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ARTICLE

Comparative Study of Two Materials Combining a Standard Building Material with a PCM

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ABSTRACT

Phase change materials (PCMs) have the ability to store thermal energy and make it available at a later stage to keep indoor temperature within a specific range and achieve better thermal comfort in buildings. This study focuses on the performances of materials obtained by combining a standard building material with a PCM. In particular, two different materials mixed with the same PCM are considered under the same climatic conditions. The related thermal behavior is assessed in the framework of numerical simulations conducted with ANSYS Fluent assuming parameters representative of a city located in Europe. The results show that the addition of PCM to concrete and bricks can improve the thermal inertia of the resulting material.

KEYWORDS

Phase change materials; building material; thermal comfort; passive cooling

Nomenclature

| Н | Enthalpy [J/kg] |
|-------------------|--|
| λ | Thermal conductivity [W/(m.K)] |
| Т | Temperature [K] |
| ρ | Density [kg/m ³] |
| Cp | Specific heat capacity [J/(kg.K)] |
| C _{app.} | Apparent specific heat capacity [J/(kg.K)] |
| L | Latent heat [kJ/kg] |
| t | Time [s] |
| Tout | Outside temperature [K] |
| T _{in} | Inside temperature [K] |
| h | Convective heat transfer coefficient $[W/(m^2.K)]$ |



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1 Introduction

In recent years, the building industry has accounted for the largest share of energy overconsumption, and interest in this sector is growing. To cope with this overconsumption of energy, several suitable methods are applied in the building sector to reduce energy consumption. The main challenge of tomorrow's building is to avoid passive cooling and heating systems. One of the solutions is the integration of smart materials in the building walls.

Several researches have studied the addition of phase change materials: a material having the capacity to store energy during the day and to restore it during the night in order to smooth the temperature fluctuations in case of overheating and specially to limit the summer discomfort. This new solution has the advantage of limiting the energy consumed by the various equipment intended for the comfort of the habitat. These materials can be integrated or combined with other construction materials such as plaster or gypsum [1-3], concrete [4-6] and other matrices [7,8]. However, studies comparing solutions in combination with concrete and brick remain rare in the literature.

The objective of this paper is to compare the same PCM with two ubiquitous building materials in construction: brick and concrete, and to evaluate their influence on temperature distribution and their impact on the reduction of internal wall temperature through numerical modeling. The numerical simulation was solved with the finite volume method integrated in the commercial software Ansys Fluent.

2 The Case Studies

Two different materials are chosen with the same PCM under the same climatic conditions: brick and concrete with the PCM Energain manufactured by DuPont.

The thermo-physical properties of PCM wallboard [9], concrete and brick [10] are listed in Tables 1 and 2.

| Thermo-physical property | Value |
|--|-------|
| Density (kg/m ³) | 900 |
| Thermal conductivity in solid phase (W(/m.K)) | 0.18 |
| Thermal conductivity in liquid phase (W/(m.K)) | 0.22 |
| Melting point (°C) | 22.3 |
| Freezing point (°C) | 17.8 |
| Specific heat capacity of the solid phase (J/(g.K)) | 12.9 |
| Specific heat capacity of the liquid phase (J/(g.K)) | 13.4 |
| Latent heat in solid phase (J/g) | 71 |
| Latent heat in liquid phase (J/g) | 72.4 |

 Table 1: Thermo-physical properties of PCM [9]

Table 2: Thermo-physical properties of building materials [10]

| Material | Thermal conductivity (W/(m.K)) | Density (kg/m ³) | Heat capacity (kJ/(kg.K)) |
|----------------|--------------------------------|------------------------------|---------------------------|
| Heavy concrete | 1.75 | 2300 | 0.92 |
| Brick | 1.15 | 1700 | 0.794 |

The effect of placement in a multi-layer wall of a PCM composite wall panel has been studied previously which showed that there is an optimized location for placement of PCM in building envelope surfaces based on its effectiveness on interior temperature control: Externally located composite PCM wall panels performed better than internally located composite PCM panels in multilayer wall systems during cooling seasons.

In this study, the PCM panel is used in the outside of the wall. From exterior to interior, the wall layer is the PCM panel of 5.3 mm thickness, followed by the building material layer (concrete or brick) with the thickness of 15 cm.

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The model is described in Fig. 1 and has been validated by comparison with an analytical solution and a numerical study [11]. Two types of boundary conditions were imposed on the inner wall: Dirichlet-type condition (Case 1) and natural convection condition (Case 2) shown in Table 3. The assumptions made to simplify the equation are listed below:

- The flow is considered laminar.
- The material is pure and homogeneous.
- Heat transfer through the wall is one-dimensional in unsteady regime.
- Integration of conduction regime.
- All other heat transfer phenomena are neglected.
- The horizontal walls are considered in adiabatic conditions.
- The thermal conduction follows the Fourier law: $q = -\lambda \partial T / \partial x$.



Figure 1: Schematic representation of the wall

(4)

| Specific case | Outdoor temperature (K) | Indoor temperature (K) |
|-------------------|------------------------------|------------------------|
| Case 1: Dirichlet | Summer day | $h = 4 W/(m^2.K)$ |
| | | $T_{in}(t) = 293.15$ |
| Case 2: | $h_o = 16 \text{ W/(m^2.K)}$ | $h_i = 4 W/(m^2.K)$ |
| Natural | Summer day | $T_{in}(t) = 293.15$ |
| convection | | |

 Table 3: Different cases of modeling [12]

The general energy conservation equation has been simplified with the apparent C_p method as follows (1):

$$\rho(T)C_{app}(T)\frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(\lambda(T)\frac{\partial T}{\partial x}\right)$$
(1)

With C_{app}, the apparent specific heat capacity in J/(kg.K).

For the phase change phenomenon, L representing the latent heat is taken into account as below:

Solid phase :
$$C_{app} = Cp_s(T)$$
 (2)

Mixing zone :
$$C_{app} = \frac{1}{2} \left(\overline{Cp_s} + \overline{Cp_l} \right) + \frac{dL(T)}{dT}$$
 (3)

Liquid phase : $C_{app} = Cp_l(T)$

With $\overline{Cp_l}$, and $\overline{Cp_s}$ are respectively the average of specific heat capacity of the liquid phase and the solid phase.

The imposed temperature is a sinusoidal approximation to simulate the real temperatures, in order to define the hottest days during the hot season in Paris, which represents the peak of summer discomfort for residents, during 24 h (a day) [8]:

$$T_{out}(t) = 296 + 6\sin(\omega t) \tag{5}$$

With the time *t* in seconds.

3 Results and Interpretations

Please note that the results were evaluated at the surface of the wall with/without the PCM.

Case 1:

Fig. 2 shows the surface temperature distribution in the concrete wall and the PCM/concrete. It was noted that compared to the reference wall, the bilayer with the presence of the PCM layer has lower temperatures. The surface temperature distribution within the brick wall and the PCM/brick wall at t = 12 h is shown in Fig. 2. Low temperatures can be observed locally, due to the addition of a PCM plate to the brick.

Fig. 3 illustrates the evolution of the surface temperature of the two walls by 24 h. It can be seen that a significant result is obtained in terms of temperature reduction. In comparison with the reference concrete, the temperature of PCM/concrete can be reduced by 1.5 K. In addition, a phase shift of the order of 2 h between the two peaks of the two walls is observed.



Figure 2: Temperature distribution within the concrete wall of concrete (a), PCM/concrete (b), wall of brick (c) and PCM/brick (d)



Figure 3: Evolution of the surface temperature of the concrete and brick wall with and without PCM

This figure presents also the evolution of the surface temperature of brick with and without PCM. A temperature reduction of 0.8 K was measured on the wall with phase change materials compared to the brick without PCM. A phase shift of 2 h between the two temperature peaks was noted.

In this case, we can observe that the amplitudes of the oscillations were greatly affected for the wall including the panel of PCM. It can be noted that the PCM/concrete have the ability to keep the wall temperature cooler than the PCM/Brick and to reduce the surface temperature of the wall more efficiently.

Case 2:

The surface temperature distribution within the concrete wall and the PCM /concrete wall at t = 12 h is shown in Fig. 4. Very low temperatures can be observed locally, due to the addition of a PCM to the reference concrete.



Figure 4: Temperature distribution within the concrete wall (a), PCM/concrete (b), wall of brick (c) and PCM/brick (d)

For the case of the brick, the presence of the isothermal lines show lower temperatures at the wall with PCM.

Fig. 5 illustrates the evolution of the surface temperature of the concrete wall and the PCM/concrete. There is a significant difference between the wall with and without PCM in terms of reduction of temperature fluctuations. Indeed, there is a drop in the internal wall temperature of about 1.5 K recorded, with a phase shift noted between the two temperature peaks of 2 h. We can underline that the wall temperature with brick and PCM is slightly lower than the reference wall temperature. Indeed, a maximum drop of 0.8 K was noted at temperature after a calculation time of about 16.5 h. It was also observed a phase shift of temperature peaks of 2 h.



Figure 5: Evolution of the surface temperature of the concrete and brick wall with and without PCM

The results of the two building materials with PCM allows us to highlight the difference in temperature fluctuations between the wall with and without phase change materials in the case of brick and concrete. Both materials show significant results with the integration of the panel with PCM.

By contrast, it can be clearly seen that the concrete has a better influence on the temperature distribution than Brick due their thermal properties.

It can be seen that the PCM plays the role of an insulator at t = 12 h for all cases since it is in the liquid state, which means that it is in the energy storage phase.

Moreover, for all cases, it is observed that the amplitudes of the oscillations were greatly affected for the wall including the panel with phase change materials. This result was therefore put forward by determining the decrement factor for each case, which is a ratio between the two values of the amplitudes to that of the reference wall and that of the wall with PCM. The final aim is to improve the thermal comfort of a room. The lower this value, the lower the thermal amplitude compared to the reference wall and the more the wall has optimized and isolated the interior temperatures.

The Table 4 below illustrates the difference in amplitudes for each case, its decrement factor and the phase shift between the wall with and without PCM. It can be seen that better damping was achieved in the concrete case with the addition of a single panel of phase change material.

| | | Case 1 | | | | |
|----------|---------------------------------|---------------------------|------------------|------------------------|--|--|
| | Amplitude of the reference wall | Amplitude of the PCM wall | Decrement factor | Phase shift ϕ (h) | | |
| Concrete | 6.3 | 3.6 | 0.6 | 2 | | |
| Brick | 5.9 | 4.2 | 0.7 | 2 | | |
| Case 2 | | | | | | |
| Concrete | 2.5 | 1.4 | 0.6 | 2 | | |
| Brick | 3.3 | 2 | 0.6 | 2 | | |

Table 4: The amplitude, the decrement factor and the phase shift of the different cases

4 Conclusion

This paper presents a numerical study to solve one dimensional transient heat transfer through the bilayer surfaces of the building envelope. The aim is to compare two building materials with the same phase change material whose phase change temperatures are well suited to the Parisian climate.

The addition of the PCM panel showed a different behavior between the two materials due to their thermal properties. The results reveal an interesting and significant potential in terms of temperature reduction within the wall. In addition, a phase shift of temperature peaks was recorded, resulting in a good thermal inertia when integrating the PCM plate.

On one hand, this comparative study showed the influence of a phase change material on the reduction of the temperature of a wall and on the improvement of the thermal inertia. On the other hand, it was found that the construction material also plays a major role in the results obtained. This highlights the importance of choosing the best combination: PCM and the building material.

In perspectives, further studies must be carried out to evaluate other types of PCM with these building materials while getting as close as possible to the real case.

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