

Temporal Stability Analysis of Magnetized Hybrid Nanofluid Propagating through an Unsteady Shrinking Sheet: Partial Slip Conditions

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Abstract: The unsteady magnetohydrodynamic (MHD) flow on a horizontal pre-able surface with hybrid nanoparticles in the presence of the first order velocity and thermal slip conditions are investigated. Alumina (Al_2O_3) and copper (Cu) are considered as hybrid nanoparticles that have been dispersed in water in order to make hybrid nanofluid ($Cu - Al_2O_3$ /water). The system of similarity equations is derived from the system of partial differential equations (PDEs) by using variables of similarity, and their solutions are gotten with shooting method in the Maple software. In certain ranges of unsteadiness and magnetic parameters, the presence of dual solutions can be found. Further, it is examined that layer separation is deferred due to the effect of the hybrid nanoparticles. Moreover, the capacity of the thermal enhancement of $Cu - Al_2O_3$ /water hybrid nanofluid is higher as compared to Al_2O_3 /water based nanofluid and enhancements in ϕ_{Cu} are caused to rise the fluid temperature in both solutions. In the last, solutions stability analyzes were also carried out and the first solution was found to be stable.

Keywords: $Cu - Al_2O_3/H_2O$; hybrid nanofluid; magnetic field; slip conditions; dual solutions

1 Introduction

The topic of research in various engineering and industrial fields, such as air-conditioning, microelectronic, and power generation is energy sustainability and the optimizations of thermal systems performance. For energy sustainability, an inventive variety in thermodynamics was important [1]. Throughout such engineering processes, the cooling systems operate on a fluid medium through a forced



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flux in the absence and presence of convective heat transfer. The thermal conductivity of the liquid is therefore worthwhile to be enhanced for a better engineering process. The nanofluid formation is created through scattering single nanoparticle into the normal fluids, for example, vegetable oil, glycol, water, or the combination of glycol with water. The nanoparticles can be classified as carbon (*CNTs*, *MWCNT*), metal oxides (Al_2O_3 , Fe_2O_3 , CuO), metal (*Cu*, *Ag*), and metal carbide and nitride. Many researchers dealt with the various kind of nanoparticle combinations for example metal oxides (Al_2O_3 , CuO), metals (*Al*, *Cu*, *Fe*), and semiconductors (SiO_2 , TiO_2) nanoparticles. The important references on nanofluid can be seen in the books of [2,3]. On the other hand, comprehensive review papers on the nanofluid were written by [4–12].

Recently, researchers introduced a new type of nanofluid, and they call it Hybrid nanofluid. Hybrid nanofluid helps the regular nanofluids to improve its thermal properties. It can be described as the hybrid nanofluid, which consists of two different kinds of nanoparticles together with new chemical and thermophysical properties that can improve the rate of heat transfer due to synergistic properties (see [13]). Esfe et al. [14] stated that the good heat transfer rate is gotten by hybridizing the small amount of the nanoparticles volume fraction in the base fluid. Yan et al. [15] stated that the rate of heat transfer of the hybridized nanofluid is more as compared to the normal water-based nanofluid during the examination of the $Cu-Al_2O_3$ /water nanofluid. They found ranges of the existence of multiple solutions and also performed stability analysis of the solutions. Lund et al. [16] examined the MHD flow of $Cu-Fe_3O_4/H_2O$ hybrid nanofluid over non-linear stretching and shrinking parameters in the presence of the joule heating. Two solutions were found, and an unstable solution was recognized by without doing stability analysis due to the existence of the singularity in the second solution. Further, Waini et al. [17] obtained two solutions during the examination of the hybrid nanofluid over vertical sheet embedded in a permeable medium. They claimed that the non-uniqueness of solutions depends on the ranges of the mixed convection parameter. Waini et al. [18] continued the problem of [19] for the hybrid nanofluid and successfully found dual solutions in the ranges of the unsteadiness parameter. Due to various practical applications of the unsteady flow, the research of [19] was also extended by the [20] for the nanofluid by using of the double phase model and successfully found the dual solutions. The same paper was also extended by the [21] for the MHD unsteady flow of the Casson type nanofluid with effects of the slip conditions and Stefan blowing and noticed that dual solutions are also possible for the accelerated surface. Further, Lund et al. [22] considered the revised model of [18,19] for the unsteady incompressible MHD flow of the hybrid nanofluid in the existence of thermal radiation effects. It is now clear the importance of the unsteady model for the practical point of view. In this paper, we also extended the work of [18] and [22] for the hybrid nanofluid in the absence of the viscous dissipation and thermal radiation effect. To date, numerous review publications are present in the literature on the synthesis and preparation and hybrid nanofluids, such as [23–30]. Besides, some significant research articles of hybrid nanofluids are also available in these references [31–38].

The main objective of the current article is, therefore, to extend the works of [18,22] of MHD flow of the hybrid nanofluid on a shrinking sheet with the effect of the magnetic field, velocity, and thermal slip conditions. The alumina (Al_2O_3) and copper (*Cu*) are known to be hybrid nanoparticles here. The nanoparticles are then dispersed in order to develop the hybrid nanofluid ($Cu - Al_2O_3$ /water). In order to validate the present results, current results are compared with the results of the previously published.

2 Mathematical Formulation

Let us take the MHD unsteady flow of $Cu - Al_2O_3$ /water hybrid nanofluid over the shrinking sheet. The coordinate system and the physical representation of the problem are shown in Fig. 1. Further, velocity and

thermal partial slip conditions are also taken into account where $v_w(x) = -\left(\frac{\partial c}{(1-\epsilon t)}\right)^{\frac{1}{2}}f(\eta)$ is the mass transfer. Besides, the flow is assumed to be subject to a transverse magnetic field $= \frac{B_0}{(1-\epsilon t)^{1/2}}$, where constant magnetic field is B_0 . The influence of B on the shrinking sheet is applied perpendicular (see Fig. 1). Tiwari and Das's model are expressed as follows based on the considered assumptions [18,22]:

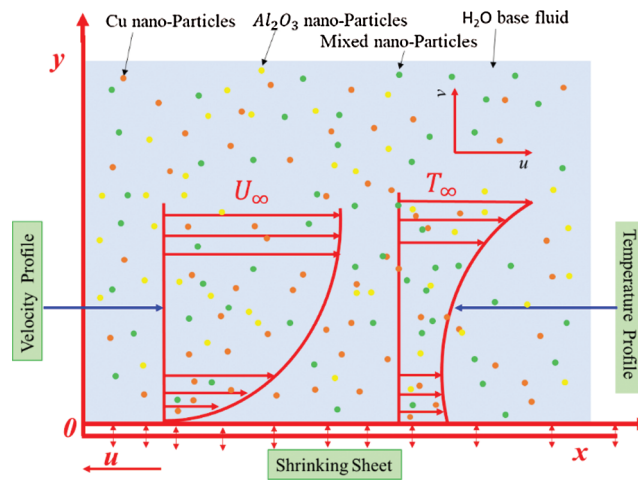


Figure 1: Physical models and coordinate systems

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{\mu_{hnf}}{\rho_{hnf}} \frac{\partial^2 u}{\partial y^2} - \frac{\sigma_{hnf}}{\rho_{hnf}} B^2 u \tag{2}$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{k_{hnf}}{(\rho c_p)_{hnf}} \frac{\partial^2 T}{\partial y^2} \tag{3}$$

The subject to boundary conditions [21]

$$\begin{cases} t < 0, u = v = 0, T = T_\infty \\ t \geq 0, v = v_w, u = u_w + N_1(x, t)v \frac{\partial u}{\partial y}, T = T_w + D_1(x, t) \frac{\partial T}{\partial y} \text{ at } y = 0 \\ u \rightarrow 0, T \rightarrow T_\infty \text{ as } y \rightarrow \infty \end{cases} \tag{4}$$

where velocity of surface is $u_w(x, t) = -\frac{cx}{(1-\epsilon t)}$. The thermophoresis property of Yan et al. [15] are followed in the present analysis.

Further, $N_1(x, t) = N_0\sqrt{1-\epsilon t}$ is velocity slip factor and $D_1(x, t) = D_0\sqrt{1-\epsilon t}$ is thermal slip factor where N_0 and D_0 are the slip factors. Tabs. 1 and 2 demonstrate these features of hybrid nanofluid.

We employ the following variable of similarity transformation to convert the Eqs. (1)–(3) into a system of ODEs.

Table 1: Thermophysical properties of hybrid nanofluid [22]

Properties	Hybrid nanofluid
Dynamic viscosity	$\mu_{hnf} = \frac{\mu_f}{(1 - \phi_{Al_2O_3})^{2.5} (1 - \phi_{Cu})^{2.5}}$
Density	$\rho_{hnf} = (1 - \phi_{Cu}) [(1 - \phi_{Al_2O_3}) \rho_f + \phi_{Al_2O_3} \rho_{Al_2O_3}] + \phi_{Cu} \rho_{Cu}$
Thermal conductivity	$k_{hnf} = \frac{k_{Cu} + 2k_{nf} - 2\phi_{Cu}(k_{nf} - k_{Cu})}{k_{Cu} + 2k_{nf} + \phi_{Cu}(k_{nf} - k_{Cu})} \times (k_{nf})$ where $k_{nf} = \frac{k_{Al_2O_3} + 2k_f - 2\phi_{Al_2O_3}(k_f - k_{Al_2O_3})}{k_{Al_2O_3} + 2k_f + \phi_{Al_2O_3}(k_f - k_{Al_2O_3})} \times (k_f)$
Heat capacity	$(\rho c_p)_{hnf} = (1 - \phi_{Cu}) [(1 - \phi_{Al_2O_3}) (\rho c_p)_f + \phi_{Al_2O_3} (\rho c_p)_{Al_2O_3}] + \phi_{Cu} (\rho c_p)_{Cu}$

Table 2: The thermo physical properties of the base fluid (water) and the nanoparticles [18,22]

Fluids	ρ (kg/m ³)	c_p (J/kg K)	k (W/m K)
Alumina (Al_2O_3)	3970	765	40
Copper (Cu)	8933	385	400
Water (H_2O)	997.1	4179	0.613

$$\eta = \left(\frac{c}{\vartheta(1 - \varepsilon t)} \right)^{\frac{1}{2}} y, u = \frac{cx}{(1 - \varepsilon t)} f'(\eta), v = - \left(\frac{\vartheta c}{(1 - \varepsilon t)} \right)^{\frac{1}{2}} f(\eta), \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty} \tag{5}$$

By applying Eq. (5) into Eqs. (1)–(3) then we have following non-dimensional form of ODEs

$$f''' + \xi_1 \xi_2 \{ff'' - f'^2 - A(0.5\eta f''' + f')\} - \xi_2 \frac{\sigma_{hnf}}{\sigma_f} Mf' = 0 \tag{6}$$

$$\frac{\xi_3}{Pr} (k_{hnf}/k_f)\theta'' + f\theta' - 0.5A\eta\theta' = 0 \tag{7}$$

Along with the boundary conditions

$$\begin{cases} f(0) = S, f'(0) = -1 + \delta f''(0), \theta(0) = 1 + \delta_T \theta'(0) \\ f'(\eta) \rightarrow 0, \theta(\eta) \rightarrow 0 \text{ as } \eta \rightarrow \infty \end{cases} \tag{8}$$

The non-dimensional quantities are given as $A = \frac{\varepsilon}{c}, M = M = \frac{\sigma_f B_0^2}{c \rho_f}, Pr = \frac{\vartheta_f}{\alpha_f}, \delta = (N_1)_0 \sqrt{c\vartheta}, \delta_T = (D_1)_0 \sqrt{\frac{\varepsilon}{\vartheta}}$.

$$\begin{cases} \xi_1 = \left\{ (1 - \phi_{Cu}) \left[1 - \phi_{Al_2O_3} + \phi_{Al_2O_3} \left(\frac{\rho_{Al_2O_3}}{\rho_f} \right) \right] + \phi_{Cu} \left(\frac{\rho_{Cu}}{\rho_f} \right) \right\} \\ \xi_2 = (1 - \phi_{Cu})^{2.5} (1 - \phi_{Al_2O_3})^{2.5} \\ \xi_3 = \frac{1}{\left\{ (1 - \phi_{Cu}) \left[1 - \phi_{Al_2O_3} + \phi_{Al_2O_3} \frac{(\rho c_p)_{Al_2O_3}}{(\rho c_p)_f} \right] + \phi_{Cu} \frac{(\rho c_p)_{Cu}}{(\rho c_p)_f} \right\}} \end{cases} \tag{9}$$

The coefficient of skin friction C_f and local Nusselt number Nu_x are given as

$$C_f = \frac{\mu_{hnf}}{\rho_f u_w^2} \left(\frac{\partial u}{\partial y} \right) \Big|_{y=0}, \quad Nu_x = -\frac{xk_{hnf}}{k_f(T_w - T_\infty)} \left(\frac{\partial T}{\partial y} \right) \Big|_{y=0} \tag{10}$$

By employing Eq. (9) in Eq. (10), we get

$$\sqrt{Re}C_f = \frac{1}{(1 - \phi_{Al_2O_3})^{2.5}(1 - \phi_{Cu})^{2.5}} f''(0); \quad \sqrt{\frac{1}{Re}}Nu_x = -\frac{k_{hnf}}{k_f} \theta'(0) \tag{11}$$

where Re is local Reynold number.

3 Stability Analysis

Merkin et al. [39–43] suggested for the stability analysis that the new non-dimensional variables of similarity transformation need to be introduced by considering $\tau = \frac{ct}{(1 - \epsilon t)}$, therefore, following new similarity transformation variables are introduced.

$$\begin{cases} u = \frac{cx}{(1 - \epsilon t)} \frac{\partial f(\eta, \tau)}{\partial \eta}, v = -\left(\frac{\vartheta c}{(1 - \epsilon t)} \right)^{\frac{1}{2}} f(\eta, \tau), \theta(\eta, \tau) = \frac{T - T_\infty}{T_w - T_\infty} \\ \eta = \left(\frac{c}{\vartheta(1 - \epsilon t)} \right)^{\frac{1}{2}} y; \tau = \frac{ct}{(1 - \gamma t)} \end{cases} \tag{12}$$

By putting Eq. (12) in Eqs. (2) and (3), we get

$$\frac{\partial^3 f}{\partial \eta^3} + \xi_1 \xi_2 \left\{ f \frac{\partial^2 f}{\partial \eta^2} - \left(\frac{\partial f}{\partial \eta} \right)^2 - A \left(0.5\eta \frac{\partial^2 f}{\partial \eta^2} + \frac{\partial f}{\partial \eta} \right) - (1 + A\tau) \frac{\partial^2 f}{\partial \tau \partial \eta} \right\} - \xi_2 \frac{\sigma_{hnf}}{\sigma_f} M \frac{\partial f}{\partial \eta} = 0 \tag{13}$$

$$\frac{\xi_3}{Pr} (k_{hnf}/k_f) \frac{\partial^2 \theta}{\partial \eta^2} + f \frac{\partial \theta}{\partial \eta} - 0.5A\eta \frac{\partial \theta}{\partial \eta} - (1 + A\tau) \frac{\partial \theta}{\partial \tau} = 0 \tag{14}$$

Along with boundary conditions

$$\begin{cases} f(0, \tau) = S, \frac{\partial f(0, \tau)}{\partial \eta} = -1 + \delta \frac{\partial^2 f(0, \tau)}{\partial \eta^2}, \theta(0, \tau) = 1 + \delta_T \frac{\partial \theta(0, \tau)}{\partial \eta} \\ \frac{\partial f(\eta, \tau)}{\partial \eta} = \theta(\eta, \tau) = 0 \text{ as } \eta \rightarrow \infty \end{cases} \tag{15}$$

According to Lund et al. [41], “to check the stability of steady flow solutions where $f(\eta) = f_0(\eta)$, and $\theta(\eta) = \theta_0(\eta)$ of satisfying the boundary value problem Eqs. (6)–(8)”, we have

$$\begin{cases} f(\eta, \tau) = f_0(\eta) + e^{-\gamma\tau} F(\eta, \tau) \\ \theta(\eta, \tau) = \theta_0(\eta) + e^{-\gamma\tau} G(\eta, \tau) \end{cases} \tag{16}$$

where $F(\eta)$ and $G(\eta)$ are relatively small to $f_0(\eta)$ and $\theta_0(\eta)$ and γ is called as unknown parameter of eigenvalue which need to be determined. Thus, we have the following linearized problems of eigenvalue, by replacing Eq. (16) in Eqs. (13) and (14) with $\tau = 0$.

$$F_0''' + \xi_1 \xi_2 \{f_0 F_0'' - 2f_0' F_0' + F_0 f_0'' - A(0.5\eta F_0'' + F_0') + F_0'\} - \xi_2 \frac{\sigma_{hnf}}{\sigma_f} M F_0' = 0 \quad e \tag{17}$$

$$\frac{\xi_3}{Pr} (k_{hnf}/k_f) G_0'' + f_0 G_0' + F_0 \theta_0' - 0.5\eta A G_0' + G_0 = 0 \tag{18}$$

Subject to the boundary conditions

$$\begin{cases} F_0(0) = 0, F_0'(0) = \delta F_0''(0), G_0(0) = \delta_T G_0'(0) \\ F_0'(\eta) \rightarrow 0, G_0(\eta) \rightarrow 0 \text{ as } \eta \rightarrow \infty \end{cases} \tag{19}$$

According to Dero et al. [44–46], one boundary condition from two should be converted to initial boundary condition (relaxed) in order to achieve the smallest values of eigenvalue. Therefore, $F_0'(\eta) \rightarrow 0$ as $\eta \rightarrow \infty$ is relaxed into $F_0''(0) = 1$.

4 Results and Discussion

The shooting method in Maple code with add of shootlib function has been employed to solve unsteady flow equations and bvp4c code in MATLAB software is used to solve the normalizing stability equations. The results of these codes are compared graphically and numerically with previously published works and found in the excellent agreements. In this study, $\eta_\infty = 4$ is kept fixed during the computations but it is also noticed that $\eta_\infty = 1$ and $\eta_\infty = 3$ are tolerable for temperature and velocity profiles in order to satisfy the $\eta \rightarrow \infty$ as shown in Figs. 9 and 10, respectively. For the numerical compression, Tab. 3 is construction for the magnitude of $f''(0)$ and $-\theta'(0)$ with previously available results of [22]. It is found that our results are showing a favorable agreement. Further, it can be observed from Tab. 4 that the first (second) solution is stable (unstable) as the values of γ are positive (negative). The positive (negative) magnitude of γ should be noted as indicating an initial decay (growth) of disturbance.

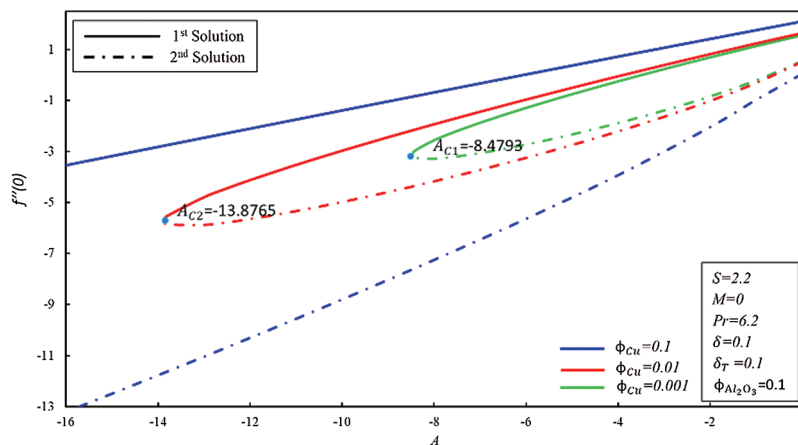


Figure 2: Comparison with the 6th Fig. of [18]

The preparation of a hybrid nanofluid has been shown in the studies of [15,17,22]. They originally considered nanoparticles of alumina (Al_2O_3) into water base fluid and then, nanoparticles of copper (Cu) were mixed with the alumina (Al_2O_3) by considering the distant fractions of solid volume in order to make a hybrid nanofluid. This kind of hybrid nanofluid was called as $Cu - Al_2O_3$ /water. We also follow their works by keeping the $\phi_{Al_2O_3} = 0.1$ as constant in the whole article while the range of $0.001 \leq \phi_{Cu} \leq 0.1$ was kept for copper nanoparticles.

Table 3: Values of $f''(0)$ and $\theta'(0)$ for Cu– Al_2O_3/H_2O hybrid nanofluid for A when $M = \delta = \delta_t = 0, S = 2.1, Pr = 6.2, \phi_{Cu} = 0.2$ and $\phi_{Al_2O_3} = 0.1$

A	$f''(0)$		$-\theta'(0)$	
	1st (2nd) Soln		1st (2nd) Soln	
	Lund et al. [22]	Present Study	Lund et al. [22]	Present
-1	1.608888 (-0.698184)	1.60889 (-0.69818)	5.22381 (5.07375)	5.22382 (5.07376)
-3	0.836978 (-2.531356)	0.83698 (-2.53136)	5.63167 (5.49251)	5.63168 (5.49251)
-5	0.775978 (-6.204355)	0.77598 (-6.20436)	7.63756 (7.44263)	7.63757 (7.44263)
-9	-0.600211 (-10.24173)	-0.60021 (-10.24174)	8.24709639 (8.05819003)	8.24710 (8.05819)

Table 4: The smallest eigenvalues γ for the numerous values of magnetic parameter M at $\phi_{Cu} = \phi_{Al_2O_3} = 0.1, S = 2, Pr = 6.2, \delta = \delta_T = 0.1$ and $A = -5$

M	γ	
	1st solution	2nd solution
1	1.5034	-1.3468
0.9	1.2073	-1.1992
0.8	0.9606	-0.9356
0.6	0.7422	-0.7492
0.3	0.3136	-0.4384
0.2	0.1430	-0.1904
0.1718	0.0072	-0.0003

We have water as a base fluid so $Pr = 6.2$ is kept as constant for the room temperature of $25^\circ C$. The graphical contrast with the sixth graph of [18] is demonstrated in Fig. 2 in order to validate our numerical coding and its results. It can be concluded that our numerical coding is working properly and can be used in this study as the critical values of our figure is the same as given in the article of [18].

Figs. 3 and 4 display the coefficient of skin friction $f''(0)$ and rate of heat transfer $-\theta'(0)$ of Cu – Al_2O_3 /water nanofluid to M for numerous estimations of ϕ_{Cu} , respectively. Range of first and second solutions is $M \geq M_{ci}$ where $i = 1, 2, 3$, whereas range of no solution is $M < M_{ci}$ where M_{ci} shows the critical values of magnetic field for respective $\phi_{Cu} = 0.001, 0.01, 0.1$.

It should be noted that at the pint of M_{ci} , fluid flow of boundary layer initiates converting from laminar flow to turbulent flow and it is noticed from the previous studies that this is possible only when fluid is flowing over the shrinking surface. Further, it is observed that dual solutions exist when the flow is decelerated which means that values of the unsteadiness parameter are negative. Moreover, the rate of heat transfer increases in the first solution for the rising effect of the magnetic field, while it decreases in the second solution.

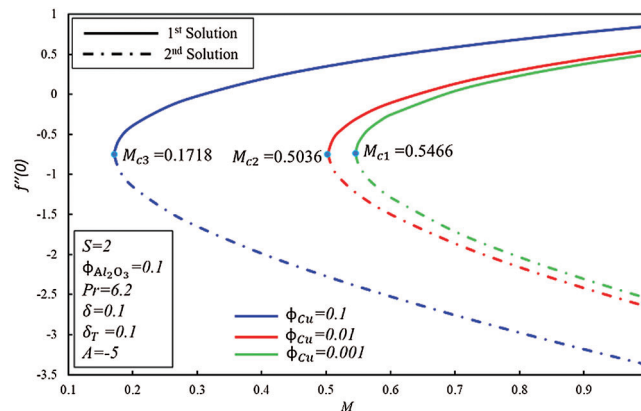


Figure 3: Variation of $f''(0)$ for ϕ_{Cu} along with various values of M

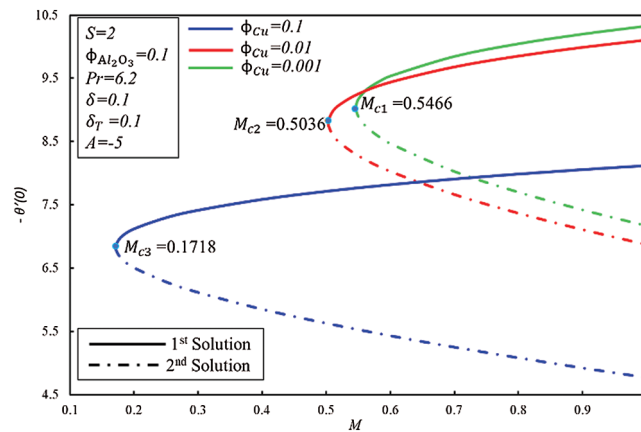


Figure 4: Variation of $-\theta'(0)$ for ϕ_{Cu} along with various values of M

Figs. 5 and 6 show the significance of unsteadiness parameter A for different values of suction parameter S on $f''(0)$ and $-\theta'(0)$, respectively. The coefficient of skin friction $f''(0)$ improves in the first solution as suction increases, whereas it decreases in the second solution. The enhancement in the $f''(0)$ is since suction generates the drag force inside the boundary layer. At the same time, the skin friction coefficient increases in both solutions as the unsteadiness parameter increases. Decreasing and increasing behavior of heat transfer rate observed in two solutions as unsteadiness parameter enhances. Further, the rate of heat transfer enhances in the first solution as suction increases, while dual nature is observed in the second solution.

Variations of $f''(0)$ against velocity slip factor δ for numerous values of A is revealed in Fig. 7. It is noticed that the dual solutions can be found in a specific range of A which is $A_c \geq A$, while no solution is obtained as $A_c < A$, where A_c is known as the critical points where existences of solutions are possible. It is perceived that the presence of slip effect delay the boundary layer separation where $A_{c2} = -6.7138$ and $A_{c2} = -5.8118$ are the critical values of the $\delta = 0.1$ and $\delta = 0.2$, respectively. At the same time, magnitudes of $f''(0)$ increase when $\delta > 0$ in the second solution, whereas there exist dual behaviors in the second solution. Fig. 8 demonstrates the variation of $-\theta'(0)$ versus thermal slip condition δ_T for many values of A . It can be detected that dual behavior is noticed in the magnitude of the rate of heat transfer in the first solution as thermal slip condition δ_T is enhanced, while the rate of heat transfer declines in the second solution when δ_T increases. It is also noticed that $\delta_T = 0, 0.1, 0.2$ has the same critical value which means that increments in the thermal slip do not affect boundary-layer separation.

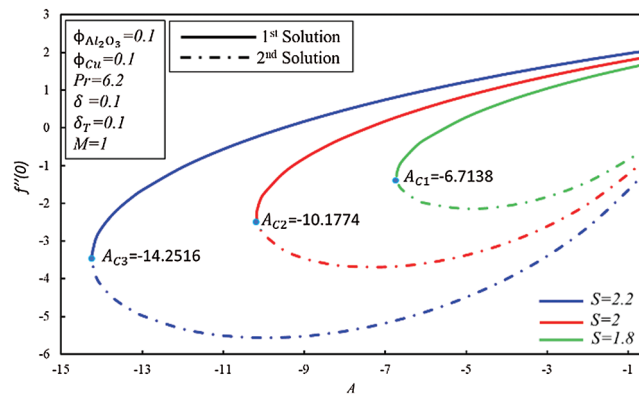


Figure 5: Variation of $f''(0)$ for S along with various values of A

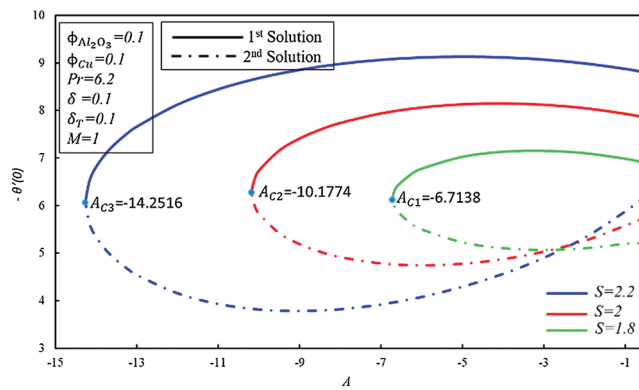


Figure 6: Variation of $-\theta'(0)$ for S along with various values of A

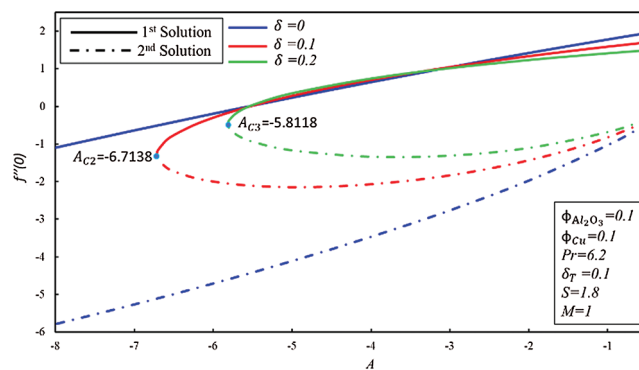


Figure 7: Variation of $f''(0)$ for δ along with various values of A

Effects of ϕ_{Cu} on profiles of velocity $f'(\eta)$ and temperature $\theta(\eta)$ are illustrated in Figs. 9 and 10, respectively. In comparison, the capacity of the thermal enhancement of $Cu - Al_2O_3$ /water hybrid nanofluid is more to Al_2O_3 /water-based nanofluid.

It is gained that fluid velocity declines in the first solution as ϕ_{Cu} enhances and as a resulting thickness of the hydrodynamic layer decreases. After all, velocity increases at first and then starts to decrease in the second solution. Further, enhancements in ϕ_{Cu} are caused to raise the temperature of the fluid in both solutions as shown in Fig. 10.

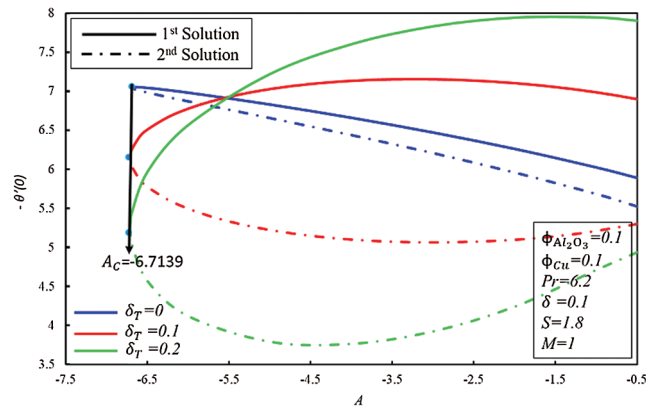


Figure 8: Variation of $-\theta'(0)$ for δT along with various values of A

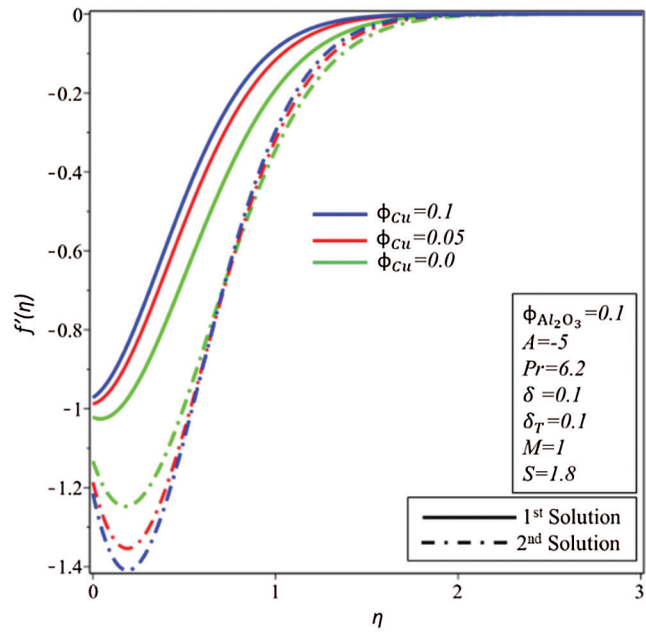


Figure 9: Variation of $f''(\eta)$ for ϕ_{Cu}

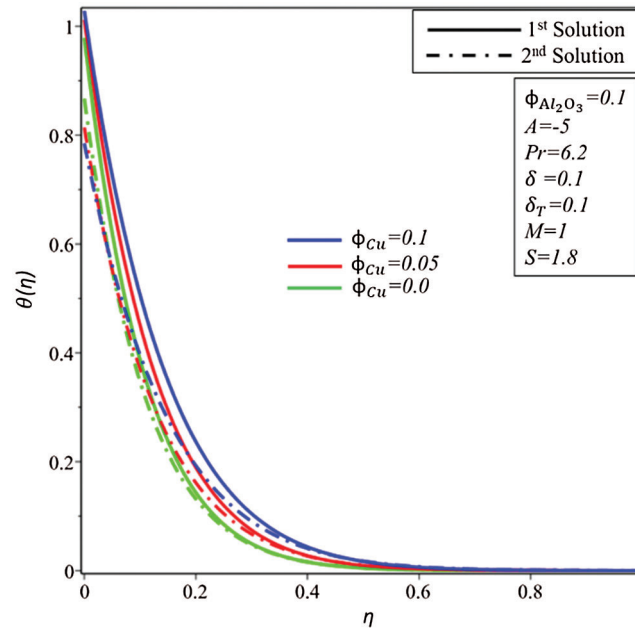


Figure 10: Variation of $\theta(\eta)$ for ϕ_{Cu}

5 Conclusion

In the current examination, the papers of [18,22] are extended in order to inspect the effects of MHD and slip for a hybrid nanofluid case. The current findings were checked for verification with previously reported data and an agreement between those findings is outstanding. Dual solutions have been found in some ranges of magnetic and unsteadiness parameter. The range of the first and second solutions is $M \geq M_{ci}$ where $i = 1, 2, 3$, whereas range of no solution is $M < M_{ci}$ where M_{ci} shows magnetic critical values for respective values of $\phi_{Cu} = 0.001, 0.01, 0.1$. Further, the magnitude of the rate of heat transfer is increased in the first solution as thermal slip condition δ_T is enhanced, while the heat transfer rate declines in the second solution as δ_T increases. The coefficient of skin friction $f'''(0)$ enhances in the first solution as suction increases, while it decreases in the second solution. Stability analyzes are carried out and the results suggest that the first solution is stable.

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Conflicts of Interest: The authors declare that they have no conflicts of interest to report regarding the present study.

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