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SCALING GROUP TRANSFORMATION FOR MIXED CONVECTION IN A POWER-LAW FLUID SATURATED POROUS MEDIUM WITH EFFECTS OF SORET, RADIATION AND VARIABLE PROPERTIES

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ABSTRACT

An analysis is performed to investigate the influence of radiation, thermal-diffusion and variable properties on mixed convection flow, heat and mass transfer from a vertical plate in a porous medium saturated with a power-law fluid. The non-linear partial differential equations are reduced to ordinary differential equations by implementing Lie scaling group transformations. These ordinary differential equations are solved numerically by implementing a shooting technique. The numerical results for dimensionless velocity, temperature and concentration profiles for pseudo-plastic, Newtonian and dilatant fluids are presented graphically for different values of variable viscosity, variable thermal conductivity, Soret and radiation parameters. Heat and mass transfer results are presented in tabular form. The present numerical results are compared with previously published work and the results are found to be in excellent agreement.

Keywords: Mixed convection, Variable viscosity, Power-law fluid, Thermal Radiation, Thermal conductivity, Soret, Lie Scaling Group Transformations.

1. INTRODUCTION

Research on convective heat and mass transfer of power-law fluids has received much attention for several years due to its theoretical and practical importance in industrial processing equipment, dealing with molten plastics, paints, polymers, pharmaceutical formulations, cosmetics and toiletries, ground water flow, etc. Several researchers have presented their work in the literature focusing on the problem of convection heat and mass transfer in power-law fluids. Details of review of the literature on power-law fluids and their applications may be found in the recent books by Pop and Ingham (2001), Nield and Bejan (2006) and Vafai (2015). On the other hand, Power-law fluid saturated porous media are a branch of research undergoing rapid growth in fluid mechanics and heat transfer characteristic of a wide range of engineering applications in several problems areas such as nuclear reactors, foodstuffs, thermal insulations, polymeric liquids and geothermal systems etc. Analytical and numerical investigation of horizontal line heating sources in a power-law fluid saturated porous medium has been discussed by Nakayama (1993). Kairi et al. (2009) carried out interesting applications of non-Darcy natural convective heat and mass transfer in a power-law fluid under the influence of thermal and solutal dispersions. Soret and Dufour effects on natural convection of a power-law fluid over a vertical plate embedded in a porous medium were reported by Srinivasacharya et al. (2012).

All the above authors assumed that the thermophysical properties of the fluid are constant. However, it is well known that these variable

properties may change with temperature, especially for fluid viscosity and thermal conductivity. These variable properties are very important in several engineering and industrial applications such as volumetric solar receivers, foam insulations, boilers, heat transfer in furnaces, fibrous and porous burners etc. Hassanien et al. (2003) expressed mixed convection along a wedge embedded in a fluid saturated porous medium for the cases of uniform heat flux and uniform mass flux by using the effect of variable viscosity and thermal conductivity. The influence of radiation and variable properties of heat transfer from a moving surface in a micropolar fluid through a porous medium was discussed Elsayed et al. (2004). Seddeek and Salama (2007) examined unsteady hydromagnetic heat transfer past a semi-infinite vertical porous moving plate with variable suction taking variable viscosity and thermal conductivity effects into account. Jayanthi and Kumari (2007) investigated numerically both free and mixed convection flow on a vertical surface in a non-Newtonian fluid saturated porous medium in the presence of temperature-dependent viscosity. Mahanti and Gaur (2009) obtained similarity solutions for natural convection flow of an incompressible viscous fluid with influence of a heat sink along an isothermal vertical surface using variable properties. Srinivasacharya et al. (2015) obtained a similarity solution to explore the effects of Soret and Dufour on mixed convective flow along a vertical wavy surface in a porous medium with variable properties. Rao et al. (2017) investigated numerically the influence of thermal radiation on MHD flow over a linearly stretching sheet in a porous medium with

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variable viscosity and thermal conductivity.

Thermal radiation on mixed convective boundary layer flow has received great attention because of very important application such as solar power technology, space technology, astrophysical flows and electrical power generation, etc. Grosan and Pop (2006) discussed numerically the influence of radiation free convective flow over a vertical surface in a power-law fluid. Hayat *et al.* (2011) focused on two dimensional mixed convection stagnation-point flow of power-law fluids towards a stretching sheet with the effect of MHD and radiation. Gbadeyan *et al.* (2011) considered the problem of magnetic field, Soret and Dufour effects on mixed convection flow over a stretching vertical surface in a viscoelastic fluid saturated porous medium. Mahmoud and Megahed (2013) expressed the influence of radiation, Dufour and Soret on mixed convective flow in a study related to laminar flow along a vertical surface. Srinivasacharya *et al.* (2014) reported mixed convection flow in a doubly stratified fluid saturated porous medium in the presence of Dufour and Soret effects.

In this paper, we introduce the Lie group analysis, namely scaling group transformations for mixed convection boundary layer problems. The main advantages of these Lie group transformations is to obtain similarity transformations for the system of nonlinear partial differential equations. Moreover, the Lie Group technique has been applied by many researchers (see Oberlack (1999), (Kandasamy *et al.*, 2010), (Afify *et al.*, 2014), (Ferdows *et al.*, 2013) and (Uddin *et al.*, 2015)). Recently, El-Aziz and Afify (2016) reported Lie group analysis for a power-law fluid over a stretching sheet with effect of magnetohydrodynamic and variable properties. To the best of the authors' knowledge, the study related to Lie group analysis for a power-law fluid with variable properties has not been explained in the literature. The main aim of this work is to express the influence of Soret, variable properties and radiation on mixed convection flow over a vertical surface embedded in a porous medium saturated with a power-law fluid by using Lie scaling group transformations.

2. MATHEMATICAL FORMULATION

Consider steady, incompressible, laminar, mixed convection heat and mass transfer boundary layer flow over a vertical surface embedded in a powerlaw fluid saturated porous medium. Choose the two dimensional coordinate system such that the \overline{X} -axis is along the vertical plate and \overline{Y} -axis normal to the plate. The physical model and coordinate system are shown in Fig (1). The plate is maintained at a constant temperature \overline{T}_w and concentration \overline{C}_w . The ambient temperature is \overline{T}_∞ and the concentration is \overline{C}_∞ . Applying the boundary layer assumption and Boussinesq approximations, the governing equations are the mass, momentum, energy and concentration equations which may be written as:

$$\frac{\partial \overline{U}}{\partial \overline{X}} + \frac{\partial \overline{V}}{\partial \overline{Y}} = 0 \tag{1}$$

$$n\overline{U}^{n-1}\frac{\partial\overline{U}}{\partial\overline{Y}} = \frac{\partial}{\partial\overline{Y}} \left[\frac{Kg\rho_{\infty}}{\mu} (\beta_T^*[\overline{T} - \overline{T}_{\infty}] + \beta_C^*[\overline{C} - \overline{C}_{\infty}])\right]$$
(2)

$$\overline{U}\frac{\partial\overline{T}}{\partial\overline{X}} + \overline{V}\frac{\partial\overline{T}}{\partial\overline{Y}} = \frac{\partial}{\partial\overline{Y}}\left[\alpha\frac{\partial\overline{T}}{\partial\overline{Y}} - \frac{1}{\rho C_p}q_r\right]$$
(3)

$$\overline{U}\frac{\partial\overline{C}}{\partial\overline{X}} + \overline{V}\frac{\partial\overline{C}}{\partial\overline{Y}} = D_m \frac{\partial^2\overline{C}}{\partial\overline{Y}^2} + \frac{D_m K_T}{T_m}\frac{\partial^2\overline{T}}{\partial\overline{y}^2}$$
(4)

where \overline{X} and \overline{Y} are the Cartesian coordinates, \overline{U} and \overline{V} are the velocity components in the stream wise \overline{X} and cross-stream \overline{Y} directions, respectively, β_T^* represents the thermal expansion coefficient and β_C^* represents the concentration coefficient, \overline{T} indicates the temperature, \overline{C} indicates the concentration, K represents the permeability, K_T indicates the thermal diffusion ratio, α represents the thermal conductivity, D_m is the mass diffusivity of the saturated porous medium, T_m is the mean fluid temperature, Cp represents the specific heat capacity, q_r is the component of radiative heat flux, n is the index in the power-law variation of viscosity. n < 1 for a pseudo-plastic fluid, n > 1 for a dilatant fluid and n = 1 for a Newtonian fluid.

The boundary conditions are

$$\overline{V} = 0, \ \overline{T} = \overline{T}_w, \ \overline{C} = \overline{C}_w \quad \text{at} \quad \overline{Y} = 0$$
 (5a)

$$\overline{U} = U_{\infty}, \ \overline{T} = \overline{T}_{\infty}, \ \overline{C} = \overline{C}_{\infty}$$
 as $\overline{Y} \to \infty$ (5b)

The viscosity μ of the fluid is considered to be an inverse function of temperature and it can be expressed as (Lai and Kulacki (1990))

$$\frac{1}{\mu} = \frac{1}{\mu_{\infty}} [1 + \gamma^* (\overline{T} - \overline{T}_{\infty})] \quad i.e \quad \frac{1}{\mu} = b(\overline{T} - \overline{T}_e) \tag{6}$$

where $b = \frac{\gamma^*}{\mu_{\infty}}$, $\overline{T}_e - \overline{T}_{\infty} = -\frac{1}{\delta}$, μ_{∞} is the coefficient of viscosity and both b, \overline{T}_e are constants and their values depend on the reference state and the small parameter γ^* , reflecting a thermal property of the fluid.

Variable thermal conductivity α which appears in Eq.(3) in the nondimensional form Slattery (1972) can be written as

$$\alpha = \alpha_0 (1 + \overline{T}\beta). \tag{7}$$

where β is the thermal conductivity.

The quantity q_r is the radiative heat flux which is simplified by using the Rosseland diffusion approximation for an optically thick fluid. Thus

$$q_r = \frac{-4\sigma^*}{3k^*} \frac{\partial \overline{T}^4}{\partial \overline{y}},\tag{8}$$

where σ^* is the Stefan-Boltzmann constant and k^* is the Rosseland mean absorption coefficient.

Now, we introduce the following dimensionless variables:

$$X = \frac{\overline{X}}{L}, \quad Y = \frac{\overline{Y}}{L} P e^{\frac{1}{2}}, \quad U = \frac{\overline{U}L}{\alpha_0 P e}, \quad V = \frac{\overline{V}L}{\alpha_0 P e^{\frac{1}{2}}}$$
$$T(\eta) = \frac{\overline{T} - \overline{T}_{\infty}}{\overline{T}_w - \overline{T}_{\infty}}, \quad C(\eta) = \frac{\overline{C} - \overline{C}_{\infty}}{\overline{C}_w - \overline{C}_{\infty}}$$
$$(9)$$

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In the view of the continuity Eq. (1) we introduce a stream function $\psi(X,Y)$ as

$$U = \frac{\partial \psi}{\partial Y}, \qquad V = -\frac{\partial \psi}{\partial X} \tag{10}$$

Substituting Eqs. (6) - (10) into Eqs. (2) - (4), leads to the following momentum, energy and concentration equations

$$\Delta_{1} = n \left(\frac{\partial \psi}{\partial Y}\right)^{n-1} \frac{\partial^{2} \psi}{\partial Y^{2}} - \lambda^{n} \left(\frac{\partial T}{\partial Y} + B \frac{\partial C}{\partial Y}\right) \left(1 - \frac{T}{\theta_{e}}\right) \qquad (11)$$
$$+ \frac{\lambda^{n}}{\theta_{e}} \left(T + BC\right) \left(\frac{\partial T}{\partial Y}\right) = 0,$$

$$\Delta_2 = \frac{\partial \psi}{\partial Y} \frac{\partial T}{\partial X} - \frac{\partial \psi}{\partial X} \frac{\partial T}{\partial Y} - \beta \left(\frac{\partial T}{\partial Y}\right)^2 - \left(1 + T\beta + \frac{4R}{3}\right) \frac{\partial^2 T}{\partial Y^2} = 0,$$
(12)

$$\Delta_3 = \frac{\partial \psi}{\partial Y} \frac{\partial C}{\partial X} - \frac{\partial \psi}{\partial X} \frac{\partial C}{\partial Y} - \frac{1}{Le} \frac{\partial^2 C}{\partial Y^2} - Sr \frac{\partial^2 C}{\partial Y^2} = 0.$$
(13)

The prescribed boundary conditions Eq.5(a,b) become

$$\frac{\partial \psi}{\partial X} = 0, \quad T = 1, \quad C = 1 \quad \text{at} \quad Y = 0$$

$$\frac{\partial \psi}{\partial Y} = 1, \quad T = 0, \quad C = 0 \quad \text{at} \quad Y \to \infty,$$
(14)

where the prime indicates differentiation with respect to η , $Pe = \frac{U_{\infty}L}{\alpha_0}$ represents the Peclet number, $R = \frac{4\sigma^*\overline{T}_{\infty}^3}{k^*k}$ represents thermal radiation, $B = \frac{\beta_c(\overline{C}_w - \overline{C}_{\infty})}{\beta_T(\overline{T}_w - \overline{T}_{\infty})}$ represents the Buoyancy ratio, $Sr = \frac{D_m K_T}{T_m \alpha_0} \left(\frac{\overline{T}_w - \overline{T}_{\infty}}{\overline{C}_w - \overline{C}_{\infty}}\right)$ represents the thermal diffusion, $Le = \frac{\alpha_0}{D_m}$ indicates the Lewis number, $Ra = \frac{L}{\alpha_0} \left[\frac{Kg\beta_T(\overline{T}_w - \overline{T}_{\infty})}{\nu_{\infty}}\right]^{1/n}$ represents the generalized Rayleigh number, $\theta_e = \frac{\overline{T}_e - \overline{T}_{\infty}}{\overline{T}_w - \overline{T}_{\infty}}$ indicates the variable viscosity and $\lambda = \left(\frac{Ra}{Pe}\right)$ indicates the mixed convection parameter.

3. APPLICATION OF LIE GROUP TRANSFORMATIONS

We introduce the one-parameter scaling group of transformations which is a simplified form of Lie group transformation

$$\Gamma: X^* = Xe^{\epsilon a_1}, Y^* = Ye^{\epsilon a_2}, \psi^* = \psi e^{\epsilon a_3}, T^* = Te^{\epsilon a_4}, C^* = Ce^{\epsilon a_5}$$
(15)
Here $\epsilon \neq 0$ is the perpendence of the group and the $\epsilon' e(I = 1, 2, -5)$

Here $\varepsilon \neq 0$ is the parameter of the group and the $a'_i s(I = 1, 2..., 5)$ are arbitrary real numbers not all simultaneously zero. Equations (11)-(13) along with the boundary conditions (14) do not alter under the group of transformations in Eq.(15) if the a_i 's satisfy the following relationship

$$na_{2} - na_{3} + a_{2} = a_{2} - 2a_{4} = a_{2} - a_{4} - a_{5} = a_{2} - a_{4} = a_{2} - a_{5};$$

$$a_{1} + a_{2} - a_{3} - a_{4} = 2a_{2} - 2a_{4} = 2a_{2} - a_{4};$$

$$a_{1} + a_{2} - a_{3} - a_{5} = 2a_{2} - a_{5} = 2a_{2} - a_{4};$$

$$a_{2} - a_{3} = 0; \quad a_{4} = 0; \quad a_{5} = 0$$
(16)

Solving the linear system Eq. (16), we have the following relationship among the exponents:

$$a_1 = 2a_3; \ a_2 = a_3; \ a_4 = 0; \ a_5 = 0.$$
 (17)

The transformation Γ reduces to

$$X^* = Xe^{2\epsilon a_3}; \quad Y^* = Ye^{\epsilon a_3}; \quad \psi^* = \psi e^{\epsilon a_3}; \quad T^* = T; \quad C^* = C.$$
(18)

Expanding Eq.(18) by Taylor series in powers of ε , and keeping terms up to the first degree (neglecting higher power of ε), we obtain

$${}^{*}-X = 2\epsilon a_{3}X; \ Y^{*}-Y = \epsilon a_{3}Y; \ \psi^{*}-\psi = \epsilon a_{3}\psi; \ T^{*} = T; \ C^{*} = C.$$
(19)

The characteristic equations are

X

$$\frac{dX}{2Xa_3} = \frac{dY}{Ya_3} = \frac{d\psi}{\psi a_3} = \frac{dT}{0} = \frac{dC}{0}.$$
 (20)

Solving the above characteristic equation, we have the following similarity transformations,

$$\psi = X^{\frac{1}{2}}S(\eta), \quad \eta = YX^{-\frac{1}{2}}, \quad T = T(\eta), \quad C = C(\eta).$$
 (21)

Substituting Eq. (21) into Eqs. (11) - (13), we obtain the following ordinary differential equations.

$$n(S')^{n-1}S'' = \lambda^n \left(T' + BC'\right) \left(\frac{\theta_e - T}{\theta_e}\right) - \lambda^n \left(T + BC\right) \frac{T'}{\theta_e}, \quad (22)$$

$$\beta(T')^2 + \left(1 + T\beta + \frac{4}{3}R\right)T'' + \frac{1}{2}ST' = 0,$$
(23)

$$\frac{1}{Le}C'' + SrT'' + \frac{1}{2}SC' = 0,$$
(24)

The transformed boundary conditions Eq. (14) become

$$S(0) = 0, \quad T(0) = 1, \quad C(0) = 1$$
 (25a)

$$S'(\infty) = 1, \quad T(\infty) = 0, \quad C(\infty) = 0.$$
 (25b)

4. HEAT AND MASS TRANSFER COEFFICIENTS

The non-dimensional heat and mass transfer coefficients in terms of Nusselt number Nu and the Sherwood number Sh are respectively given by:

$$q_w = -k \left(\frac{\partial \overline{T}}{\partial \overline{Y}}\right)_{\overline{Y}=0} - \frac{4\sigma^*}{3k^*} \left(\frac{\partial \overline{T}^4}{\partial \overline{Y}}\right)_{\overline{Y}=0} \quad \text{and} \quad q_m = -D \left(\frac{\partial \overline{C}}{\partial \overline{Y}}\right)_{\overline{Y}=0} \tag{26}$$

The Nusselt number $Nu = \frac{q_w \overline{X}}{k(\overline{T}_w - \overline{T}_\infty)}$ and Sherwood number

$$Sh = \frac{q_m X}{D(\overline{C}_w - \overline{C}_\infty)} \text{ are given by}$$
$$\frac{Nu}{X^{1/2}} = -\left(1 + \frac{4R}{3}\right)T'(0) \quad \text{and} \quad \frac{Sh}{X^{1/2}} = -C'(0).$$
(27)

5. RESULTS AND DISCUSSIONS

To solve the system of nonlinear Eqns. (22) - (24) along with the corresponding boundary conditions (25), we apply the Runge-Kutta fourthorder method with a shooting technique, which has been implemented by the many researchers ((Srinivasacharya *et al.* (2011) and Srinivasacharya *et al.* (2012))) to solve boundary value problems. In order to validate our code, we compare our obtained results with those of Chaoyang *et al.* (1990) as a special case by taking $Sr = R = B = \beta = 0$, Le = 1.0, and $\theta_e \to \infty$. Excellent agreement as presented in Tables.1 and Table.2 is obtained.

The results for the non-dimensional velocity, temperature and concentration have been computed and presented graphically in Figs.2-6 to analyze the influence of variable viscosity (θ_e), thermal conductivity (β), radiation (R) Soret parameter (Sr) and mixed convection parameter (λ).

Figure 2 displays the dimensionless velocity $S'(\eta)$, temperature $T(\eta)$ and concentration $C(\eta)$ distribution in the boundary layer for different

Table 1 Comparison of Nusselt number for $R = Sr = B = \beta = 0$, $Le = 1.0, \theta_e \to \infty$

	n = 0.5	
λ	(Chaoyang et al., 1990)	Present results
0.0	0.5641	0.564190
0.5	0.8209	0.821704
1.0	0.9303	0.929635
4.0	1.3010	1.300685

Table 2 Comparison of Nusselt number for $R = Sr = B = \beta = 0$, $Le = 1.0, \theta_e \to \infty$

	n = 1.5	
λ	(Chaoyang et al., 1990)	Present results
0.0	0.5641	0.564190
0.5	0.6034	0.60339
1.0	0.6634	0.663375
4.0	1.0180	1.017582

values of the variable viscosity (θ_e) and power-law index *n* namely, shear thinning, Newtonian and shear thickening fluids. Figure 2(a) illustrates that velocity $S'(\eta)$ enhances near the plate up to a certain value and then reduces far away from the plate with increasing value of variable viscosity for the three types of fluids. The reason for above behavior is that, for a given fluid, when γ is fixed, smaller (θ_e) implies higher temperature difference between the wall and the ambient fluid. From Figs. 2(b) -2(c) we observe that when the variable viscosity is increased there is a reduction in the value of temperature and concentration for the three types of fluids. The reason for this is enhancement in the obstruction of fluid motion to enhance in temperature-dependent viscosity (θ_e).

The variation of thermal conductivity (β) and power-law index (n), namely (n < 1, n = 1, n > 1) for fixed values of the other parameters on dimensionless velocity $S'(\eta)$, temperature $T(\eta)$ and concentration $C(\eta)$ profiles in the boundary layer is displayed in Fig. 3. It is observed from Fig. 3(a) that increase in the value of thermal conductivity reduces velocity near the plate and enhances it far away from the plate for the three types of fluids. Figure 3(b) shows that the temperature $\theta(\eta)$ is more pronounced with increasing values of thermal conductivity results in an increase in the thermal boundary layer thickness. From Fig. 3(c), it is clear that enhancement in the value of thermal conductivity slightly decreases the concentration profile for the three types of fluids. The reason is that molecular motion of the fluid reduces at a slower rate for larger values of (β) .

The effect of radiation parameter (R) and the power-law index (n) namely, pseudo-plastic fluid, Newtonian, dilatant fluids in the boundary layer is illustrated in Fig.4. Figure 4(a) indicates that an enhancement in the radiation parameter, reduces the velocity $S'(\eta)$ slightly near the plate and enhances it far away from the plate for the three types of fluids. In Fig. 4(b) temperature $T(\eta)$ increases monotonically with enhancing values of the radiation parameter(R) for the three types of fluids. This is due to fact that the slope of the temperature distribution near the surface in the presence of (R) is always negative and thus heat is always transferred from the surface. Moreover, Fig. 4(c) shows that for the three different types of fluid concentration $C(\eta)$ reduces slightly with increasing radiation parameter (R).

Figure 5 represents the boundary layer for different values of the Soret parameter (Sr) and power-law fluid index (n), and fixed values of the other parameters. Figure 5(a) shows that the velocity $f'(\eta)$ enhances with an enhancement in the Soret parameter (Sr) for the three variations

of fluids. Moreover, enhancement in the value of the Soret parameter (Sr) results a slightly raised temperature $T(\eta)$ of the fluid as shown in Fig. 5(b). The influence of Soret parameter (Sr) on the concentration profile $C(\eta)$ is depicted in fig. 5(c). The profile enhancement with enhance in the value of (Sr) for the three variations of fluids. Figure 6 shows the variation of mixed convection parameter (λ) and power-law



Fig. 2 Variation of (a) Velocity (b) Temperature and (c) Concentration profiles with variable viscosity (θ_e) .

index n, respectively. From Fig. 6(a) enhancing the value of mixed convection parameter (λ) continuously raises the velocity $S'(\eta)$ for the three variations of fluids. Figure 6(b) represents that the temperature $T(\eta)$ increases with decrease in the values of the mixed convection parameter (λ) for three variations of fluids. Figure 6(c) depicts that the concentra-

tion $C(\eta)$ decreases with an increase in the mixed convection parameter (λ) for the three variations of fluids.

Table.3 shows the influence of heat and mass transfer for various values of the power law index (n), variable viscosity (θ_e) , thermal conductivity (β) , thermal radiation (R), Soret parameter (Sr) and mixed convection parameter (λ) for fixed values of the other parameters. En-



Fig. 3 Variation of (a) Velocity (b) Temperature and (c) Concentration profiles with thermal conductivity (β) .



Fig. 4 Variation of (a) Velocity (b) Temperature and (c) Concentration profiles with radiation parameter (R).

hancing the value of the n reduces the heat and mass transfer rates. An increase in the values of variable viscosity, radiation and mixed convection parameters raises both the heat and mass transfer rates. It is noticed that an increase in the value of the thermal conductivity decreases the heat transfer, but a reverse trend is observed in the mass transfer rate. Higher

value of the Soret parameter enhance the heat transfer rate and decrease the mass transfer rate.



Fig. 5 Variation of (a) Velocity (b) Temperature and (c) Concentration profiles with Soret parameter (Sr).



Fig. 6 Variation of (a) Velocity (b) Temperature and (c) Concentration profiles with mixed convection $parameter(\lambda)$.

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Table 3 Values of heat and mass transfer rates at Le=1.0 and B=1.0 for varying values of power-law index, temperature dependent viscosity, variable thermal conductivity, radiation, Soret and mixed convection parameters.

n	$ heta_e$	β	R	Sr	λ	$-T'(0)\left(1+\frac{4R}{3}\right)$	-C'(0)
0.5	2.0	0.5	0.5	0.5	1.0	1.083878	0.898871
1.0	2.0	0.5	0.5	0.5	1.0	0.811355	0.665762
1.5	2.0	0.5	0.5	0.5	1.0	0.737721	0.603112
0.5	1.5	0.5	0.5	0.5	1.0	0.985773	0.810344
0.5	2.5	0.5	0.5	0.5	1.0	1.143469	0.952729
0.5	3.0	0.5	0.5	0.5	1.0	1.183445	0.988888
0.5	2.0	0.0	0.5	0.5	1.0	1.305338	0.849427
0.5	2.0	1.0	0.5	0.5	1.0	0.939365	0.928902
0.5	2.0	1.5	0.5	0.5	1.0	0.836542	0.948922
0.5	2.0	0.5	0.0	0.5	1.0	0.790250	0.854522
0.5	2.0	0.5	1.0	0.5	1.0	1.311348	0.925503
0.5	2.0	0.5	1.5	0.5	1.0	1.501126	0.943220
0.5	2.0	0.5	0.5	0.0	1.0	1.060429	1.028426
0.5	2.0	0.5	0.5	1.0	1.0	1.107032	0.768095
0.5	2.0	0.5	0.5	1.5	1.0	1.129908	0.636080
0.5	2.0	0.5	0.5	0.5	0.5	0.945030	0.780440
0.5	2.0	0.5	0.5	0.5	1.5	1.190563	0.989876
0.5	2.0	0.5	0.5	0.5	2.0	1.280580	1.066663

6. CONCLUSION

In the present paper, we have analyzed mixed convective flow, heat and mass transfer over a vertical surface in a porous medium saturated with power-law fluid. The numerical results were obtained for different values of the power law index (n), variable viscosity (θ_e) , variable thermal conductivity (β) , thermal radiation (R) and Soret parameter (Sr). The main conclusions are as follows.

- The variable viscosity parameter (θ_e) affects the flow field, i.e. enhancement in values of the variable viscosity parameter increases the velocity, heat and mass transfer rates, but decreases the temperature and concentration profiles.
- The effect of variable thermal conductivity (β) decreases the velocity, concentration and heat transfer rates, but enhances the temperature and mass transfer rates.
- The effect of the radiation parameter (*R*) reduces the velocity and concentration profiles, but enhances the temperature, heat and mass transfer rates.
- An increasing value of the Soret parameter (*Sr*) decreases the temperature and mass transfer rates, but monotonically increases the velocity, concentration and heat transfer rates.
- The influence of the mixed convection parameter (λ) results in an enhancement in velocity and heat transfer rates, but reduces the temperature, concentration and mass transfer rates.

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