

An Error Estimator for the Finite Element Approximation of Plane and Cylindrical Acoustic Waves.

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Abstract: This paper deals with a Finite Element Method (FEM) for the approximation of the Helmholtz equation for two dimensional problems. The acoustic boundary conditions are weakly posed and an auxiliary problem with homogeneous boundary conditions is defined. This auxiliary approach allows for the formulation of a general solution method. Second order finite elements are used along with a discretization parameter based on the fixed wave vector and the imposed error tolerance. An explicit formula is defined for the mesh size control parameter based on Padé approximant. A parametric analysis is conducted to validate the rectangular finite element approach and the mesh control parameter. The results of the examples show that the discrete dispersion relation (DDR) can be used for the rectangular finite element mesh refinement under predefined error tolerances. It is also shown that the numerical formulation is robust and can be extended to higher order finite element analyses.

Keywords: Numerical Methods in Engineering, Finite Element Method, Helmholtz Equations, Plane and Cylindrical Wave Propagation.

1 Introduction

Numerical solutions of the Helmholtz Equation are well-known in literature, where finite and boundary element methods of approximation have been proposed for a broad range of problems.

One particular issue addressed by many authors is the necessary/minimum mesh discretization for the solution approximation for a fixed wavenumber. See for instance, Harari et al. (1996), who used the technique of dispersion analysis to include complex wavenumbers. In addition, complex Fourier analysis techniques were

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used by them to observe the dispersion and attenuation characteristics of the p -version finite element method. Based on numerical evidences they conjectured that the elements of degree p provide an approximation of order $2p$ for the dispersion relation in the limit when the element size tends to zero. Ainsworth (2003) analyzed the discrete dispersion in the approximation by finite elements with relatively high wavenumbers. Sarkar et al. (2011) showed that infinite flexible structural acoustic waveguides have a general form for the dispersion equation. Christon (1999) considered the dispersive behaviour of a variety of second order finite elements for wave equations and presented numerical comparisons between the discrete phase, group velocity and the analytical value. Babuška et al. (1995) studied the scattering properties of high order finite elements for the Helmholtz equation in one dimension, and obtained estimates up to the fifth order approximation, in which the product between the temporal frequency and the mesh parameter is smaller than one, that is, when $\omega h < 1$. The same article presents numerical evidences, which lead to the conjecture that elements of order p have an order approximation $2p$ for dispersion relation when the mesh parameter h tends to zero. Sebold et al. (2014) presented analytical expressions that provide information to the mesh control of edge finite element for the approximation of Maxwell's equations. Such expressions were generated from the numerical phase velocity and dispersion analysis. Another important task in the present work is the use of hierarchical basis functions, Adjerid (2002). A hierarchical basis has the property that the base level $p + 1$ is obtained by adding new functions to the base level p , i.e., the base as a whole does not need to be rebuilt when the degree of the polynomial is increased. This property is desirable, if not essential, when using the p -version of the finite element method. The hierarchical basis functions in one-dimension are defined as integrals of Legendre polynomials. Thus, the orthogonality properties are guaranteed, leading to sparse and well conditioned stiffness matrices. Although the proposal of analytical expressions for the mesh refinement, based on the discrete dispersion relation, is a significant contribution of this article, the main novelty is the presentation of a contribution applied to acoustic which related with the works mentioned above. This contribution enables one to extend the work of Sebold et al. (2014) to nodal finite elements, unifying, from this point of view, the acoustic studies presented by Christon (1999) for numerical phase velocity and Babuška et al. (1995) for discrete dispersion relation.

In this study the discrete dispersion relation suggests the used of the phase velocity number as an error estimator for the finite element approximation of the Helmholtz equation. The analytical expressions for the numerical phase velocity can be used to estimate the approximation error in the presence of plane or cylindrical waves, thus providing a faster, more efficient and less expensive computationally way to

obtain results within an imposed error margin. It is the authors' reasoning that restricting the study to quadrilateral elements is a convenient way to provide an initial understanding for those readers interested in the foundations of this theory.

2 Basis functions

Let Ω be an open and bounded domain in the real set \mathbb{R} , and let $\mathcal{X}_{hp} \subset H^1(\Omega)$ be a subspace of piecewise continuous polynomials of degree $p \in \mathbb{Z}^+$ with m variables denoted by $\mathcal{P}_p^{(m)}$, i.e.

$$\mathcal{X}_{hp} = \{u_{hp} \mid u_{hp} \in C^0(\Omega) \cap \mathcal{P}_p^{(m)}(\Omega_e)\}, \quad (1)$$

where $C^0(\Omega)$ is the space of all continuous functions on Ω , $H^1(\Omega)$ is the Hilbert space of differentiable functions u , such that u and $\frac{\partial u}{\partial x_j}$, with $j = 1, \dots, m$, are integrable square functions.

2.1 Legendre hierarchical base functions

Let M_j be the set of Legendre polynomials defined on a reference element Ω_e , which are given by Rodrigues formula, Olver et al. (2010), for $0 \leq j \leq p$ as:

$$M_j(\xi) = \frac{1}{2^j j!} \frac{d^j}{d\xi^j} [(\xi^2 - 1)^j], \quad \xi \in \Omega_e$$

Furthermore, consider the subset $N_k^{(p)} \in \mathcal{P}_p^{(1)}$, with $k \in \mathbb{Z}^+$, defined according to:

$$\begin{cases} N_k^{(p)}(\xi) = \frac{1}{2}(1 + \xi_k \xi), & k = 1, 2, \\ N_k^{(p)}(\xi) = \frac{1}{\|M_{k-2}\|} \int_{-1}^{\xi} M_{k-2}(t) dt, & k = 3, \dots, p+1 \end{cases} \quad (2)$$

where $\xi_1 = -1$, $\xi_2 = 1$ and $\|M_{k-2}\|^2 = \frac{2}{2k-3}$. Note that $N_k^{(p)}(\pm 1) = 0$ for $k \geq 3$. Note that this happens because of the orthogonality of M_j with respect to the L_2 -inner product when the upper limit of integration, in equation (2), is $\xi = 1$. One may arrive intuitively at the same conclusion by taking $\xi = -1$.

The functions defined by equations (2) form what is called Legendre Hierarchical Shape Functions, Harari et al. (1996) and Thompson and Pinsky (1994).

2.2 Hierarchical base functions for rectangular elements of p -order

Let $\mathcal{P}_p^{(2)}$ be the space of polynomials in two variables, associated to the elements of p -order, defined as

$$\mathcal{P}_p^{(2)} = \{\hat{f}(\xi, \eta); \hat{f}(\xi, \eta) \in span\{X_{p,q}\}; \text{ with } q \in \mathbb{Z}^+\} \quad (3)$$

where $X_{p,q}$ is the monomial set of degree less or equal to p in ξ and of degree less or equal to q in η , i.e.

$$X_{p,q} = \{\xi^r \eta^s; \quad 0 \leq r \leq p; \quad 0 \leq s \leq q\} \tag{4}$$

Thus, the basis functions with two variables, ξ and η , of order $p = q$, are given by the tensor product

$$\begin{bmatrix} N_1^{(p)}(\xi) \\ N_3^{(p)}(\xi) \\ \vdots \\ N_k^{(p)}(\xi) \\ N_2^{(p)}(\xi) \end{bmatrix} \begin{bmatrix} N_1^{(p)}(\eta) & N_3^{(p)}(\eta) & \cdots & N_k^{(p)}(\eta) & N_2^{(p)}(\eta) \end{bmatrix}, \tag{5}$$

where each product $N_i^{(p)}(\xi)N_j^{(p)}(\eta) \in \mathcal{P}_p^{(2)}$, for $i, j = 1, 2, \dots, k$. Each polynomial appearing in the tensor product entries (5) is associated with a single node l of the reference element. In particular, for $p = 2$, the basic functions \hat{f} are defined as follows. Considering the set (3), the basis functions are generated by

$$span\{X_{2,2}\} = span\{1, \xi, \eta, \xi^2, \eta^2, \xi\eta, \xi^2\eta, \eta^2\xi, \xi^2\eta^2\}$$

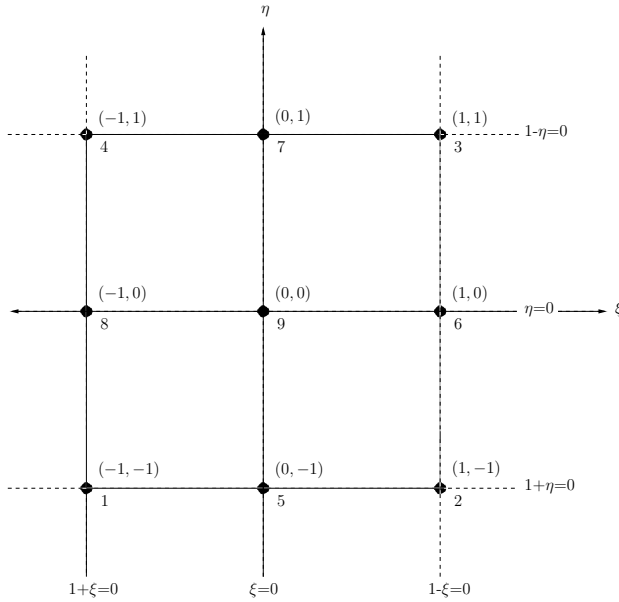
Thus, it follows that each basis function $\hat{f}_l(\xi, \eta) = N_i^{(2)}(\xi)N_j^{(2)}(\eta)$, with $l = 1, \dots, 9$ and with $i, j = 1, 2, 3$, associated with the node l , appears at the tensor product entries, see equation (6) and Figure 1(a),

$$\begin{bmatrix} N_1^{(2)}(\xi) \\ N_3^{(2)}(\xi) \\ N_2^{(2)}(\xi) \end{bmatrix} \begin{bmatrix} N_1^{(2)}(\eta) & N_3^{(2)}(\eta) & N_2^{(2)}(\eta) \end{bmatrix} =$$

$$\begin{bmatrix} N_1^{(2)}(\xi)N_1^{(2)}(\eta) & N_1^{(2)}(\xi)N_3^{(2)}(\eta) & N_1^{(2)}(\xi)N_2^{(2)}(\eta) \\ N_3^{(2)}(\xi)N_1^{(2)}(\eta) & N_3^{(2)}(\xi)N_3^{(2)}(\eta) & N_3^{(2)}(\xi)N_2^{(2)}(\eta) \\ N_2^{(2)}(\xi)N_1^{(2)}(\eta) & N_2^{(2)}(\xi)N_3^{(2)}(\eta) & N_2^{(2)}(\xi)N_2^{(2)}(\eta) \end{bmatrix} =$$

$$\begin{bmatrix} \hat{f}_1(\xi, \eta) & \hat{f}_8(\xi, \eta) & \hat{f}_4(\xi, \eta) \\ \hat{f}_5(\xi, \eta) & \hat{f}_9(\xi, \eta) & \hat{f}_7(\xi, \eta) \\ \hat{f}_2(\xi, \eta) & \hat{f}_6(\xi, \eta) & \hat{f}_3(\xi, \eta) \end{bmatrix} =$$

$$\begin{bmatrix} \frac{1}{4}(1-\xi)(1-\eta) & \sqrt{\frac{3}{32}}(1-\xi)(\eta^2-1) & \frac{1}{4}(1-\xi)(1+\eta) \\ \sqrt{\frac{3}{32}}(\xi^2-1)(1-\eta) & \frac{3}{8}(\xi^2-1)(\eta^2-1) & \sqrt{\frac{3}{32}}(\xi^2-1)(1+\eta) \\ \frac{1}{4}(1+\xi)(1-\eta) & \sqrt{\frac{3}{32}}(1+\xi)(\eta^2-1) & \frac{1}{4}(1+\xi)(1+\eta) \end{bmatrix} \quad (6)$$



(a)

Figure 1: Reference element Ω_e associated with the basis functions of $p = 2$.

3 Helmholtz equation and the finite element method approach

3.1 Plane wave

Let $\Omega \subset \mathbb{R}^2$ be a domain with boundary Γ . The homogeneous acoustic wave equation can be written as

$$\frac{\partial^2 u}{\partial x_1^2} + \frac{\partial^2 u}{\partial x_2^2} - \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2} = 0 \quad (7)$$

For time harmonic waves, a solution of equation (7) can be written as

$$u(\mathbf{x}, t) = \tilde{u}(\mathbf{x})e^{-i\omega t}, \tag{8}$$

where $\tilde{u}(\mathbf{x})$ is the sound pressure amplitude in the frequency domain and c is the speed of sound. Substituting equation (8) in equation (7), the following homogeneous scalar Helmholtz Equation in two dimensions can be obtained:

$$\nabla^2 \tilde{u}(\mathbf{x}) + \frac{\omega^2}{c^2} \tilde{u}(\mathbf{x}) = 0 \quad \forall \mathbf{x} \in \Omega \tag{9}$$

Furthermore, one can assume that the wave vector $\boldsymbol{\kappa} = (\kappa_1, \kappa_2)$ is related to the circular frequency ω by the dispersion relation, Oliveira et al. (2007),

$$\omega = c|\boldsymbol{\kappa}| = c\sqrt{\kappa_1^2 + \kappa_2^2} \tag{10}$$

Thus, the following variational problem, present in Liu (2009), can be stated: Find $\tilde{u} \in H^1(\overline{\Omega})$ such that

$$(\nabla \tilde{u}, \nabla w)_{L_2} = \frac{\omega^2}{c^2} (\tilde{u}, w)_{L_2} \quad \forall w \in H_0^1(\Omega) \tag{11}$$

in which $(\cdot, \cdot)_{L_2}$ denotes the inner product $L_2(\Omega)$. The problem (11) is subject to boundary conditions

$$\begin{cases} \text{Pressure :} & \tilde{u} = u_B \quad \forall \mathbf{x} \in \Gamma. \\ \text{Velocity :} & \frac{\partial \tilde{u}}{\partial x_j} = i\kappa_j \rho v(\mathbf{x}) \quad \forall \mathbf{x} \in \Gamma \end{cases} \tag{12}$$

where $i = \sqrt{-1}$, ρ is the mass density ($\rho = 1,29 \text{ kg/m}^3$ for air under 0°C and 1-atm), v is the particle velocity and the quantity u_B is a given complex function. If one chooses $v(\mathbf{x}) = e^{i\boldsymbol{\kappa}\cdot\mathbf{x}}$, then an exact solution to the problem (11) with boundary conditions (12) is given by $u(\mathbf{x}) = \rho e^{i\boldsymbol{\kappa}\cdot\mathbf{x}}$. Approximation by finite elements with $u_h \in \mathcal{X}_{hp} \subset H^1(\Omega)$ is such that

$$(\nabla u_h, \nabla w_h)_{L_2} = \frac{\omega^2}{c^2} (u_h, w_h)_{L_2} \tag{13}$$

for all $w_h \in \mathcal{X}_{hp} \cap H_0^1(\Omega)$, where $H_0^1(\Omega) = \{u \in H^1(\Omega); u(\mathbf{x}) = 0 \quad \forall \mathbf{x} \in \Gamma\}$. The boundary conditions are applied requiring $u_h(\mathbf{x}) = \rho v_h(\mathbf{x})$, $\forall \mathbf{x} \in \Gamma$, where $v_h(\mathbf{x})$ is the discrete version of the complex exponential $v(\mathbf{x}) = e^{i\boldsymbol{\kappa}\cdot\mathbf{x}}$, Sebold et al. (2014).

An alternative approach, which aims a simpler programming solution for the problem (11)-(12), is presented in the sequence. The idea is to establish, from $u(\mathbf{x})$ data,

a new problem with homogeneous boundary conditions. The new problem is solved with second order finite element method using the Legendre hierarchical shape functions for rectangular elements. Once the solution to the new problem has been found, the next step is the recovery of the solution of the problem given by equations (11)-(12). For this approach, $\alpha(\mathbf{x}) = 1 + x_1^2 x_2^2 (1 - x_1)^2 (1 - x_2)^2$ is defined, as well as $u_0(\mathbf{x}) = \alpha(\mathbf{x})u(\mathbf{x})$ and $\bar{u}(\mathbf{x}) = u(\mathbf{x}) - u_0(\mathbf{x})$ for all $\mathbf{x} \in \Omega = (0, 1) \times (0, 1)$. Thus, one has the new boundary conditions: $\bar{u}(\mathbf{x}) = \frac{\partial \bar{u}(\mathbf{x})}{\partial x_j} = 0, \forall \mathbf{x} \in \Gamma$, with $j = 1, 2$. Proceeding this way, the problem defined by (11)-(12) turns into the non-homogeneous problems

$$\nabla^2 \bar{u}(\mathbf{x}) + \frac{\omega^2}{c^2} \bar{u}(\mathbf{x}) = f(\mathbf{x}) \quad \forall \mathbf{x} \in \Omega \tag{14}$$

where $f(\mathbf{x}) = \nabla^2 u_0(\mathbf{x}) + \frac{\omega^2}{c^2} u_0(\mathbf{x})$. Therefore, $\bar{u} \in H_0^1(\Omega)$ satisfies the following variational problem:

$$(\nabla \bar{u}, \nabla w)_{L_2} - \frac{\omega^2}{c^2} (\bar{u}, w)_{L_2} = (f, w)_{L_2} \quad \forall w \in H_0^1(\Omega), \tag{15}$$

subject to the boundary conditions

$$\left\{ \begin{array}{l} \text{Pressure : } \bar{u}(\mathbf{x}) = 0 \\ \text{Velocity : } \frac{\partial \bar{u}(\mathbf{x})}{\partial x_j} = 0 \end{array} \right. \quad \forall \mathbf{x} \in \Gamma \tag{16}$$

Discretizing the domain Ω , the approximation by second order finite elements $\bar{u}_h \in \mathcal{X}_{h2} \cap H_0^1(\Omega)$ is calculated, such that

$$(\nabla \bar{u}_h, \nabla w_h)_{L_2} - \frac{\omega^2}{c^2} (\bar{u}_h, w_h)_{L_2} = (f, w_h)_{L_2} \tag{17}$$

for all $w_h \in \mathcal{X}_{h2} \cap H_0^1(\Omega)$. Once the problem (15)-(16) is solved for \bar{u}_h the approximate solution of the problem (11)-(12) is obtained by carrying out the substitution: $u_h = \bar{u}_h + u_0$.

3.2 Cylindrical wave

Another relevant case appears when one has as solution of (14) the convolution

$$\hat{u}(\mathbf{x}) = (g * f)(\mathbf{x}) = \int_{\mathbb{R}^d} g(\mathbf{x} - \mathbf{y}) f(\mathbf{y}) d\mathbf{y} \tag{18}$$

where $g, f \in L^p(\Omega)$, with $1 \leq p \leq \infty$, has compact support in the domain $\Omega \subset \mathbb{R}^d$, with $d = 1, 2, \dots, n$. In the solution (18), g is known as free space Helmholtz Green's function, Beylkin et al. (2009). Furthermore, the function g satisfy

$$\nabla^2 g + \frac{\omega^2}{c^2} g = -\delta_{\mathbf{x}} \quad \forall \mathbf{x} \in \Omega \tag{19}$$

onde $\delta_{\mathbf{x}}$ is the Dirac-delta function concentrated in $\mathbf{x}^{(d)}$, Monk (2003). In three dimension, with $\mathbf{x}^{(3)} = (x_1, x_2, x_3)$ and $\mathbf{y}^{(3)} = (y_1, y_2, y_3)$, the expression of the fundamental solution to equation (19) is given by

$$g(\mathbf{x}^{(3)}, \mathbf{y}^{(3)}) = \frac{1}{4\pi} \frac{e^{i\frac{\omega}{c^2}|\mathbf{x}^{(3)}-\mathbf{y}^{(3)}|}}{|\mathbf{x}^{(3)}-\mathbf{y}^{(3)}|}, \quad \mathbf{x}^{(3)} \neq \mathbf{y}^{(3)} \tag{20}$$

The main interest of this work is the case $d = 2$. Thus, the fundamental solution in two dimensions can be obtained by taking $\mathbf{x}^{(2)} = (x_1, x_2)$ and $\mathbf{y}^{(2)} = (y_1, y_2)$, $r_1 = |\mathbf{x}^{(3)}-\mathbf{y}^{(3)}|$, $r_2 = |\mathbf{x}^{(2)}-\mathbf{y}^{(2)}|$, $x_3 = 0$, $y_3 = r_2 \sinh(t)$, with $t \in \mathbb{R}$ and the identity $\cosh(\theta) - \sinh(\theta) = 1$ for any θ angle. Thus, by taking

$$\begin{aligned} g(\mathbf{x}^{(2)}, \mathbf{y}^{(2)}) &= \int_{-\infty}^{\infty} g(\mathbf{x}^{(3)}, \mathbf{y}^{(3)})|_{x_3=0} dy_3 \\ &= \frac{1}{4\pi} \int_{-\infty}^{\infty} e^{i\frac{\omega}{c^2}r_2 \cosh(t)} dt \\ &= \frac{i}{4} h_0^{(1)} \left(\frac{\omega^2}{c^2} r \right) \end{aligned} \tag{21}$$

where $r = r_2 e^{h_0^{(1)}}$ is the Hankel function of the first kind, see equation 10.9.10 in Olver et al. (2010). Note that the solution in (21) satisfies the Sommerfeld radiation condition, that is:

$$\lim_{r \rightarrow \infty} r^{\frac{1}{2}} \left(\frac{\partial g}{\partial r} - i \frac{\omega^2}{c^2} g \right) = 0 \tag{22}$$

Suppose the cylindrical waves expanding from a punctual source which is located at $(0, 0) \in \mathbb{R}^2$, see Figure 2(a). Finite element approximation is considered on square domain $\Omega \subset \mathbb{R}^2$ extracted from Figure 2(a)(see Figure 2(b)).

3.3 Numerical experiments

Figure 3(a) shows the analytical solution of the problem (11)-(12), while Figure 3(b) shows the result of alternative approach suggested using second order finite elements, the wave vector $\boldsymbol{\kappa} = (10\pi, 10\pi)$, $h = 1/16$ and the Legendre hierarchical

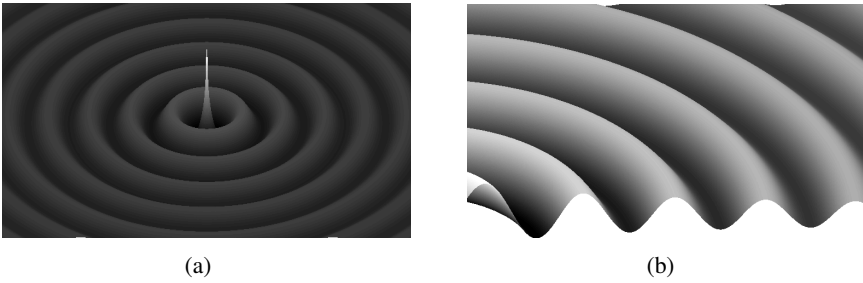


Figure 2: (a) Cylindrical wave; (b) Domain Ω .

basis functions for rectangular elements. Figures 4(a) and 4(b) show the exact solution (21) and finite element approach, respectively, referring to the cylindrical wave. This approximation is calculated using the same wave vector and the same parameter h for the plane wave approximation.

Figures 5(a), 5(b) and 5(c) depict the diagonal slice in the $(1, 1)$ direction of the plane wave from Figure 3(a), and of the discrete surface encountered by alternative approach from Figure 3(b), at different levels of refinement: $h = 1/16$, $h = 1/32$, $h = 1/64$.

Figures 6(a), 6(b) and 6(c) depict the diagonal slice in the $(1, 1)$ direction of the region propagation $\Omega = [1, 1] \times [2, 2]$ of the cylindrical wave, Figure 4(a), and of the discrete surface encountered by alternative approach, Figure 4(b), at different levels of refinement: $h = 1/16$, $h = 1/32$, $h = 1/64$.

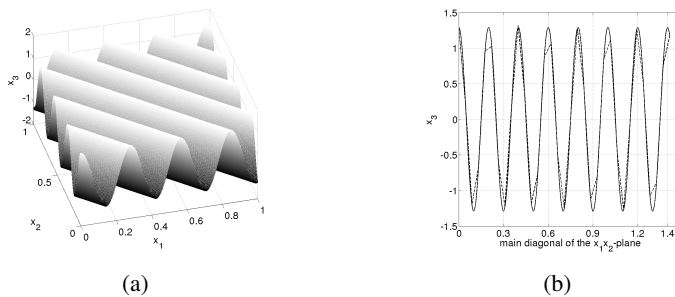


Figure 3: (a) Analytic solution of the problem (11)-(12); (b) Alternative finite element method approach with $p = 2$, $\kappa = 10\pi$ and refinement level $h = 1/16$.

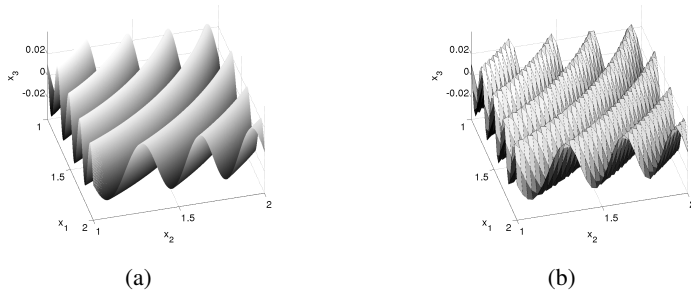


Figure 4: (a) Analytic Solution for cylindrical wave; (b) Alternative finite element method approach for cylindrical wave with refinement level $h = 1/16$.

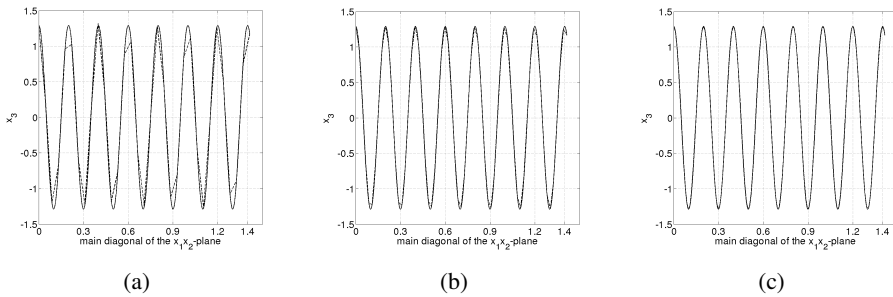


Figure 5: (a), (b) and (c) depict the diagonal slice in the (1, 1) direction of the plane wave, at different levels of refinement, $h = 1/16$, $h = 1/32$, $h = 1/64$, respectively.

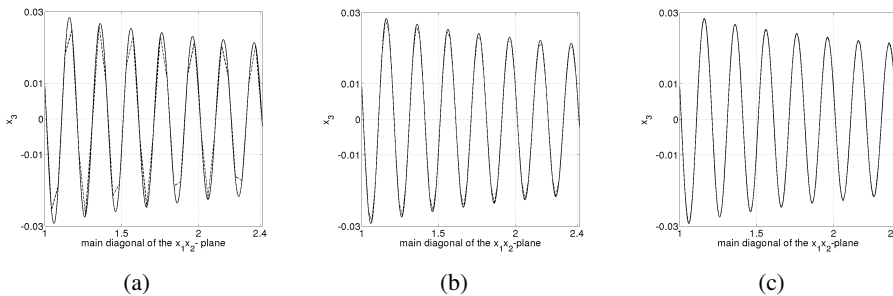


Figure 6: (a), (b) and (c) depict the diagonal slice in the (1, 1) direction of the region propagation $\Omega = [1, 1] \times [2, 2]$ of the cylindrical wave, at different levels of refinement, $h = 1/16$, $h = 1/32$, $h = 1/64$, respectively.

4 Discrete dispersion relation

First let's establish some requirements for the definition of the discrete dispersion relation for the scalar Helmholtz equation in two dimensions must be establish. Suppose that a uniform mesh size $h = \frac{1}{n} > 0$, with $n \in \mathbb{Z}$, is placed on the real line with nodes located at $h\mathbb{Z}$, where \mathbb{Z} is the set of integers. The set of continuous piecewise linear functions on the mesh is denoted \mathcal{X}_{h1} . In analogy to the continuous problem defined by equation (7), one should be concerned with solutions of the form

$$u_h(x, t) = \tilde{u}_h(x)e^{-i\omega t} \tag{23}$$

Let $l_n^{(1)} \in \mathcal{X}_{h1}$ be defined as $l_n^{(1)}(s) = \frac{s}{h} + 1 - n$ if $nh - h < s \leq nh$, and $l_n^{(1)}(s) = \frac{s}{h} + 1 - n$ if $nh < s < nh + h$. Note that $l_n^{(1)}$ one has the property

$$l_n^{(1)}(x + mh) = l_{n-m}^{(1)}(x), \quad x \in \Omega \text{ and } m \in \mathbb{Z} \tag{24}$$

If \tilde{u}_h is defined as

$$\tilde{u}_h(x) = \sum_{n \in \mathbb{Z}} e^{inkh} l_n^{(1)}(x), \tag{25}$$

then the property (24) shows that

$$\tilde{u}_h(x + nh) = e^{i\kappa nh} \tilde{u}_h(x), \quad \forall x \in \Omega \text{ and for each } n \in \mathbb{Z} \tag{26}$$

Thus, the analysis can be performed uniformly at any point of the mesh. The function $\tilde{u}_h \in \mathcal{X}_{h1}$ is a discrete version of the complex exponential $\tilde{u}(s) = e^{i\kappa s}$, where κ is the wavenumber, which is related to the frequency ω by the dispersion relation, found at Oliveira et al. (2007), and written below

$$\omega(\kappa) = c\kappa \tag{27}$$

Considering the Helmholtz equation in one dimension

$$\tilde{u}'' + \omega(\kappa)^2 \tilde{u} = 0 \tag{28}$$

the following variational problem can be stated: Find $\tilde{u}_h \in \mathcal{X}_{h1}$ such that

$$\int_{\mathbb{R}} \tilde{u}'_h(s) \overline{w}'_h(s) ds = \omega_h(\kappa)^2 \int_{\mathbb{R}} \tilde{u}_h(s) \overline{w}_h(s) ds \quad \forall w_h \in \mathcal{X}_{h1} \tag{29}$$

From another point of view, one can consider (29) as an eigenvalue problem, where $\omega_h(\kappa)^2$ can be calculated by setting $w_h = l_m^{(1)}$. In fact, after replacing equation (25)

into equation (29) and noting that $l_n^{(1)}(s)l_m^{(1)}(s) \neq 0$ for $s \in (mh - h; mh + h)$ and following a similar statement for $(l_n^{(1)}(s))'(l_m^{(1)}(s))'$, then follows

$$\omega_h(\kappa)^2 = \frac{6}{h^2} \left(\frac{1 - \cos(h\kappa)}{2 + \cos(h\kappa)} \right) \tag{30}$$

If $0 < h\kappa \ll 1$, equation (30) can be expanded as Maclaurin series, so

$$\omega_h(\kappa)^2 = \kappa^2 \left(1 + \frac{(h\kappa)^2}{12} + \dots \right) \tag{31}$$

By taking $c = 1$, from relation (27) it is found that $\omega(\kappa) = \kappa$. Considering the limit when $h \rightarrow 0$ in (31) one has

$$\omega^2(\kappa) = \omega_h^2(\kappa) \tag{32}$$

Expression (32) corresponds to the discrete dispersion relation for the scalar Helmholtz equation in one dimension.

4.1 Discrete dispersion relation for the Helmholtz equation in two dimensions

Suppose now that we have a real plane with nodes located at $h\mathbb{Z}^2$. The set of continuous piecewise polynomials with degree p less than or equal to two on the mesh is denoted \mathcal{X}_{h2} . In analogy to the solution of the continuous problem defined by equation (25), one should be concerned with solutions of the form

$$\tilde{u}_h(\mathbf{x}) = \beta L_h(\kappa_1, x_1) L_h(\kappa_2, x_2), \tag{33}$$

where

$$L_h(\kappa, s) = \sum_{m \in \mathbb{Z}} e^{im\kappa h} l_m^{(2)}(s) \quad \text{with} \quad l_m^{(2)} \in \mathcal{X}_{h2} \tag{34}$$

has nodal values defined by $l_m^{(2)}(nh) = \delta_{mn}$ (this feature can also be observed in $l_m^{(1)}$) and β is a constant. Thus, the presented problem is: Find $\tilde{u}_h \in \mathcal{X}_{h2}$, such that

$$\left(\frac{\partial \tilde{u}_h}{\partial x_1}, \frac{\partial w_h}{\partial x_1} \right) + \left(\frac{\partial \tilde{u}_h}{\partial x_2}, \frac{\partial w_h}{\partial x_2} \right) - \omega^2(\tilde{u}_h, w_h) = 0 \quad \forall w_h \in \mathcal{X}_{h2} \tag{35}$$

Choosing $w_h(\mathbf{x}) = l_m^{(2)}(x_1) l_m^{(2)}(x_2)$ and using equation (29), one has

$$(\tilde{u}_h, w_h) = \beta \prod_{r=1}^2 \int_{\mathbb{R}} L_h(\kappa_r, x_r) l_m^{(2)}(x_r) dx_r, \tag{36}$$

$$\left(\frac{\partial \tilde{u}_h}{\partial x_1}, \frac{\partial w_h}{\partial x_1} \right) = \beta \omega_h(\kappa_1)^2 \prod_{r=1}^2 \int_{\mathbb{R}} L_h(\kappa_r, x_r) l_m^{(2)}(x_r) dx_r \quad (37)$$

and

$$\left(\frac{\partial \tilde{u}_h}{\partial x_2}, \frac{\partial w_h}{\partial x_2} \right) = \beta \omega_h(\kappa_2)^2 \prod_{r=1}^2 \int_{\mathbb{R}} L_h(\kappa_r, x_r) l_m^{(2)}(x_r) dx_r \quad (38)$$

Replacing (36), (37) and (38) in (35) the discrete dispersion relation for the Helmholtz equation in two dimensions is obtained. It is written as follows:

$$\omega^2 = \omega_h(\kappa_1)^2 + \omega_h(\kappa_2)^2 \quad (39)$$

4.2 Discrete dispersion relation for elements of p -order.

In order to use equation (30), it is desirable to express $\omega_h(\kappa)$ in terms of κ . A practical way to achieve this goal consist is finding an implicit definition for $\omega_h(\kappa)$ in terms of $\cos(h\kappa)$. For example, for the case of elements of the first order, relation (30) can be rewritten as

$$\cos(h\kappa) = \frac{6 - 2(h\omega_h)^2}{6 + (h\omega_h)^2}, \quad (40)$$

This expression is generalized to arbitrary orders of p in the following theorem, presented by Ainsworth (2003).

Teorema 4.1 *Let $[2N_e + 2/2N_e]_{\kappa \tan(\kappa)}$ and let $[2N_o/2N_o - 2]_{\kappa \cot(\kappa)}$ be the notations for the Pad approximation of $\kappa \tan(\kappa)$ and $\kappa \cot(\kappa)$, respectively, where $N_e = \lfloor p/2 \rfloor$ and $N_o = \lfloor (p+1)/2 \rfloor$. Thus, ω_{hp} satisfies $\cos(h\kappa) \approx R_p(h\omega_{hp})$, where R_p is a rational function*

$$R_p(2\kappa) = \frac{[2N_o/2N_o - 2]_{\kappa \cot(\kappa)} - [2N_e + 2/2N_e]_{\kappa \tan(\kappa)}}{[2N_o/2N_o - 2]_{\kappa \cot(\kappa)} + [2N_e + 2/2N_e]_{\kappa \tan(\kappa)}} \quad (41)$$

where $\lfloor x \rfloor = \max\{m \in \mathbb{Z}; m \leq x \in \mathbb{R}\}$.

According to Theorem 4.1 expressions that represent the approximation $\cos(h\kappa) \approx R_p(h\omega_{hp})$ for $p = 1$ and $p = 2$ are, respectively

$$\cos(h\kappa) = \frac{6 - 2(h\omega_{h1}(\kappa))^2}{6 + (h\omega_{h1}(\kappa))^2} \quad (42)$$

and

$$\cos(h\kappa) = \frac{3(h\omega_{h2}(\kappa))^4 - 104(h\omega_{h2}(\kappa))^2 + 240}{(h\omega_{h2}(\kappa))^4 + 16(h\omega_{h2}(\kappa))^2 + 240} \quad (43)$$

5 Parameter selection for mesh

Now the theory developed in the two previous sections is used to establish a criterion for selection of the mesh refinement parameter n for second order rectangular elements.

First, consider the speed of numerical phase as

$$C = \frac{\omega}{|\boldsymbol{\kappa}|}. \tag{44}$$

Second, to establish a connection with the numerical experiments carried out in Section 3, consider a wave vector with the same characteristics as that used in the approximation of the problem (11)-(12), i.e., $\boldsymbol{\kappa} = (\kappa, \kappa)$. Thus, note that $\omega^2 = 2\kappa^2 C^2$. On the other hand, equation (39) shows that $\omega^2 = 2\omega_h(\kappa)^2$, consequently

$$C = \frac{\omega_h(\kappa)}{\kappa}, \tag{45}$$

Considering the $\cos(h\kappa)$ approximations for $p = 1$ and $p = 2$, equations (42) and (43), respectively, the numerical phase velocity C can be written as a function of $h\kappa$, thus obtaining,

$$C = \frac{1}{h\kappa} \left(\frac{6(1 - \cos(h\kappa))}{2 + \cos(h\kappa)} \right)^{1/2} \quad \text{for } p = 1 \tag{46}$$

and

$$C = \frac{1}{h\kappa(6 - 2(\cos(h\kappa)))^{1/2}} \left[16\cos(h\kappa) + 104 + (\beta)^{1/2} \right]^{1/2} \quad \text{for } p = 2, \tag{47}$$

where $\beta = (16\cos(h\kappa) + 104)^2 - 960(\cos(h\kappa) - 3)(\cos(h\kappa) - 1)$.

However, from dispersion relation (10) of the continuous problem, the exact phase velocity is given by $c = 1$. For example, for $p = 2$, Figure 7(a) shows the exact phase velocity compared with the numerical phase velocity given by equation (47). Figure 7(b) presents a closer view of Figure 7(a), with $0 \leq h\kappa \leq 1$, from which it is possible to determine, for example, the minimum value of the parameter h so that the estimated phase velocity error is less than 0.01%. This is done simply by observing the point at which the velocity curve reaches the value 1.0001 (or $h\kappa \approx 0.62$).

Note that the wave vector in the numerical example was $\boldsymbol{\kappa} = 10\pi(1, 1)$, then by taking $\kappa = 10\pi$, has $h \approx \frac{0.62}{10\pi} \approx 0.01973 \approx \frac{1}{51}$. Consequently, for $n \geq 51$, the error between the approximated and exact phase velocity is less than 0.01%. The possible use of this approximation for mesh refinement is now evaluated through a convergence analysis.

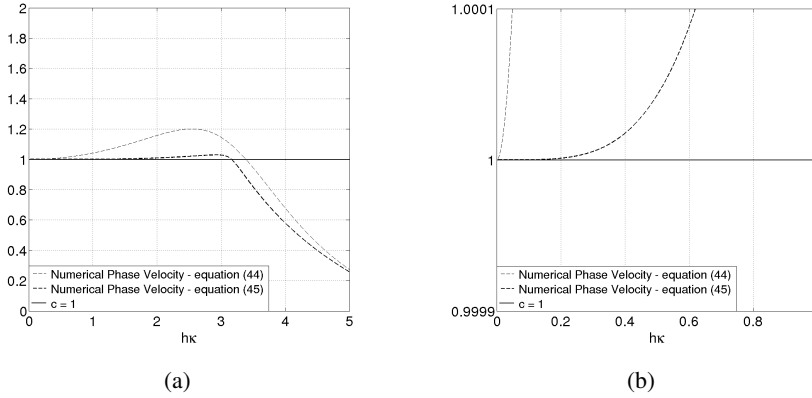


Figure 7: (a) Numerical phase velocity for first and second order elements; (b) Closer view of Figure 7(a).

5.1 Convergence analysis

Let d be the relative error in the phase velocity given by $|1 - C|$. Equation (46) is employed to show the phase velocity approximation for a fixed κ and an increasing n . This is shown in Figure 8(a) for three different κ values and, as expected, it is clear that improving the approximation for c requires smaller h values for larger frequency numbers. For convenience, it would be interesting to vali-

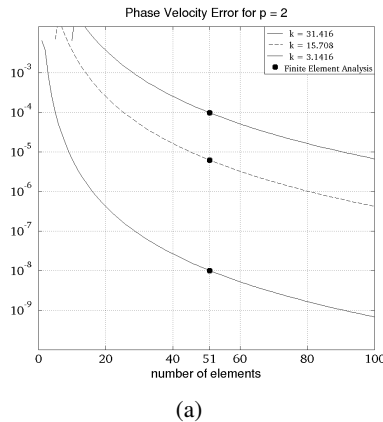


Figure 8: Phase Velocity approximation by Equation (47) with increasing discretization and FEM results for $n = 51$.

date the equation (27) for problems in two dimensions. To do so, it is assumed that $\boldsymbol{\kappa} = \kappa(\cos(\theta), \sin(\theta))$. Let $u_a \in H^1(\Omega)$ be defined by $u_a(\mathbf{x}) = \rho e^{i\frac{\omega}{c}[\cos(\theta)x_1 + \sin(\theta)x_2]}$. Note que u_a is an analytical solution of problem (11)-(12).

For calculation purposes let $\|\cdot\|$ be the norm for a real value function, defined by

$$\|u\| = \frac{\left(\sum_j |u(x_j)|^2\right)^{\frac{1}{2}}}{n^2} \quad \forall \mathbf{x} \in \Omega \tag{48}$$

Consider $u_h \in \mathcal{X}_{h2}$ the Finite Element numerical solution of problem (11)-(12), with 51 elements in the mesh discretization. By taking the same direction of propagation of the plane wave of the numerical experiment, i.e., $\theta = \frac{\pi}{4}$, one can define $u_{adj} \in H^1(\bar{\Omega})$ by

$$u_{adj}(\mathbf{x}) = \rho e^{i\frac{\sqrt{2}\omega}{2c_{adj}}[x_1+x_2]}, \tag{49}$$

that are analytics solutions within the range $0.9 < c_{adj} < 1.1$. Furthermore, we consider the analytical solutions of diagonal points of the domain Ω , i.e., $x_1 = x_2$, are considered. The error norm $\|u_{adj} - u_h\|$ is shown in Figure 9(a), where can be noticed that the numerical result is better adjusted by an analytic expression with c_{adj} very close to 1. A closer view is shown in Figure 9(b) where it becomes clear that the numerical phase velocity error is in neighborhood $d < 0.01\%$, conforming the estimated result obtained from 7(b).

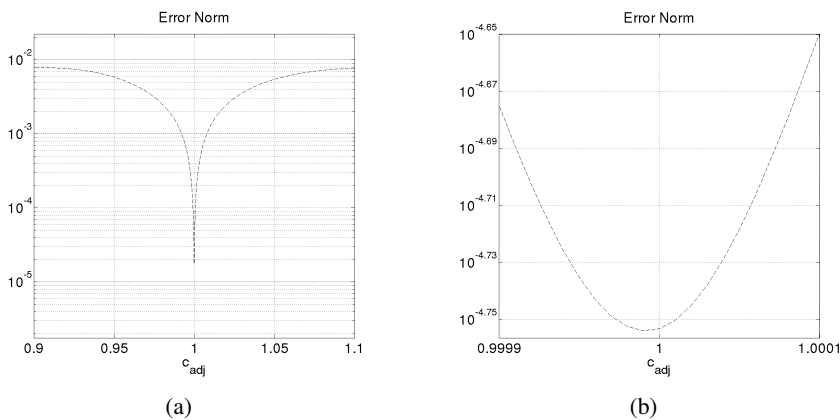


Figure 9: (a) Error norm with 51 elements in the mesh indicating the better adjust by analytic expression with c_{adj} very close to 1; (b) Closer view of Figure 9(a).

The same analysis can be made for the experiment involving cylindrical waves. In this version, u_{adj} is defined according to:

$$u_{adj} \left(\frac{\omega}{c_{adj}} r \right) = \frac{i}{4} h_0^{(1)} \left(\sqrt{2} \frac{\omega}{c_{adj}} r \right) \tag{50}$$

where r is the distance between any point on the diagonal of the domain $\Omega = [1, 1] \times [2, 2]$ and the point $(0,0)$. Figures 10(a) and 10(b) show the error norm reaching its lowest value, $\approx 10^{-7}$, also in the neighborhood $d < 0.01\%$ of $c_{adj} \approx 1$.

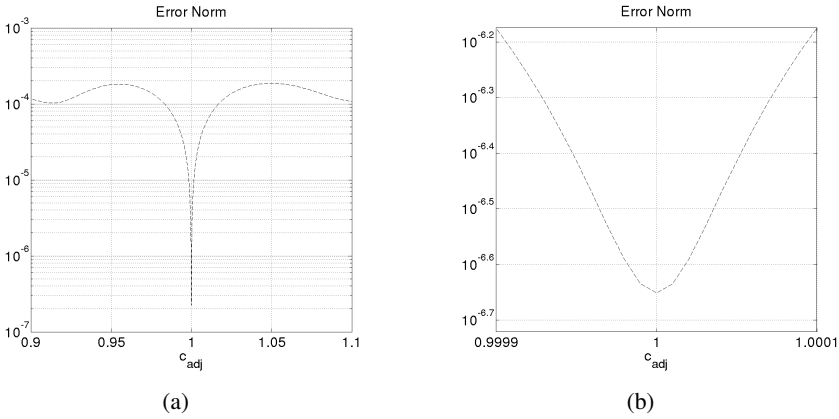


Figure 10: (a) Error norm with 51 elements in the mesh indicating the better adjust by analytic expression with c_{adj} very close to 1; (b) Closer view of Figure 10(a).

In both experiments, with plane and cylindrical waves, the correlation between the error in the numerical phase velocity and the error of the approximation by finite element is evident and shows that the phase velocity equations obtained from the discrete dispersion analysis may be used as error estimators in the FEM solution of the Helmholtz equation problems.

6 Conclusion

The use of Legendre hierarchical basis functions facilitate the computer implementation of the finite element method for solving Helmholtz equation problems. It is always possible to take advantage of the functions used in the approximation of order p in the numerical experiments of order $p + 1$. Solution approximations of a simple numerical problem with fixed wavenumber were presented, until fourth order, demonstrating the already known efficiency of the method.

From the variational formulation of the Helmholtz equation the already known expression of the discrete dispersion relation was presented for a finite element space of order $p = 1$. Such relation was reformulated with aid of Padé approximation and extended to spaces of elements of order $p = 2$. A direct link between the phase velocity, written as a function of the discrete dispersion relation, and the size of the elements used in domain discretization is shown for orders $p = 1$ and $p = 2$. Graphical interpretation of these equations clearly indicate the phase velocity error reduction with the increasing mesh refinement for several wavenumbers.

Finite element analyses were carried out and confirmed the validity of the developed phase velocity equations for $p = 1$ and $p = 2$. FEM results were fitted to obtain a numerical phase velocity and it was shown that the best fit was in perfect agreement with the error estimates derived from the phase velocity equation and the number of elements in the uniform discretization.

Error norms were evaluated in all FEM analysis and a strong correlation was observed with the phase velocity error in the analyzed problem. This evidence suggests that the numerical phase velocity defined from the discrete dispersion can be used as an error estimator in the approximation of the Helmholtz equation by the finite element method.

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