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ARTICLE

Experimental Investigation of Performance Characteristics of PZT-5A with Application to Fault Diagnosis

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ABSTRACT

In the previous couple of decades, techniques to reap energy and empower low voltage electronic devices have received outstanding attention. Most of the methods based on the piezoelectric effect to harvest the energy from ambient vibrations have been revolutionized. There's an absence of experiment-based investigation which incorporates the microstructure analysis and crystal morphology of those energy harvest home materials. Moreover, the impact of variable mechanical and thermal load conditions has seldom been studied within the previous literature to utilize the effectiveness of those materials in several practical applications like structural health monitoring (SHM), etc. In the proposed research work, scanning electron microscope (SEM) and energy dispersive x-ray (EDX) analysis are performed to examine the inside crystal morphology of PZT-5A and ensure the quality of the piezoelectric ceramic. Further, the performance of piezoelectric vibration-based energy harvester has been investigated in the second phase of current research work under the variable mechanical and thermal load conditions through a regular series of experiments. It's been found that the output voltage of piezoelectric sensors will increase by increasing the applied load, whereas a decreasing trend in output voltage is noticed by increasing the applied temperature, resistance and frequency. Within the third part, a measuring setup is developed in the laboratory to further investigate the effectiveness of PZT-5A in practical applications such as electromechanical impedance (EMI) based structural health monitoring under the controlled heating environment. Therefore, this analysis not only evaluates the performance of PZT sensors under the variable operating conditions but also encourages developing a temperature compensation approach in EMI-based SHM.

KEYWORDS

Piezoelectric energy harvester; crystal morphology; scanning electron microscope; structural health monitoring; electromechanical impedance



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1 Introduction

Piezoelectric energy harvesters have the capability to convert the strain energy that is generated by some external source into electrical energy and in a similar way these materials change the electric potential into mechanical energy because of their crystalline structure [1]. This distinguished aspect of these materials enables them to absorb the ambient vibrations available in the surrounding in the form of mechanical energy. This mechanical energy is converted into an electrical charge that is used to empower the low voltage electronic devices [2]. There are also some alternative methods to extract the energy besides piezoelectric energy harvesters such as the magnetic force device method. Piezoelectric materials are considered a better choice for some practical applications because of their usefulness as compared to other energy harvesting techniques. These energy harvesters can be adjusted into many microelectromechanical systems (MEMS) due to their small dimensions. Moreover, the working capability of the system can be enhanced when the external parameters like temperature and load are within the suitable limit of piezoelectric energy harvesters. The mechanical potential that is required for the transformation is obtained from the surrounding. Despite possessing ideal specifications, however, piezoelectric materials have not earned so much attention in the field of energy scavenging because of the small output voltage. Piezoelectric energy harvesters are adaptable because most of the dynamic systems are based on the phenomenon of vibration. These piezoelectric energy harvesters have low noise and a broad dynamic range [3-5]. These vibrations based piezoelectric energy harvesters are classified into thirty-two types. There are twenty piezoelectric crystals that show a direct piezoelectric effect [6]. The most famous piezoelectric materials are Lead Zirconate Titanate, Barium Titanate, Lithium Tantalite, Lead Potassium Niobate and Sodium Tungstate. The research conducted in 2014 revealed that piezoelectric materials that were developed through circular arrays produce output voltage over the wide range of frequency and load resistance [7]. It has been observed that the resonance frequency has a negative impact on the output voltage of the piezoelectric specimen [8]. The temperature has a significant impact on the performance of piezoelectric materials in many practical applications. Many piezoelectric properties are temperature-dependent and these properties play a vital role in the performance of piezoelectric energy harvesters [9]. Since the output voltage obtained from piezoelectric material is minute, so this voltage is rectified and regulated to charge the batteries [10,11]. Experimental research on piezoelectric materials has revealed that these materials show non-linear response when subjected to the large electric field. This non-linearity has a vital role in the design stage of piezoelectric devices [12]. The concept of functionally graded piezoelectric materials has been introduced to enhance the performance of conventional piezoelectric materials [13]. As described earlier that these materials have small dimensions so they are fitted into any electronic system without affecting its stability [14]. Considering the limitations of other types of sensors, structural health-monitoring systems based on embedded PZTs are now widely used in real-time inspections. These surface-bonded piezoelectric ceramics can perform the function of both actuator and sensor simultaneously. Because of small size, light in weight and high sensing capability, PZTs have a significant role in ultrasonic guided wave inspections. PZT sensors have less impact on the host structure and they are considered more suitable for the integration of health monitoring systems than any other type of sensors. However, to inspect the large surface area, a sensor network is required consists of multiple PZT sensors. The main benefit of such type of sensors' arrangement is that there exists no difficulty of extracting echo signals. However, all the configurations of PZT sensor networks contain the definite number of sensors. It will not only significantly increase the monitoring cost, but also makes the maintenance work of a large number of sensors more complicated. These two major challenges reduce the practical implementation of PZT sensor networks for the inspection of large surface areas and complex structures. These materials have high polarization rates under the applied vibrating load conditions and as a result, the electric potential is increased [15]. Piezoelectric materials have been applied in electromechanical devices as sensors and actuators. These materials contain many microscopic crystal grains and domains. Because of their asymmetrical crystal structures, such as cubic, tetragonal, and rhombohedran, all domains

display anisotropic mechanical and electrical behaviors, and the macroscopic properties of these materials rely heavily on this microscopic crystal morphology. Therefore, it is essential to study the microstructural characteristics of these polycrystalline materials using SEM and EDX [16]. Scanning electron microscopes use concentrated beams of electrons that by interacting with materials at their atomic levels produce signals regarding the materials' surface composition and topography to generate microscopic images [17]. Clarification of the current environmental sources of variations is also essential to enhance the reliability of other damage inspection techniques, such electromechanical impedance (EMI), etc. [18–23]. The piezoelectric energy harvesters have limited practical applications, so advanced scientific research is essential in this field to investigate their characteristics.

This research work aims to investigate the performance characteristics of PZT-5A under variable mechanical and thermal loading conditions. Firstly, to examine the inside crystal morphology of PZT-5A and ensure the quality of the piezoelectric ceramics, the scanning of electron microscope (SEM) and energy dispersive x-ray (EDX) analysis are carried out. Further, the performance of piezoelectric vibration-based energy harvester has been investigated in the second phase of current research work under the variable mechanical and thermal load conditions through a regular series of experiments. In the next phase, a calculation arrangement is developed to inspect the effectiveness of PZT-5A in electromechanical impedance (EMI) under the controlled conditions.

The research work is arranged into the following sections. Section 2 will cover experimental test procedure and research methodology including material selection. In Section 3, results are discussed in detail. Section 4 will represents the conclusions of the experimental investigation.

2 Research Methodology

2.1 Material Selection

Lead Zirconate Titanate is selected in the current research due to its high strain constants, coupling constants, permittivity and high Curie temperature [24,25]. The following equations are derived through the Gibbs free energy:

$$D_m = d_{m\beta}^{H,\theta} T_\beta + \varepsilon_{mk}^{T,H,\theta} E_k + m_{mk}^{T,\theta} H_k + p_m^{T,H} d\theta$$
⁽¹⁾

$$S_{\alpha} = s_{\alpha\beta}^{E,H,\theta} T_{\beta} + d_{\beta m}^{H,\theta} E_m + d_{\beta m}^{E,\theta} H_m + \alpha_{\alpha}^{E,H} d\theta$$
⁽²⁾

where d_{mb} and $d_{\beta m}$ represent the piezoelectric constants, H_k and H_m are termed as magnetic field components, m_{mk} exhibits the magneto-dielectric constants, θ shows the temperature, p_m illustrates the pyroelectric constants, α_{α} depicts the thermal expansion coefficients, T_{β} exhibits the mechanical stress tensor, and S_{α} represents the mechanical strain tensor.

Suppose the influence of the temperature and the magnetic field is neglected, Eqs. (1) and (2) can be written as:

$$D_m = d_{m\beta}T_\beta + \varepsilon_{mk}^I E_k \tag{3}$$

$$S_{\alpha} = s^{E}_{\alpha\beta}T_{\beta} + d_{\beta m}E_{m} \tag{4}$$

Eq. (5) elaborates the electrical impedance of sensor [26]:

$$Z_{E}(\omega) = \frac{1}{j\omega C_{0}} \|jZ_{T}\left(\frac{s_{11}}{d_{31}l}\right)^{2} \left[\frac{1}{2}\tan\left(\frac{kl}{2}\right) - \frac{1}{\sin(kl)} + \frac{Z_{s}}{j2Z_{T}}\right]$$
(5)

2.2 Microstructure and Crystal Morphology

To verify the elemental composition of the specimen, the morphological investigation of polycrystalline PZT has been carried out using a scanning electron microscope (SEM) operating at 20.0 KV as shown in Fig. 1.



Figure 1: SEM for morphological investigation of PZT sample

The specimen was initially electrically poled in the thickness direction and then cracked with a thin gold layer in the evaporator to charge the electron before scanning. Fig. 2 shows the microstructure of piezoelectric material (PZT-5A). It can be analyzed that the crystal grains are non-uniformly distributed and agglomerated with the large particles all over the substrate.



Figure 2: Crystal morphology of PZT-5A

Energy-Dispersive X-ray analysis (EDX) was also done to verify the elemental percentage of the sample at multiple selected spots. Fig. 3 shows the four spectrums on the PZT-5A sample with the grain size 5 μ m to evaluate the material composition.



Figure 3: Electron image of PZT-5A with grain size 5 µm

Fig. 4 reveals the elemental composition of the PZT-5A in spectrum 4. It can be noticed that there are no impurities found in the specimen and the EDX shows a clear peak of all elements. Hence the EDX analysis depicts the purity of PZT-5A used for current research work.



Figure 4: The weight percentage of elements in PZT-5A in spectrum 4

2.3 Experiment Testing Procedure

The experimental setup consists of a load cell to determine the connection between frequency and peak to peak DC output voltage at different loading parameters. Surfaces of the piezoelectric specimen are covered with copper electrodes because these electrodes generate extremely low magnetic permeability and can be operated over a wide range of temperature. The specimen is fitted on a load cell in such a sequence that copper electrodes appear on their top and bottom surfaces. Loading conditions are provided by a 100 N electro-mechanical shaker which is well suited for applications with small strokes and high forces. A function generator is used to adjust the frequency of sinusoidal voltage and electrically shock the piezoelectric specimen. To examine the effect of temperature on the specimen, a heater is placed in an

insulating temperature chamber to change the room temperature up to the required high-temperature condition. Particular resistance is provided by two crocodile probes which are connected in series through a decade resistor. To measure peak DC voltage, the electrodes are connected to a digital oscilloscope. The output voltage is analyzed on a digital oscilloscope. The investigational equipment is demonstrated in Fig. 5.



Figure 5: Investigational test setup

Fig. 6 shows the 100 N electromagnetic shaker of model JZK-10 used in the current experimental setup. It consists of a small vibration table, connecting rod, mounting screws and power cable. It can compute the powerful reaction, regular recurrence and mechanical impedance for medium and enormous size structures at a wide recurrence range. Its performance parameters are described in Table 1.



Figure 6: 100 N electromagnetic shaker

Table 1: Performance parameters of 100 N electromagnetic shaker of model JZK-10

Performance parameter	Range
Maximum force output	100 N
Vibration amplitude	-5 to $+5$ mm
Max. Acceleration	280 ms^{-2}

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In the next phase, a standardized measurement setup is developed in the laboratory to further investigate the effectiveness of PZT-5A in EMI based structural health monitoring or (SHM) under the controlled heating environment. The wide-ranging laboratory equipment is demonstrated in Fig. 7.



Figure 7: Laboratory equipment

Some significant aspects of the electric thermostatic drying oven chamber are following:

- Elegant design and easy handling;
- Digital temperature controller;
- Stainless steel heating structure and internal shelves;
- Air exhaust mechanism at the top surface;
- Uniform temperature distribution.

The following steps should be performed to operate this chamber:

- 1. The box should be placed horizontally on a dry work surface in the laboratory.
- 2. After turning on the electrical power supply, first, check the electrical performance of the box, and pay attention to whether there are open circuits or short circuits.
- 3. In the next step, the heating switch is turned on immediately, and the temperature regulator knob is turned clockwise from the "0" position to the "10" index. At this time, the temperature inside the box starts to rise and the heating indicator lights up.
- 4. When the temperature has risen to the required working condition (it can be observed on the thermometer inserted into the vent hole), immediately turn the temperature regulator knob counterclockwise until the heating indicator stops lightening, and then adjust it to light up the heating indicator again. Repeat this adjustment setting at least two to three times till the constant temperature of the box is achieved. If the thermometer shows that the temperature is still rising during the initial stage of the constant temperature, it is caused by the inertia of the working room's temperature. This phenomenon will be stabilized within half an hour. If the thermometer reading exceeds or falls below the required temperature value, the temperature regulator can be adjusted slightly as described before to achieve the desired temperature.

A beam is shown in Fig. 8 with a slight evident fatigue crack of 10 mm and the bonded location of the PZT sensors.

To generate the electrical waveforms, an arbitrary function generator is recognized as a significant part of an electronic test setup. Depending on the application, these waveforms are generated in different shapes such as single-shot or repetitive. The required waveform is passed through the examined specimen and analyzed as it propagates to identify the structural abnormality. By utilizing the voltage-controlled oscillator, such kind of function generators is capable of automatically adjusting the frequency of the output signal. This characteristic is very useful to estimate the frequency response of the developed electronic test setup. The practical applications of the function generator are electronic test, sensor simulation and functional test.



Figure 8: Beam geometry with the exact location of bonded PZTs

An amplifier is a type of electronic equipment which is usually used to boost up the amplitude of the applied signal. To this purpose, its electronic circuit consists of two-ports to receive the power supply for the signal provided to its input terminals and generate a comparatively greater amplitude signal at its output terminals. The range of signal amplification is estimated by its gain that is the ratio of the output voltage to the input voltage. It has the following practical applications:

- Piezoelectric transducer driving
- Meter calibrations
- Low distortion AC power source

To actuate the Hanning window and the amplification of the guided wave signal, an AFG3022B arbitrary/Function generator with an external amplifier (KROHN-HITE-7602M) was used in the current experimental series. To obtain the numerous measurements, the excitation signal was provided continuously while allowing the previous signal to disappear before the propagation of the next signal.

The schematic of these devices is shown in Fig. 9.



Figure 9: Measuring instruments to deal with signal behaviour

Key specifications of the amplifier (KROHN-HITE-7602M) are represented in Table 2.

Specification	Value	Unit
Output power	34	W
Output voltage	282	V rms
Frequency range	DC-1	MHz
Max. input voltage	200	V
Max. current	200	mA
Voltage gain	0-42	dB
Distortion	< 0.01	%
DC offset	±200	V

 Table 2: Key specifications of the amplifier (KROHN-HITE-7602M)

To graphically illustrate the fluctuating signal voltages, a specific kind of electronic test instrument named oscilloscope is utilized in the laboratory experiments. It transforms the sound or vibration signals into the voltages and then displays these signal voltages in the form of the two-dimensional plot as a function of time. On the graphical scale, it illustrates the variation of an electronic signal over time in terms of voltage on Y-axis and time on X-axis, respectively. The corresponding waveform signal is then interpreted to evaluate some significant properties such as frequency, time interval, amplitude, distortion, etc. In the earlier time, the real values of these properties were calculated manually by analyzing the signal waveforms against the scales set into the screen of the measuring device. In this research work, the digital phosphor oscilloscope named Tektronix DPO 3014 is used to save all the measured signals. Its key specifications are demonstrated in Table 3. It has several advanced analysis modules.

 Table 3: Key specifications of digital phosphor oscilloscope (Tektronix DPO 3014)

Specification	Value	Unit
Analog channels	4	
Analog bandwidth	100	MHz
Record length	5 M points	
Sample rate	2.5	GS/s

3 Results and Discussion

Experimental observations and obtained results are interpreted in this section.

3.1 Effect of Mechanical Loading Conditions

By applying the variable loading conditions on the specimen (PZT-5A), it has been analyzed that the maximum peak voltage of 2.9 V is obtained at the applied frequency and mechanical load of 2-5 Hz and 60 kN/m^2 , respectively. The results are shown in Fig. 10.

It has been found that the maximum peak voltages are obtained at high vibrating load and low-frequency conditions because the rate of polarization of PZT-5A increases at higher vibrating load conditions, while at low frequency there are excellent dielectric, piezoelectric and ferroelectric properties of the examined

specimen with less characteristic energy losses. So, piezoelectric materials are suitable for low-frequency range and high loading conditions.



Figure 10: Mechanical load vs. peak DC voltage

3.2 Effect of Thermal Loading Conditions

Fig. 11 shows that on increasing the temperature the output voltage decreases under operational vibrating loading conditions. In the current analysis, the maximum peak dc voltage of 4.78 V is measured at 120 kN/m² and 50°C. So, it can be deduced that the piezoelectric materials show good performance when the applied temperature is less than the Curie temperature of the material. Further increment in temperature causes the depolarization in the materials because the piezoelectric properties of materials are disturbed due to highly induced mechanical stresses.



Figure 11: Thermal load vs. peak DC voltage

3.3 Effect of Applied Resistance

To evaluate the effect of the resistance on PZT-5A at constant room temperature 25°C by varying the frequency from 30 to 120 Hz, an experiment is conducted and results are shown in Fig. 12.

In Fig. 11, we can assume that the output voltage decreases by increasing the value of resistance at a constant temperature as the rate of polling decreases at higher resistance values. According to analysis, the minimum output voltage of 3.2 V is obtained at the applied frequency and resistance of 120 Hz,

140 k Ω , respectively. The output voltage and power of PZT-5A are also examined at constant mechanical loading conditions and varying resistance, the results are shown in Fig. 13.



Figure 13: (a) Resistance vs. peak DC voltage (b) Resistance vs. Power

From Fig. 12, obviously the resultant voltage and power first increases and afterward diminishes with applied resistance. Extreme output voltage and power can be achieved at 100 k Ω resistance. At high resistance values, the rate of poling in piezoelectric material decreases and the mechanical quality factor also decreases which cause the reduction in the overall power of PZT-5A. Hence, piezoelectric materials exhibit optimum voltage and power at specific values of applied resistance and frequency.

3.4 Impact of Temperature on the Frequency Shifts

In addition, the normal frequency of the monitored structure is also affected by the temperature variations and its value declines [27]. The frequency shifts (Δf) at applied conditions have been calculated and demonstrated in Fig. 14.



Figure 14: The magnitude of frequency shifts under operational conditions

It can be noticed that the change in (Δf) is almost linear within the frequency range of 100 kHz, but its slope depends on the temperature variation. However, an obvious deviation in the normal trend of (Δf) can be observed when temperature and excitation frequency are increased over 130°C and 100 kHz, respectively.

Ailete 502 adhesive is utilized to fix the sensors on beam surface and its elastic properties are mentioned in [28]. Fig. 15 demonstrates the percentage of the sensor's bonding strength with temperature.



Figure 15: Percentage of sensor's bonding strength with temperature

It is pretty clear from Fig. 15 that the sensor's bonding strength is impacted after 130°C and turns out to be practically 60% at 180°C. Therefore, the execution of an appropriate temperature recompense procedure is essential to control the impedance signature of PZT sensors. Moreover, the effect of damping is not considered in current research because the ultrasonic guided wave has a low attenuation rate towards the

damping phenomenon. The author has only analyzed the guided wave signals with tens of microseconds which have not occurred to attenuation because of damping under the operating conditions.

4 Conclusions

In the proposed research, thermal and mechanical analysis is performed for the piezoelectric energy harvester (PZT-5A) to examine its performance characteristics. The conclusions are as follows:

- 1. Microscopic analysis of piezoelectric energy harvester has indicated the heterogonous distribution of grains all over the substrate and the occurrence of certain agglomeration. Energy-dispersive X-ray (EDX) results have revealed that there are no impurities in the piezoelectric energy harvester.
- 2. In view of experimental results, piezoelectric materials exhibit maximum performance when subjected to low frequency and peak vibrating load conditions. Hence, these materials are highly recommended for low frequency and maximum vibrating load applications.
- 3. Also, it has been investigated that the temperature and external resistance has a negative impact on the output voltage of piezoelectric energy harvesters.
- 4. The experiment outcomes have revealed that the dielectric constant (ε_{33}^T) leads to an inaccurate damage inspection because of significant temperature effect.
- 5. Hence, the current research has not only evaluated the performance characteristics of PZT-5A but also indicated its effectiveness in practical applications such as EMI-based SHM under varying environmental and operating conditions (EOCs). The proposed research recommends developing an optimized temperature compensation approach to omit the basic reasons for false fault diagnosis in EMI-based structural health monitoring.

The proposed research results can be implemented to different material components in complex configurations such as cylindrically shaped Aluminum material parts with alternative material properties and the multiple numbers of modes. The piezoelectric transducer's configuration adopted in the current study can be further improved in terms of specific angles or degrees between the inspected specimens and applied loading conditions. The measurement system can be upgraded to further enhance the practicality of the temperature compensation approach. There is still a need for its verification in real-time industries such as transportation, power plants and architectural applications.

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