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Study on a Gas Plunger Lift Model for Shale Gas Wells and Its Effective Application

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ABSTRACT

The problem of efficient gas lift for gas well annulus packers that rely on their own energy plungers is considered. The complex related gas-liquid problem is addressed in the frame of model where the gas inflow dynamics and liquid inflow dynamics of the considered shale gas wells are weakly coupled. On this basis, and with the aiding support of indoor simulation experimental data, a new gas plunger lift design taking into account liquid leakage is obtained. Finally, a dedicated software relying on this approach is developed and used to verify the reliability of the model by means of field examples.

KEYWORDS

Packers; their own energy plungers; shale gas wells; weakly coupled; liquid leakage

Nomenclature

A_a	oil sleeve annulus cross-sectional area, m^2
A_t	tubing cross-sectional area, m^2
C	constant related to tubing size
c	gas well exponential equation coefficient, $10^4 m^3/d/MPa^{2n}$
$f(V_{up})$	loss speed (quantity) function related to factors such as plunger speed (obtained in the above experiment)
f	pressure coefficient of produced gas column in oil and gas well
g	acceleration of gravity, $9.8 kg \cdot m/s^2$
H_k	downhole stopper position, m
H_{tl}	height of liquid level recovery during shut-in, m
H	medium-deep reservoir, m
J	gas well fluid production index, $m^3/d/MPa$
K	constants related to tubing size
n_p	daily cycle times of plunger, times/d
p_a	local atmospheric pressure, MPa
p_{cavg}	average casing pressure, MPa
p_{cmax}	maximum casing pressure, MPa
p_{cmin}	minimum wellhead casing pressure, i.e., the casing pressure when the plunger reaches the wellhead, MPa



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p_p	required pressure to lift the plunger itself (p_p = plunger weight/plunger cross-sectional area), MPa
p_{LH}	required pressure to lift each liquid, MPa/m ³
p_{LF}	friction caused by lifting each liquid, MPa/m ³
q_L	lifting liquid volume per cycle, m ³
p_{tmin}	oil pressure after the plunger reaches the wellhead, MPa
p_{wf}	bottom hole pressure, MPa
q_{gcyc}	air volume required for single-cycle lifting, m ³ ;
Q_G	gas well gas production, 10 ⁴ m ³ /d
Q_l	gas well liquid production, m ³ /d
Q_{real}	actual maximum liquid volume (initial) lifted during the ascent of the plunger every day considering the effect of leakage, m ³ /d
q_{LN}	lifting liquid volume out of the wellhead in a single cycle, m ³ /time
q_L	average liquid volume during single-cycle lifting, m ³ /time
R	production gas-liquid ratio (Calculated based on actual output), m ³ /m ³
t_{dg}	time of plunger falling in gas, min
t_{dl}	time that the plunger falls in the liquid, min
t_{gj}	time for the plunger shut-in pressure recovery, min
t_{up}	plunger up time, min
t_{xl}	time of plunger freewheeling production, min
V_{dg}	speed at which the plunger falls in the gas, m/min
V_{dl}	speed of the plunger falling in the liquid, m/min
V_{up}	average rising speed of the plunger, m/min

Greek letters

ρ	density of the output mixed liquid (usually calculated by weighted average method), 10 ³ kg/m ³
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Plunger drainage gas recovery technology is one of the main drainage technology measures for production from gas wells. Research on the optimization design of plunger gas lift production systems is of great significance to ensure the efficient development of gas wells and improve the work efficiency of on-site management staff. Especially in the current large-scale development and application of shale gas fields, due to the widespread use of large-scale fracturing and commissioning, the initial fluid production levels are relatively large, fluid production continues to slowly decline, and the production parameters change more quickly than those of conventional gas wells. Therefore, drainage gas production is generally required for gas wells [1,2]. The aforementioned plunger gas lift working system is unsuitable at present, and it is difficult for on-site plunger gas lift wells to remain in their optimal production states. Thus, it is necessary to focus more on the inflow dynamics of gas-liquid production from shale gas wells and the corresponding research on plunger gas lift design methods. It is helpful to improve the efficiency of plunger gas lift methods, reduce the intensity of on-site work, save labor costs, increase economic benefits, and provide technical support for the long-term stable production and efficient development of oilfields.

Studies of plunger gas lift technologies began in the late 1930s. At that time, several new plunger structures were designed but not widely used in the oilfield. The main reason was that no plunger gas lift dynamic model could reasonably describe the plunger operation, and these plunger structures had significant defects. In the 1960s, Foss et al. [3] deduced the statistical analysis method of the plunger gas lift wellhead pressures, casing pressures and production based on a large amount of gas well field data by summarizing the actual test data from 110 test wells in the Ventura oil field. For the first time, the static operating model of plunger gas lift was established, and a series of more general plunger lift dynamic curves was drawn, which provided a foundation in the development history of plunger gas lift and has

thus far become the most commonly used empirical method for plunger gas lift designs in vertical wells. The predictions of the model are very close to field data, but the model has limitations and does not consider the nature of gas reservoirs and liquid leakage. This model assumes that the liquid accumulation in the upper part of the lift plunger is driven by the expansion of gas in the annulus (this is the case in most wells, and some gas well tubing and annuli are sealed by packers because the upper annulus and tubing are not connected, so this model is not suitable for use).

Abercrombie [4] established a static model in 1980. He collected a large amount of data for the falling speed of the plunger. Based on this, he adjusted the falling speed of the plunger to be closer to the actual speed, improved the static model, and studied how to best design the plunger.

Lea [5] established the first dynamic model in 1982, which focused on studying the plunger rising stage, and he believed that the plunger speed changes when the plunger is rising, which is contrary to the assumption in the previous static models that the speed is constant. The plunger speed is variable. When establishing the mechanical relationship, he introduced a stable gas reservoir inflow dynamic production curve and assumed that the gas above the plunger was in a stable state during the run of the plunger. The essence of this model was to allow the plunger speed to change with time and depth. After this change, this model was also used to create a computer program to analyze and guide the operating parameters of plunger gas lift wells.

In 1985, Mower et al. [6] established a new model, but this model was quite similar to Lea's model. He introduced a liquid loss term based on field data.

In 1994, Marcano et al. [7] studied the application of plunger gas lift technology in oil and gas wells with high gas-liquid ratios based on previous studies. By assuming a linear relationship between the fallback amounts and the plunger speeds, a plunger gas lift dynamic model that considered liquid leakage during the lifting process was established using the law of mass conservation. Simultaneously, the fallback shapes were compared, verified and corrected in combination with the field data. The errors between the model predictions and actual production data were 15%–20%. It is recommended to correct the application in combination with accurate on-site measured data for complex situations.

In 1995, Baruzzi et al. [8] proposed a dynamic model that simply described the plunger gas lift based on experiments. The model is consistent with the production and pressure dynamics of actual wells. Through the analysis of sensitive parameters based on the model, the following conclusions were drawn: (1) when the wellhead pressure is known, there is an optimal time after flow, and (2) when the time after flow is known, a lower wellhead pressure corresponds to a higher output. They developed a recommended method to optimize the working system for plunger gas lift technology.

In 1997, Gasbarri et al. [9] improved the dynamic model of plunger lifting. The established model considers the friction of the plunger and liquid column, the gas expansion pressure of the upper and lower sections of the plunger and liquid column, and the transient changes in the liquid column that reaches the wellhead, which are convenient for understanding that the plunger gas lift improves the lifting efficiency, increases production and improves the entire production process. The model provides a more complete description of the discharge system, and the simulation results show that the discharge system directly affects the casing pressures, liquid column sizes and rising speeds, so it is also very key. Thus, the model is improved in two aspects: the upward liquid drop of the plunger and the falling speed of the plunger.

In 2000, Maggard et al. [10] established a plunger gas lift performance model that could be applied to tight gas wells based on the characteristics of short-term, rapid changes during tight gas well production and introduced the transient inflow performance curve for gas reservoirs. This model numerically simulates the full-cycle process of the plunger.

In 2008, Chava et al. [11] proposed a new method to simulate plunger lifting. In this method, the pressure and temperature data are obtained by using an intelligent plunger; then, the obtained pressure and temperature data are substituted into the basic mass, momentum and energy conservation equations that control the plunger dynamics to predict the changes in other parameters. This method can accurately reflect the actual dynamics of the plunger, but it cannot predict the dynamic process of plunger lift and can be adjusted and optimized only after installation.

In the same year, Tang et al. [12,13] proposed a new model to describe the plunger movement, which considered the influences of tubing casing pressure changes, fluid accumulations, liquid fall and plunger resistance. However, the model must first quantitatively describe the tubing casing pressure of the plunger gas lift process based on oilfield test data and subsequently use the plunger motion equation to simulate the changes in other parameters, which improves the prediction accuracy of the plunger lift process.

In 2010, based on the application of plunger gas lift in horizontal wells in Sierra oil and gas fields, Sask et al. [14] reported that the greatest difficulty when using plunger gas lift in horizontal wells was that it was difficult for the liquid to rise from the horizontal section to a level above the stopper and one-way valve in the section of the inclined well. Because there is a certain inclination angle, the one-way valve leaked significantly, and the one-way valve was improved to prevent leakage in the inclined well section when the inclination angle was less than 67° . In some horizontal wells, the lifting efficiency and descent speed test measurements of different types of plungers were also carried out, and the influences of the wellbore trajectory and liquid retention in the horizontal wellbore on the performance of the plunger were explored through examples.

In 2011, Kravits et al. [15] conducted a theoretical study on using plunger gas lift technology for drainage gas recovery in horizontal gas wells. A plunger gas lift monitoring system was used to record the falling speed of the plunger and changes in wellhead tubing casing pressures during the test, and the test data were analyzed. The study found that after the plunger passed the wellbore kickoff point, the falling speed significantly increased and then gradually decreased. It was proven that plunger gas lift technology could be applied at large inclination angles in horizontal wells.

In 2015, Nascimento et al. [16] studied three shale gas wells, each with a different trajectory. 1) A transient multiphase simulation device was used to simulate the liquid filling processes of the three wells; 2) a plunger lift was used to simulate gas well drainage; and 3) the startup procedures of the oil wells were optimized. These simulations provided valuable insights into the flows and pressure transients that characterize shale production. The research results provide guidance for optimizing the startup of horizontal shale wells and designing the best shale well trajectory for plunger lifting operations. This method was not previously introduced in the literature, and it emphasizes the role of transient simulations in the shale development planning stage.

In 2018, Nandola et al. [17] proposed an effective method to optimize the plunger lift process of shale gas wells. Plunger lifting is a cyclic process that consists of binary decision-making and continuous and discrete state variables. The time series data that are obtained from surface measurements are converted into process-related periodic data performance outputs, and the binary manipulated variables are converted into continuous threshold values. These converted variables are used to develop a reduced-order cycle-to-cycle model and corresponding rolling optimization problems to maximize daily outputs while meeting operational constraints. The effectiveness of the algorithm was verified on the simulated plunger.

In 2021, a new model proposed by Zhao et al. [18] can obtain the basic parameters of the plunger lifting cycle, including the plunger speeds/accelerations, tubing/casing pressures and productivities. Compared with the previous model, the predicted plunger rising and falling speeds are improved. In this study, the hydrocarbon mixture properties in gas wells are calculated by a component model to provide more accurate and reasonable predictions of the tubing and casing pressures.

In recent years, since the plunger gas lift technology has demonstrated good field application effects and obvious advantages, this technology has entered a period of vigorous development of its popularization and application, and the application scope and technical theory of plunger gas lift technology have been improved. At present, the application of plunger gas lift liquid and gas production technology gradually tends to be intelligent and integrated, and an intelligent plunger production skid for several typical high-liquid well conditions has been developed. The trend of using integrated and intelligent plunger equipment is obvious. Research on the remote intelligent monitoring of plunger drainage technology and dynamic decision-making and planning issues is relatively extensive. However, for completed shale gas horizontal wells, the well structures are complex, the production conditions are complex and variable, and few studies require long-term and efficient development. Considering this limitation and some limitations of Foss's empirical method [1], this paper studies the plunger gas lift design based on the most commonly used empirical method of plunger gas lift design.

1 Theoretical Model

1.1 Gas-Liquid Inflow Dynamic Method for Shale Gas Wells

Because the gas-liquid inflows of shale gas wells are complex and variable, the gas-liquid inflow proportions are not necessarily fixed. Therefore, this paper loosely couples the gas inflow dynamics of shale gas wells with the liquid inflow dynamics, and the gas-liquid flows follow their own inflow dynamic equations. Among them, the inflow dynamic equation for formation gas production can use the binomial equation or other gas well productivity prediction methods, such as the exponential equation. Taking the exponential equation as an example, the equation is:

$$Q_G = c(p_r^2 - p_{wf}^2)^n, \quad n = 0.5 \sim 1.0 \quad (1)$$

The inflow dynamic equation for formation liquid production can be the liquid production index equation, which can be Vogel equation, Fetkovich equation, or Petrobras equation. Using the liquid production index equation as an example, the equation is:

$$Q_l = J \cdot (p_r - p_{wf}) \quad (2)$$

where Q_G is the gas well gas production, $10^4 \text{ m}^3/\text{d}$; Q_l is the gas well liquid production, m^3/d ; c is the gas well exponential equation coefficient, $10^4 \text{ m}^3/\text{d}/\text{MPa}^{2n}$; and J is the gas well fluid production index, $\text{m}^3/\text{d}/\text{MPa}$.

1.2 Design Method of Plunger Gas Lift

The process parameters must be optimized before the plunger gas lift is implemented. The main working parameters of the optimized design include the minimum casing pressure, maximum casing pressure, single-cycle lifting liquid volume, and number of plunger cycles. Among these, parameters such as the minimum casing pressure and maximum casing pressure can be solved by empirical formulas. Since the method of Jin et al. [1] does not consider liquid leakage, this model considers this factor by using the results of an indoor plunger gas lift simulation experiment (e.g., pad plunger simulation experiment), as shown in Fig. 1. Based on the nodal analysis principle, the flow chart (Fig. 2) and calculation method of the plunger gas lift design are as follows.

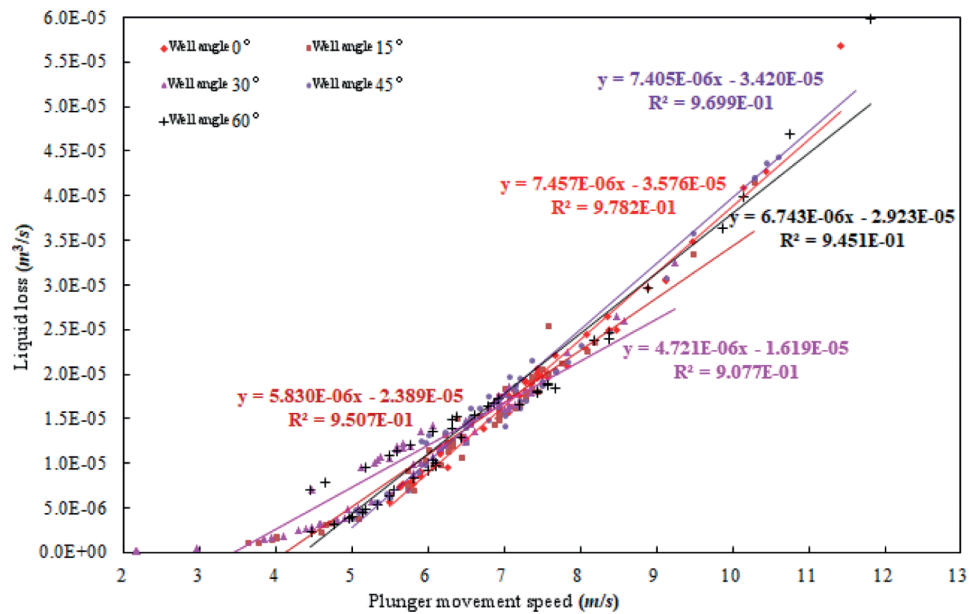


Figure 1: Analysis of the leakage law for the pad plunger

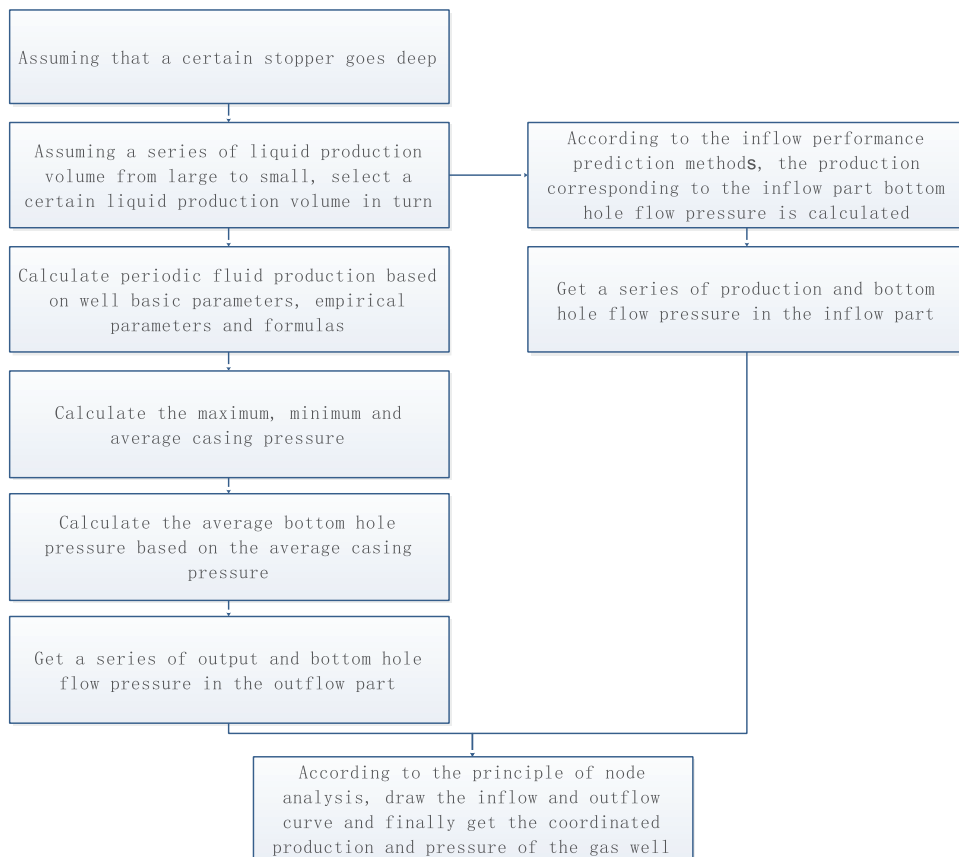


Figure 2: Flow chart of the plunger gas lift design program

(1) Minimum casing pressure

After the well is opened, when the liquid slug on the upper part of the plunger just reaches the wellhead, the tubing and casing pressures are in a balanced state. At this time, the pressure converted from the tubing nozzle to the bottom of the well is equal to the pressure converted from the casing head to the bottom of the well. Simultaneously, relative to the tubing, the annulus volume is larger, and the gas in the annulus expands after the well is opened, so the gas flow rate is very low, and the friction generated by this flow can be ignored. The plunger is very short relative to the liquid slug, so the friction caused by plunger movement can also be ignored. Thus, the following equation applies:

$$p_{cmin} = [p_p + p_{tmin} + p_a + (p_{LH} + p_{LF}) \times q_L] \times \left(1 + \frac{H_k}{K}\right) \quad (3)$$

where p_{cmin} is the minimum wellhead casing pressure, which is the casing pressure when the plunger reaches the wellhead, MPa; p_p is the pressure required to lift the plunger (e.g., p_p = plunger weight/plunger cross-sectional area), MPa; p_{LH} is the pressure required to lift liquid in each cycle, MPa/m³; p_{LF} is the friction caused by lifting liquid in each cycle, MPa/m³; q_L is the liquid lifting volume per cycle, m³; p_{tmin} is the oil pressure after the plunger reaches the wellhead, MPa; p_a is the local atmospheric pressure, MPa; H_k is downhole stopper position, m; and K is a constant related to the tubing size.

(2) Maximum casing pressure and average casing pressure

$$p_{cmax} = \left[\frac{A_t + A_a}{A_a} \right] \times p_{cmin} \quad (4)$$

where p_{cmax} is the maximum casing pressure, MPa; A_t is the cross-sectional area of the tubing, m²; and A_a is the cross-sectional area of the oil sleeve annulus, m².

Then, the average casing pressure can be calculated as the average maximum casing pressure, and the minimum casing pressure is:

$$p_{cavg} = \left(1 + \frac{A_t}{2A_a}\right) \times p_{cmin} \quad (5)$$

where p_{cavg} is the average casing pressure, MPa.

(3) Gas and liquid production of gas wells

To calculate the gas and liquid production of gas wells according to the method of gas-liquid inflow performance in [Section 1.1](#) for middle shale gas wells, the average bottom hole flow pressure according to the average casing pressure is first calculated; then, the gas production Q_G and liquid production Q_L are calculated according to the methods described in [Section 1.1](#). The formula to calculate the average bottom hole pressure is as follows:

$$p_{wf} = p_{cavg}(1 + f) + \rho g(H - H_k)/1000 \quad (6)$$

where p_{wf} is the bottom hole pressure, MPa; ρ is the density of the mixed liquid output (usually calculated by the weighted average method), 10³ kg/m³; H is the depth of a medium-deep reservoir, m; g is the gravitational acceleration, 9.8 kg · m/s²; and f is the pressure coefficient of the produced gas column in an oil and gas well.

Assuming that Q_L is the fluid production volume at the production wellhead, considering the effect of leakage, the actual daily maximum liquid volume (initial) that is lifted during the ascent of the plunger is:

$$Q_{real} = Q_L + t_{up} \times n_p \times f(V_{up}) \quad (7)$$

where $f(V_{up})$ is the loss speed (quantity) function that is related to factors such as the plunger speed (obtained in the above experiment).

(4) Gas volume and gas-liquid ratio required for single-cycle lifting

$$q_{gcyc} = C \times H_k \times P_{cavg} \quad (8)$$

where q_{gcyc} is the air volume required for single-cycle lifting, m^3 , and C is a constant related to the tubing size.

(5) Daily plunger cycle times

The time required for the plunger gas lift process to complete one working cycle is defined by the opening time and closing time. The well opening time includes the time when the plunger goes up and the time when the upper liquid section of the plunger continues to flow at the wellhead. The shut-in time includes the downward time of the plunger and the time when the plunger remains at the bottom of the well to wait for pressure recovery. Therefore, the daily plunger operating cycle times are:

$$n_p = \frac{1440}{t_{up} + t_{xl} + t_{dg} + t_{dl} + t_{gj}} \quad (9)$$

$$t_{dg} = \frac{H_{il}}{V_{dg}} \quad (10)$$

$$t_{dl} = \frac{H_k - H_{il}}{V_{dl}} \quad (11)$$

$$t_{up} = \frac{H_k}{V_{up}} \quad (12)$$

where n_p is the daily plunger cycle time, time/d; t_{up} is the plunger up time, min; t_{xl} is the plunger freewheeling production time, min; t_{dg} is the time that the plunger falls in gas, min; t_{dl} is the time that the plunger falls in liquid, min; t_{gj} is the time for the plunger shut-in pressure to recover, min; H_{il} is height of the liquid level recovery during shut-in, m; V_{dg} is the speed at which the plunger falls in gas, m/min; V_{dl} is the speed at which the plunger falls in liquid, m/min; and V_{up} is the average rising speed of the plunger, m/min.

The recovery time for the plunger shut-in pressure can be calculated as follows:

$$t_{gj} = \frac{1440q_{gcyc}}{Q_G} - t_{dg} - t_{dl} \quad (13)$$

The continuous flow production time of the plunger must be determined based on the time required for the wellhead oil pressure to drop to p_{cmin} after the wellhead fluid is discharged.

(6) Single-cycle lifting liquid volumes

$$q_L = \frac{Q_L + Q_{real}}{2n_p} \quad (14)$$

$$q_{LN} = \frac{Q_L}{n_p} \quad (15)$$

$$R = \frac{q_{gcyc}}{q_{LN}} \quad (16)$$

where q_L is the average liquid volume during single-cycle lifting, m^3/time ; q_{LN} is the lifting liquid volume out of the wellhead in a single cycle, m^3/time ; and R is the production gas-liquid ratio (calculated based on the actual output), m^3/m^3 .

2 Software Compilation and Example Verification Analysis

2.1 Software Compilation

The software is developed based on the new theoretical model. The bottom function algorithm of the software adopts VB (Visual Basic), and the top interface design and diagram drawing use C# (C sharp). The software is not open-source. The trial version can be obtained by contacting the corresponding author (luoruichang@163.com). The operating environment is as follows.

System Requirements:

Windows Server 2008, Windows Vista, or Windows 7/8/10 operating system;

Windows XP, Windows Server 2003 and other operating systems need to install Microsoft.NET Framework version 4.0;

AMD/Intel 1.6 GHz or above processor;

Total RAM memory of 2 GB or above.

Recommended configuration:

Microsoft Windows version 7 or higher;

Intel Core i3 or an equivalent AMD processor;

2.2 Example Verification

Example 1 involves example well XXX1 (Table 1), and the basic parameters are as follows.

Table 1: Basic parameters of well XXX1

Well parameters	Unit	Value
Formation pressure	MPa	27.86
Fluid production index	$m^3/d/MPa$	1.5
Relative density of crude oil	-	0.7517
Relative density of water	-	1.008
Water cut	decimal	0.75
Wellhead oil pressure	MPa	8.5
Well depth	m	3998
Casing inner diameter	mm	124
Plunger quality	kg	8
Wellhead temperature	C	30
Bottom hole temperature	C	113.8
Gas relative density	-	0.6066
Gas production index	$10^4 m^3/d/MPa^2$	0.025
Tubing inner diameter	mm	62

(1) Parameter input (Figs. 3–5)

Plunger well information

Well Name: Angle with horizontal(°): 90 Well diameter(mm): 200

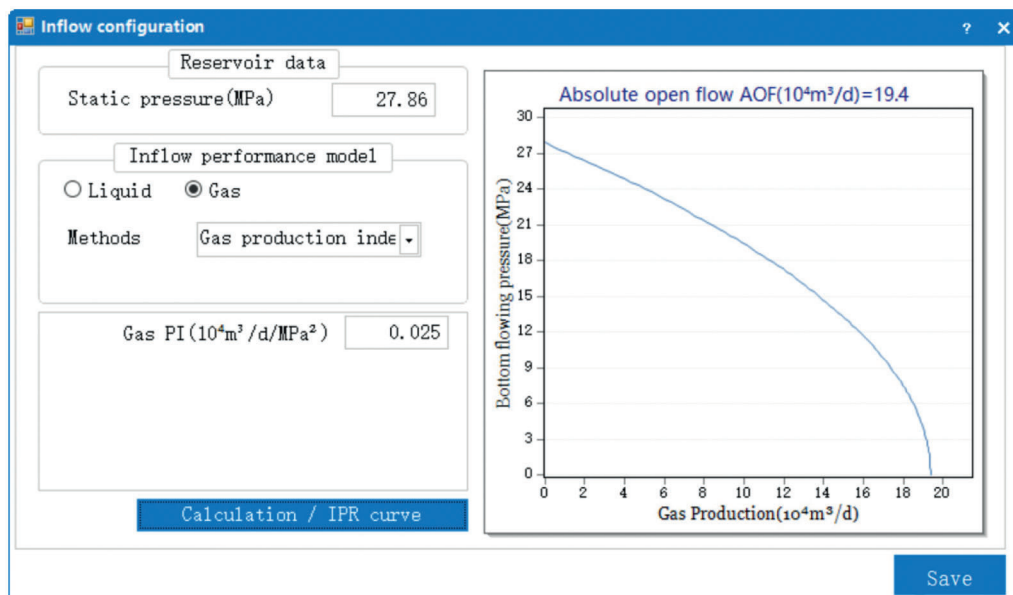
Well TVD(m): 3998 Casing Diameter(mm): 124 Tubing diameter(mm): 62

Well Type:
☐ Oil Well ☒ Gas Well

Physical parameters
 Water Density(kg/m³): 1008 Gas relative density: 0.61 Oil Density(kg/m³): 751.7
 GOR(m³/m³): 0

Production parameters
 WHP(MPa): 8.5 WHT(°C): 30 Reservoir Temp(°C): 113.8
 Liquid Rate(m³/d): 4 Gas rate(10⁴m³/d): 3.6 Water cut(%): 75

OK

Figure 3: Basic gas well parameters (e.g., fluid properties and well profile configuration)**Figure 4:** Graph of the gas inflow performance

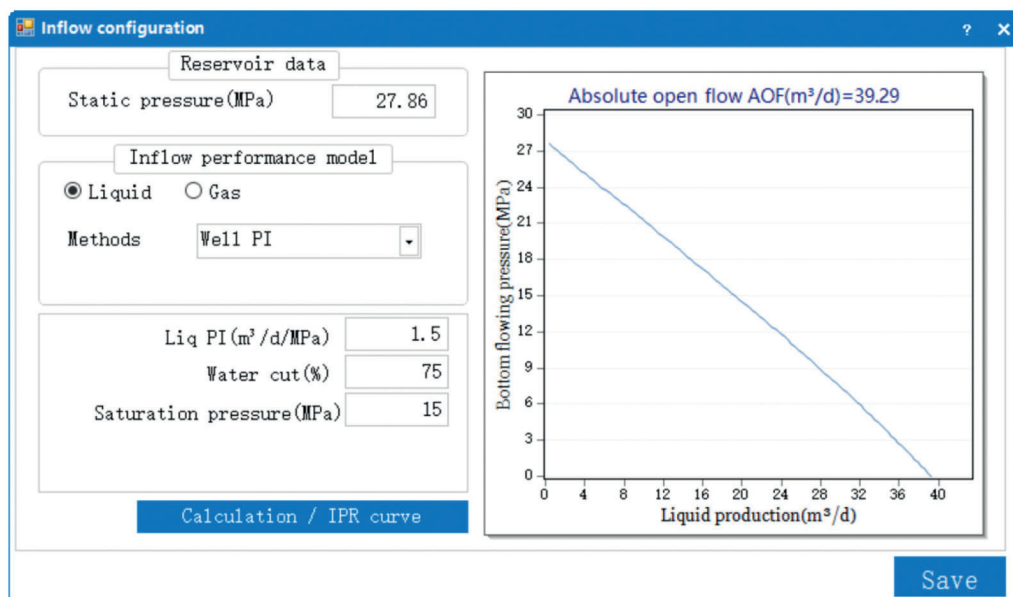


Figure 5: Graph of the liquid inflow performance

(2) Depth optimization of the stopper

The design results for different plunger stopper depths using a model that considers leakage are shown in the following Figs 6–8. Figs. 7 and 8 show that the liquid discharge increases with increasing stopper depth, but the increase in liquid discharge decreases after the stopper depth reaches approximately 3600 m. Therefore, the recommended stopper depth is approximately 3600 m.

Plunger rising speed(m/min) Falling in gas(m/min) Falling in liquid(m/min) Plunger mass(kg)

Sensitivity parameters

☐ Wellhead residence time

☐ Stay time on the stopper

☒ Depth of stopper

parameter settings

Depth of stopper(m)

3000

-

3800

Wellhead stay time (min)

105

Stay time on the stopper(min)

15

Depth of stopper(m)

Parameters save

calculate

Liquid leakage

☐ Without

☒ With

Depth of stopper(m)	cycle (min)	Number of cycles per day	Cycle lift volume (m³)	Daily lifting volume (m³)	Periodic gas injection (m³)	Daily gas injection (m³)	Cycle gas reduction(m³)	Daily gas production (m³)	Pcmin(MPa)	Pcmax(MPa)
▶ 3000	168.51	8.55	0.19	1.6	0	0	1701.48	14539.89	12.82	17.09
3040	169.22	8.51	0.22	1.9	0	0	2029.64	17271.12	13.05	17.4
3080	169.94	8.47	0.26	2.19	0	0	2338.93	19819.38	13.27	17.7
3120	170.65	8.44	0.29	2.46	0	0	2623.13	22134.56	13.49	17.98
3160	171.35	8.4	0.32	2.66	0	0	2844.07	23900.83	13.67	18.22
3200	172.06	8.37	0.34	2.85	0	0	3059.34	25604.86	13.85	18.46
3240	172.76	8.34	0.37	3.04	0	0	3268.97	27247.46	14.02	18.7
3280	173.45	8.3	0.38	3.19	0	0	3434.59	28513.62	14.17	18.9
3320	174.15	8.27	0.4	3.34	0	0	3600.96	29774.96	14.33	19.1
3360	174.85	8.24	0.42	3.47	0	0	3755.28	30926.96	14.47	19.3
3400	175.55	8.2	0.44	3.61	0	0	3910.27	32074.89	14.62	19.5
3440	176.25	8.17	0.46	3.72	0	0	4040.31	33011.1	14.76	19.67
3480	176.94	8.14	0.47	3.83	0	0	4171.05	33944.59	14.89	19.86
3520	177.65	8.11	0.48	3.93	0	0	4289.66	34772.09	15.02	20.03
3560	178.33	8.07	0.5	4	0	0	4382.83	35391.3	15.13	20.18
3600	179.02	8.04	0.51	4.08	0	0	4476.64	36009.31	15.25	20.33
3640	179.71	8.01	0.52	4.15	0	0	4571.01	36626.11	15.37	20.49
3680	180.41	7.98	0.53	4.21	0	0	4652.88	37139.19	15.47	20.63
3720	181.1	7.95	0.54	4.27	0	0	4735.2	37651.43	15.58	20.78
3800	182.49	7.89	0.55	4.36	0	0	4868.63	38418.22	15.79	21.05
*										

Figure 6: Plunger gas lift design for different plunger stopper depths

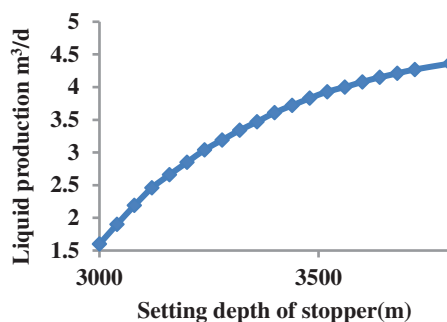


Figure 7: Liquid production for the plunger gas lift design for different plunger stopper depths

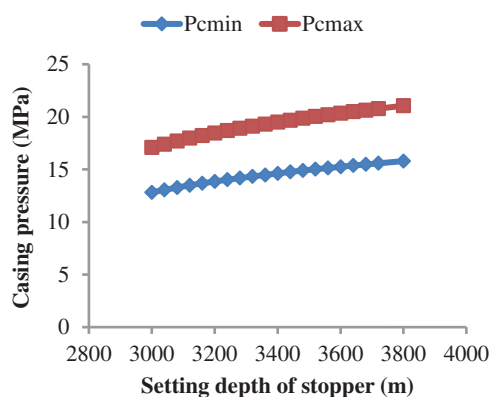


Figure 8: Casing pressures for the plunger gas lift design for different plunger stopper depths

The software determines that when the depth of the plunger stopper is 3640 m, the well is opened for 2 h and closed for 1 h, the gas production is 36626.1 m³/day, and the liquid production is 4.15 m³/day when a model that considers leakage is employed. As shown in Table 2, compared with the production data of the gas well with an actual plunger stopper depth of 3642.16 m (the gas production is 36000 m³/day and liquid production is 4 m³/day), the calculation error of the software simulation of the well is less than 5.0%.

Table 2: Plunger gas lift design parameters using a model considering leakage and a model that does not consider leakage

Design parameters	The model with liquid leakage	The model without liquid leakage
Depth of stopper (m)	3640	3640
Cycle (min)	179.71	179.71
Number of cycles per day	8.01	8.01
Cycle lift volume (m ³)	0.518	0.521
Daily lifting volume (m ³)	4.15	4.17
Periodic gas injection (m ³)	0	0
Daily gas injection (m ³)	0	0
Cycle gas production (m ³)	4571.01	4596.56

(Continued)

Table 2 (continued)		
Design parameters	The model with liquid leakage	The model without liquid leakage
Daily gas production (m ³)	36626.11	36731.44
P _{cmin} (MPa)	15.37	15.36
P _{cmax} (MPa)	20.49	20.48
Periodic gas demand (m ³)	1700.04	1699.26
Dropping time of plunger liquid column (min)	4.86	4.85
Plunger air column drop time (min)	41.86	41.86
Plunger up time (min)	13	13
Shut-in time (min)	61.71	61.71
Opening time (min)	118	118

Table 2 and Fig. 9 show the model that considers leakage and one that does not consider leakage factors. The changes in fluid production are small. Figs. 10 and 11 show that a higher plunger speed corresponds to a higher casing pressure and smaller corresponding liquid production.

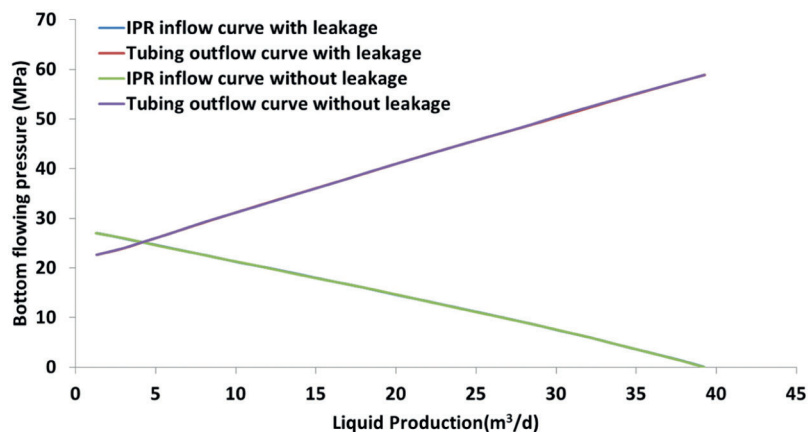


Figure 9: Nodal analysis graph of the plunger gas lift design

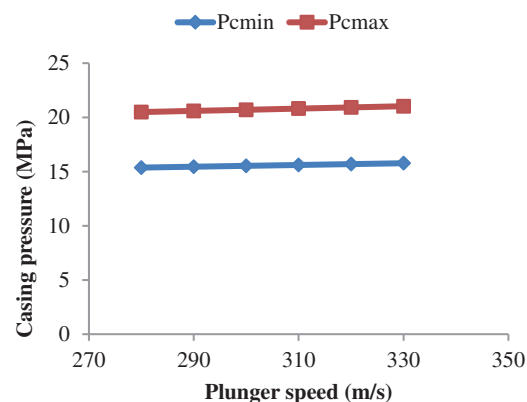


Figure 10: Casing pressures by analyzing the sensitive parameter of plunger velocity for a stopper depth of 3640 m

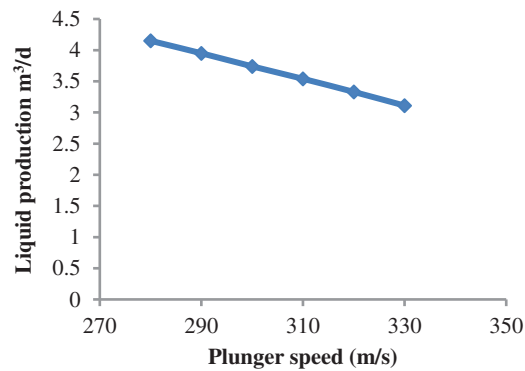


Figure 11: Liquid production by analyzing the sensitive parameter of plunger velocity for a stopper depth of 3640 m

Example 2 involves example well XXX2 (Table 3), and the basic parameters are as follows.

Table 3: Basic parameters of well XXX2

Well parameters	Unit	Value
Formation pressure	MPa	32.71
Fluid production index	m ³ /d/MPa	2.03
Relative density of crude oil	-	0.7766
Relative density of water	-	1.0073
Water cut	decimal	0.76
Wellhead oil pressure	MPa	8
Well depth	m	3846.56
Casing inner diameter	mm	121
Plunger quality	kg	8
Wellhead temperature	C	21
Bottom hole temperature	C	111.7
Gas relative density	-	0.6214
Gas production index	10 ⁴ m ³ /d/MPa ²	0.012
Tubing inner diameter	mm	62

(1) Parameter input (Figs. 12–14)

Plunger well information

Well Name: 326 Angle with horizontal(°): 90 Well diameter(mm): 200

Well TVD(m): 3846.6 Casing Diameter(mm): 121 Tubing diameter(mm): 62

Well Type:
☐ Oil Well ☒ Gas Well

Physical parameters

Water Density(kg/m³): 1007.3 Gas relative density: 0.62 Oil Density(kg/m³): 776.6

GOR(m³/m³): 0

Production parameters

WHP(MPa): 8 WHT(°C): 21 Reservoir Temp(°C): 111.7

Liquid Rate(m³/d): 9.54 Gas rate(10⁴m³/d): 3.45 Water cut(%): 76.06

OK

Figure 12: Basic gas well parameters (e.g., fluid properties and well profile configuration)

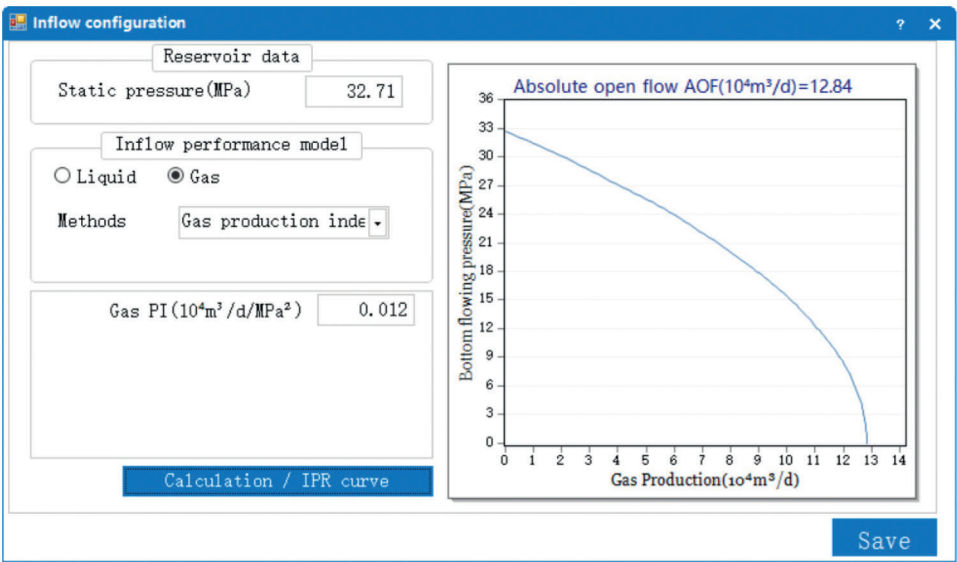


Figure 13: Graph of the gas inflow performance

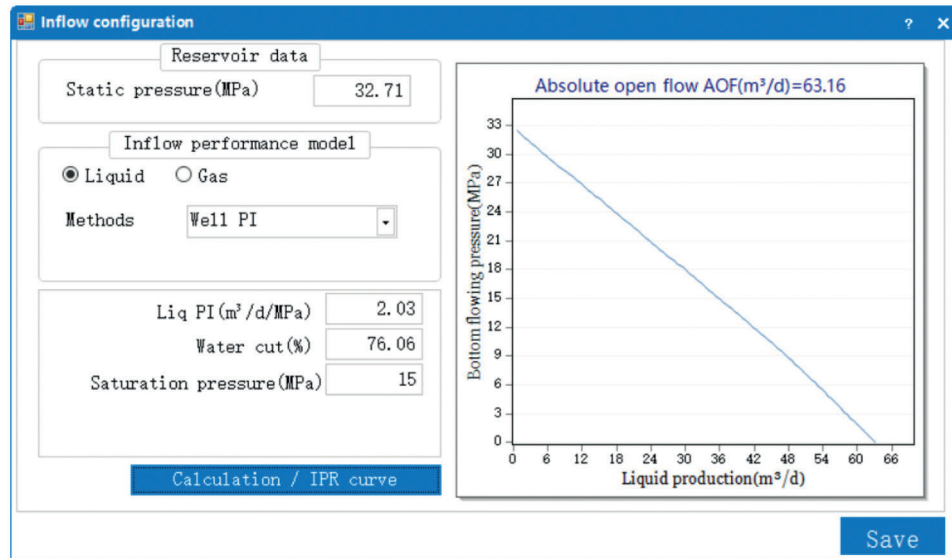


Figure 14: Graph of the liquid inflow performance

(2) Depth optimization of the stopper

The design results for different plunger stopper depths are shown in the following Figs 15–17. Figs. 16 and 17 show that the liquid discharge amounts increase with increasing stopper depths, but when the stopper depth reaches approximately 3500 m, the discharge volume slowly increases. Therefore, the depth of the stopper is recommended to be set to approximately 3500 m.

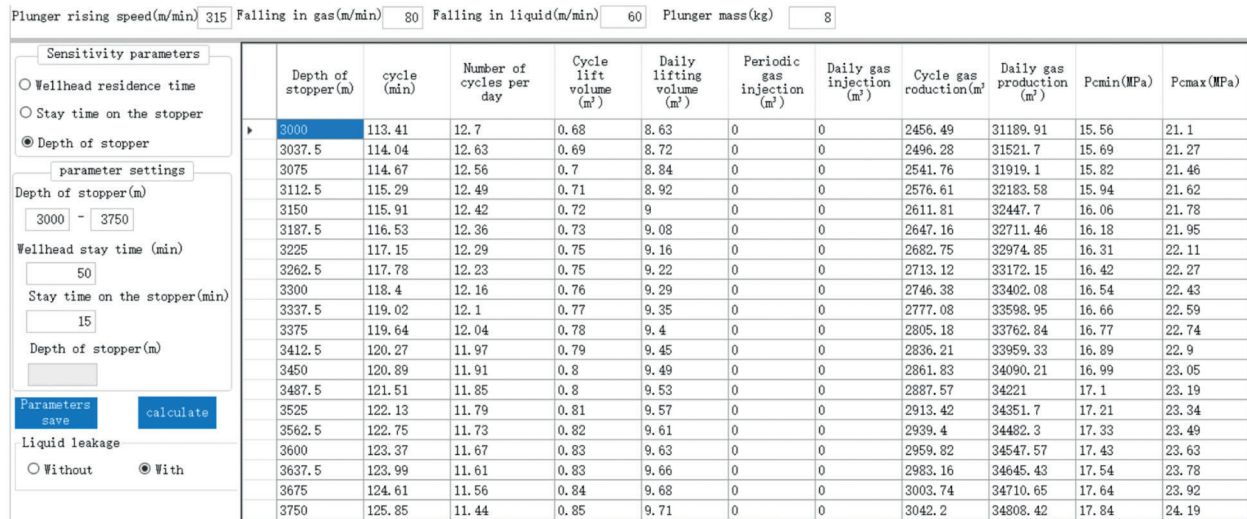


Figure 15: Plunger gas lift design for different plunger stopper depths

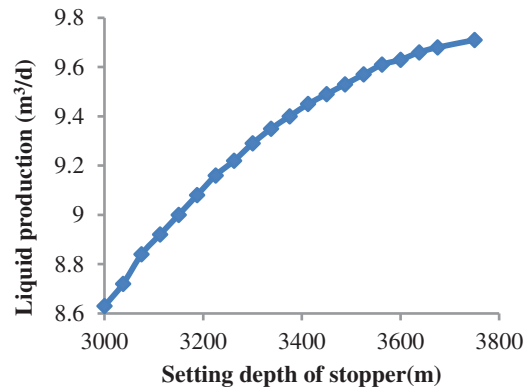


Figure 16: Liquid production of the plunger gas lift design for different plunger stopper depths

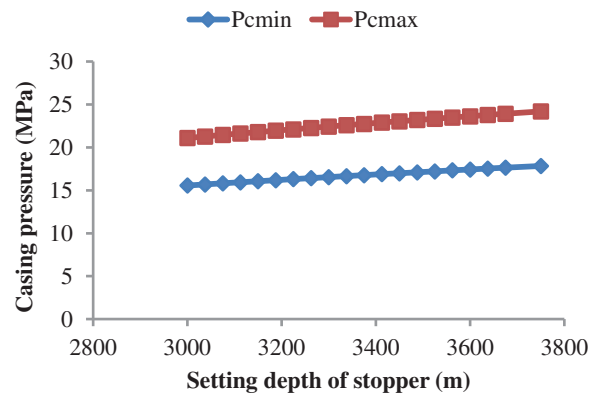


Figure 17: Casing pressures of the plunger gas lift design for different plunger stopper depths

The software determines that when the depth of the plunger stopper is 3525 m, the well is opened for 1 h and closed for 1 h, the gas production is 34351.7 m³/day, and the liquid production is 9.57 m³/day. As shown in the figure below, compared with the production data of the actual plunger stopper depth of 3500 m (e.g., gas production is 34500 m³/day and liquid production is 9.54 m³/day), the software simulation calculation error for the well is less than 5.0%.

Table 4 and Fig. 18 show the results when the model considers leakage and does not consider leakage factors; the changes in fluid production are small. Figs. 19 and 20 show that a higher plunger speed corresponds to a higher casing pressure and smaller corresponding liquid production.

Table 4: Plunger gas lift design parameters using a model with leakage and a model without leakage

Design parameters	The model with liquid leakage	The model without liquid leakage
Depth of stopper (m)	3525	3525
Cycle (min)	122.13	122.12
Number of cycles per day	11.79	11.79
Cycle lift volume (m ³)	0.81	0.82
Daily lifting volume (m ³)	9.57	9.69

(Continued)

Table 4 (continued)		
Design parameters	The model with liquid leakage	The model without liquid leakage
Periodic gas injection (m^3)	0	0
Daily gas injection (m^3)	0	0
Cycle gas production (m^3)	2913.42	2946.33
Daily gas production (m^3)	34351.7	34743.25
Pcmin (MPa)	17.21	17.17
Pcmax (MPa)	23.34	23.29
Periodic gas demand (m^3)	1862.35	1858.01
Dropping time of plunger liquid column (min)	7.5	7.45
Plunger air column drop time (min)	38.44	38.47
Plunger up time (min)	11.19	11.19
Shut-in time (min)	60.94	60.93
Opening time (min)	61.19	61.19

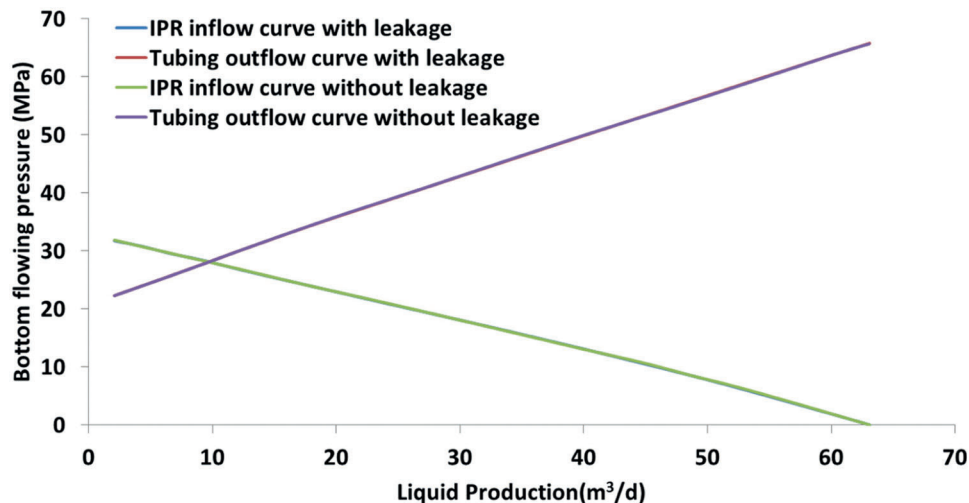


Figure 18: Nodal analysis graph of the plunger gas lift design

2.3 Feasibility Analysis of the Plunger Gas Lift with a Packer in the Annulus

Taking well XXX2 as an example, the following principles are:

- (1) The principle of equivalent casing inner diameter states that the storage space below the packer is equal to the volume of an equivalent amount of casing;
- (2) The maximum achievable pressure in the reservoir space is the formation pressure; i.e., the designed maximum casing pressure + pressure gradient cannot be greater than the formation pressure.

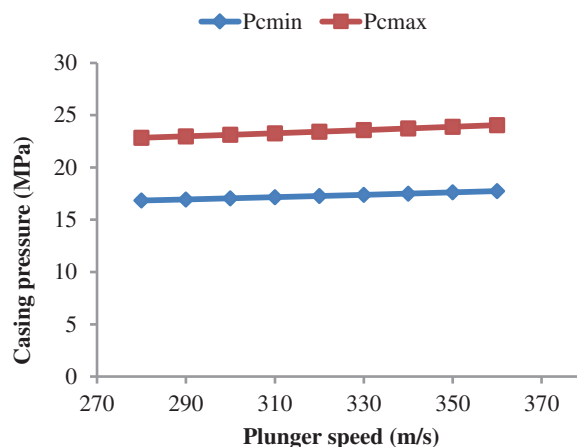


Figure 19: Casing pressures by analyzing the sensitive parameter of plunger velocity for a stopper depth of 3525 m

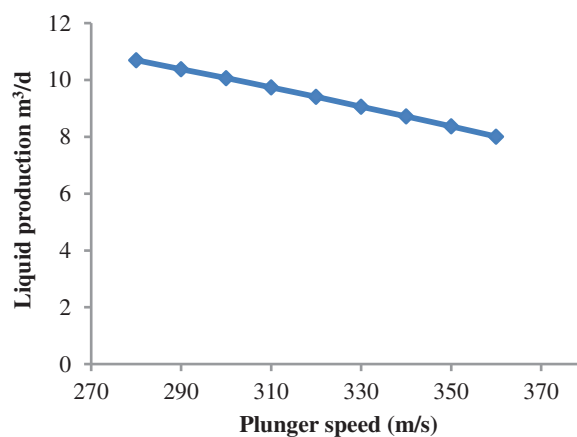


Figure 20: Liquid production by analyzing the sensitive parameter of plunger velocity for a stopper depth of 3525 m

According to these principles, the plunger gas lift dynamic model is used for simulation analysis. [Tables 5–7](#) provide the maximum running depths of the stopper for the plunger gas lift based on the energy of a gas well with a 121-mm inner casing diameter. [Table 5](#) shows that for the case of a 121-mm inner casing diameter and 8 MPa wellhead pressure, plunger gas lift drainage is not feasible after the depth of the packer exceeds 3200 m. When the wellhead pressure decreases to 2 MPa, plunger gas lift drainage can occur when the packer is not deeper than 3600 m and the stopper is not deeper than 2900 m. [Tables 5–7](#) show that with decreasing formation pressures, the feasible range for plunger gas lift in gas wells with packers gradually decreases.

① The formation pressure is 32.71 MPa

Depth feasibility analysis of the plunger gas lift with a packer in the casing with an inner diameter of 121 mm.

Table 5: Plunger depth analysis of the plunger gas lift in the casing with an inner diameter of 121 mm with a packer

Packer depth/m	Well depth/m	Packer storage length/m	Tubing inner diameter/mm	Casing inner diameter/mm	Relative casing inner diameter/mm	The maximum allowable depth of the retainer produced by its own energy plunger/m	Wellhead oil pressure/MPa
1000	3846.6	2846.6	62	121	108.8	3800	8
1200	3846.6	2646.6	62	121	106.2	3800	8
1400	3846.6	2446.6	62	121	103.5	3800	8
1600	3846.6	2246.6	62	121	100.7	3800	8
1800	3846.6	2046.6	62	121	97.9	3800	8
2000	3846.6	1846.6	62	121	95.0	3800	8
2200	3846.6	1646.6	62	121	92.0	3800	8
2400	3846.6	1446.6	62	121	88.9	3800	8
2600	3846.6	1246.6	62	121	85.7	3800	8
2800	3846.6	1046.6	62	121	82.4	3720	8
3000	3846.6	846.6	62	121	78.9	2900	8
3200	3846.6	646.6	62	121	75.2	3800	2
3400	3846.6	446.6	62	121	71.4	3800	2
3600	3846.6	246.6	62	121	67.4	2900	2
3800	3846.6	46.6	62	121	63.0		

② The formation pressure is 20 MPa

Table 6: Plunger depth analysis of plunger gas lift in casing with an inner diameter of 121 mm with a packer

Packer depth/m	Well depth/m	Packer storage length/m	Tubing inner diameter/mm	Casing inner diameter/mm	Relative casing inner diameter/mm	The maximum allowable depth of the retainer produced by its own energy plunger/m	Wellhead oil pressure/MPa
1000	3846.6	2846.6	62	121	108.8	3600	8
1200	3846.6	2646.6	62	121	106.2	3560	8
1400	3846.6	2446.6	62	121	103.5	3800	2
1600	3846.6	2246.6	62	121	100.7	3800	2
1800	3846.6	2046.6	62	121	97.9	3800	2
2000	3846.6	1846.6	62	121	95.0	3800	2
2200	3846.6	1646.6	62	121	92.0	3800	2
2400	3846.6	1446.6	62	121	88.9	3800	2
2600	3846.6	1246.6	62	121	85.7	3800	2

(Continued)

Table 6 (continued)

Packer depth/m	Well depth/m	Packer storage length/m	Tubing inner diameter/mm	Casing inner diameter/mm	Relative casing inner diameter/mm	The maximum allowable depth of the retainer produced by its own energy plunger/m	Wellhead oil pressure/MPa
2800	3846.6	1046.6	62	121	82.4	3800	2
3000	3846.6	846.6	62	121	78.9	3800	2
3200	3846.6	646.6	62	121	75.2	3800	2
3400	3846.6	446.6	62	121	71.4	3480	2
3600	3846.6	246.6	62	121	67.4		
3800	3846.6	46.6	62	121	63.0		

③ The formation pressure is 15 MPa

Table 7: Plunger depth analysis of plunger gas lift in casing with an inner diameter of 121 mm with a packer

Packer depth/m	Well depth/m	Packer storage length/m	Tubing inner diameter/mm	Casing inner diameter/mm	Relative casing inner diameter/mm	The maximum allowable depth of the retainer produced by its own energy plunger/m	Wellhead oil pressure/MPa
1000	3846.6	2846.6	62	121	108.8	3800	2
1200	3846.6	2646.6	62	121	106.2	3800	2
1400	3846.6	2446.6	62	121	103.5	3800	2
1600	3846.6	2246.6	62	121	100.7	3800	2
1800	3846.6	2046.6	62	121	97.9	3800	2
2000	3846.6	1846.6	62	121	95.0	3800	2
2200	3846.6	1646.6	62	121	92.0	3800	2
2400	3846.6	1446.6	62	121	88.9	3800	2
2600	3846.6	1246.6	62	121	85.7	3800	2
2800	3846.6	1046.6	62	121	82.4	3800	2
3000	3846.6	846.6	62	121	78.9	3600	2
3200	3846.6	646.6	62	121	75.2	3120	2
3400	3846.6	446.6	62	121	71.4		
3600	3846.6	246.6	62	121	67.4		
3800	3846.6	46.6	62	121	63.0		

3 Conclusions

Considering the complex and variable gas-liquid inflows in shale gas wells, a loosely coupled method to determine the shale gas well gas inflow dynamics and liquid inflow dynamics is proposed, and the gas and

liquid follow their respective inflow dynamic equations, which are combined with the experimental data of plunger gas lift leakage. Using the node analysis principle, a new model for plunger gas lift design that considers leakage factors was established, software development was completed, and the analysis was verified using field examples. Based on this model, a method for evaluating the feasibility of plunger gas lift by using the equivalent annulus inner diameter method for a gas well annulus with a packer is provided, and a feasibility analysis of the plunger gas lift is carried out for typical gas wells. The following conclusions are reached:

- (1) By comparing the calculated cycle, wellhead oil casing pressures and other operational parameters with the actual operational production parameters, the coincidence rate is more than 90%, which verifies the reliability of the established model.
- (2) The leakage amounts are closely related to the movement speeds of the plunger, but when the average movement speed of the plunger is small, the upward leakage of the plunger is small. The wellhead casing pressures are also closely related to the movement speeds of the plunger. With higher movement speeds of the plunger, higher wellhead casing pressures are required.
- (3) For a 121-mm-inner-diameter gas well casing, when the wellhead pressure is 8 MPa and the depth of the packer exceeds 3200 m, the plunger gas lift drainage is not feasible. When the wellhead pressure decreases to 2 MPa, plunger gas lift drainage can occur when the packer is lowered to deeper than 3600 m and the retainer is lowered to deeper than 2900 m. With a decrease in formation pressure of the gas well, the feasible range for plunger gas lift in the gas well with a packer gradually decreases.

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