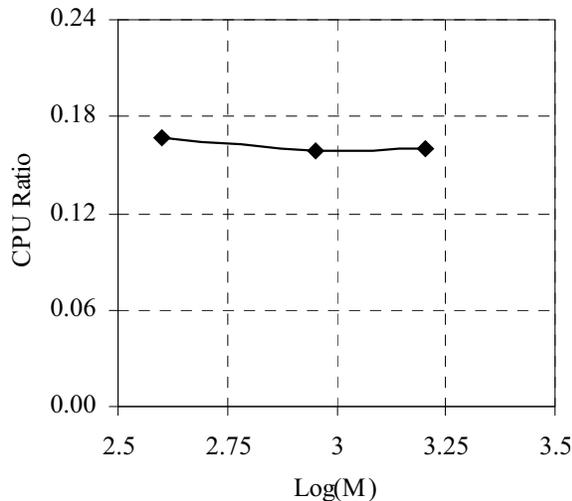


Figure 19: Ratio of CPU time used by the SFDI to that by the MLS method for estimating the gradient

6 Conclusions

In this paper, a new meshless interpolation scheme, named as the SFDI, for the MLPG_R method is developed and numerically investigated. This method is derived by using the Taylor series with ignoring the terms of second and higher order derivatives and is therefore of second order accuracy. Based on the numerical tests, one observes the following features of the scheme. (1) The SFDI is as accurate as the MLS method generally but may be more accurate than the later when the number of neighbour nodes is small. (2) The SFDI needs considerably less CPU time to evaluate than the MLS. (3) The scheme is not sensitive to the scale factors. (4) It is much more accurate than the scheme used in the MPS method when nodes are irregularly distributed. Although this scheme is purposely developed for the MLPG_R method, it may also be used for interpolation of a function and calculation of its gradients in the other meshless methods.

Acknowledgement: This work is sponsored by The Leverhulme Trust, UK, to which the author is most grateful.

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