

Frontiers in Heat and Mass Transfer



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EFFECTS OF VARIABLE VISCOSITY AND VARIABLE THERMAL CONDUCTIVITY ON HYDROMAGNETIC DUSTY FLUID FLOW DUE TO A ROTATING DISK

Jadav Konch* and G. C. Hazarika

Department of Mathematics, Dibrugarh University, Dibrugarh-786004, Assam, India

ABSTRACT

This paper investigates momentum, heat and mass transfer characteristics of a hydromagnetic Newtonian dusty fluid flow due to a rotating disk with radiation and viscous dissipation. The main objective of this paper is to study effects of temperature dependent viscosity and thermal conductivity on flow, temperature and species concentration. Radiation and viscous dissipation effects are also taken into account. Saffman model for dusty fluid is considered for the problem. The partial differential equations governing the flow are converted into ordinary differential equations employing similarity transformations. The resulting highly nonlinear coupled ordinary differential equations are solved numerically using shooting technique with fourth order Runge-Kutta integration scheme. The influence of variable fluid viscosity, variable thermal conductivity, fluid particle interaction, magnetic interaction and radiation parameters as well as Eckert number are presented graphically and discussed for velocity, temperature and species concentration profiles. Numerical values of the wall shear stress, rate of heat transfer (in terms of Nusselt number) and rate of mass transfer (in terms of Sherwood number) are obtained, analyzed and presented in tabular form.

Keywords: Dusty fluid, variable viscosity, variable thermal conductivity, radiation, rotating disk, shooting method.

1. INTRODUCTION

The study of a two-phase gas-particle flow has a wide range of applications in power plant piping, combustion, petroleum transport, waste water treatment, corrosive particles in engine oil flow and formation of raindrops. Its relevance is also seen in the field of smoke emission from vehicles, agriculture and food technologies. Motivated by the applications of a two-phase flow, Saffman (1962) has initiated and formulated the governing equations for the flow of dusty fluid and discussed the stability of a laminar flow of a dusty gas. In this model, he considered that the dust particles were uniformly distributed. Michael and Miller (1966) discussed the motion of dusty gas occupying the semi infinite space above a rigid plane boundary. Nayfeh (1966) studied oscillating dusty flow through a rigid pipe. Gupta and Gupta (1976) discussed the flow of a gas containing solid particles in a channel with arbitrary time varying pressure. The flow of a dusty fluid in the boundary layer over a semi-infinite flat plate was analyzed by Datta and Mishra (1982). Ramamurthy (1990) investigated the effects of free convection on the Stokes problem for the flow of dusty fluid in an infinite vertical plate. Attia (2006) analyzed unsteady MHD Couette flow and heat transfer of dusty fluid with variable physical properties. Palani and Kim (2010) obtained the approximate solution for the flow of a dusty-gas along a semi-infinite vertical cylinder. Gireesha et al. (2011; 2012; 2013) discussed interesting results on the flow of dusty fluid due to linear and exponential stretching of porous and nonporous sheet with various effects like radiation, source/sink parameter, viscous dissipation etc. Manjunatha (2015) studied the effect of radiation on MHD flow and heat transfer of dusty fluid over a stretching cylinder in a porous medium.

The study of dusty viscous fluid flow under the influence of various physical conditions has been carried out by several researchers or authors. This interest stems from the fact that the flow and heat transfer of magnetohydrodynamic boundary layer flow finds its applications in wide range of science and technology like MHD power generation, purification of crude oil, cooling of nuclear reactors, centrifugal separation of matter from fluid and in several astrophysical situations. The theory of rotating fluid is highly important due to its occurrence in various natural phenomena and for its applications in various technological situations. The broad subjects of oceanography, meteorology, atmospheric sciences, and limnology all contain some important and essential features of rotating fluid.

Further, the fluid flow problems of rotating fluid have attracted many scholars and there appeared a number of studies in literature viz. Tiwari and Kamal Singh (1983) analyzed viscous incompressible hydromagnetic boundary layer flow of dusty fluid over a semi-infinite plate. Prasada Rao and Krishna (1981) investigated the Hall Effect on unsteady hydromagnetic flow. The effects of Hall current on unsteady MHD flow past a rotating disk was studied by Kanch and Jana (1999). Debnath *et al.* (1979) studied the Hall effects on the unsteady hydromagnetic flow of a rotating fluid system over a porous plate.

Turkyilmazoglu (2009; 2010) studied the steady laminar flow of viscous, incompressible, electrically-conducting fluid over a rotating disk in the presence of a transverse magnetic field. The problem of heat transfer from a rotating disk maintained at a constant temperature for various values of Prandtl number in steady state was considered by Millsaps and Pohlhausen (1952). Heat transfer characteristic of MHD steady flow of a viscous incompressible electrically conducting fluid past a rotating disk with Hall current, viscous dissipation and Ohmic heating were studied by Sibanda and Makinde (2010). They found that magnetic field opposed fluid motion due to the Lorentz force generated by the magnetic field.

It is interesting that in the above flow problems generated by a rotating disk, fluids are considered in pure form. But, it is well known

^{*} Corresponding Author Email: jadavkonch@gmail.com

that air and water, by nature, contain impurities like dust particles and foreign bodies. In fact, the problem of two-phase flows in which solid particles are distributed in clean fluid has several practical applications such as the environmental pollution, sedimentation, centrifugal separation of particles, blood rheology, purification of crude oil and physiological flows.

Moreover, from the above studies, it is also seen that most of the investigators restricted their investigations by assuming viscosity and thermal conductivity of the fluid as constant. However, it was known from the work of Herwig and Wicken (1986) that these properties may change with temperature. A theoretical investigation of the effects of temperature dependent viscosity on forced convection over a flat plate in porous medium has been presented by Ling and Dybbs (1987). So, a more accurate prediction for the flow, heat transfer and mass transfer can be achieved by taking into account the variation of such properties with temperature. Hazarika and Konch (2016) and Konch and Hazarika (2016) have studied the influence of varying viscosity and thermal conductivity on convective heat and mass transfer in the flow of dusty fluid with radiation and viscous dissipation.

Motivated by the above-mentioned investigations and applications, the aim of this work is to investigate effects of temperature dependent fluid viscosity and thermal conductivity on the hydromagnetic boundary layer flow of a dusty fluid due to a rotating disk with radiation and viscous dissipation. Shooting technique with fourth order Runge-Kutta integration scheme is employed to obtain the solution of the boundary value problem.

2. MATHEMATICAL FORMULATION

Consider the problem of steady, hydromagnetic axially symmetric flow of an electrically conducting incompressible dusty fluid with viscous dissipation and radiation. The flow is generated due to a rotating disk. It is assumed that fluid is extent infinitely in the positive z-direction. Let (r, ϕ, z) be the set of cylindrical polar coordinates and let the disk be

rotates with constant angular velocity $\hat{\Omega}(0, 0, \Omega_0)$ and be placed at z = 0 as indicated in Fig. 1.



Fig. 1 Schematic diagram of the problem

The fluid and dust phase velocity components are (u, v, w) and (u_p, v_p, w_p) respectively in the directions of (r, φ, z) . The surface of the rotating disk is maintained at uniform temperature T_w . The free stream (far away from the wall) is kept at constant temperature T_{∞} and at constant pressure P_{∞} . An external uniform magnetic field of strength $\vec{B}(0, 0, B_0)$ is applied perpendicular to the surface of the disk.

The analysis is based on the following assumptions:

- Fluid properties are assumed as constant except the fluid viscosity and thermal conductivity.
- Dust particles are assumed as electrically non-conducting, spherical in shape having same radius and mass, and undeformable.
- The number density of dust particles is taken as constant throughout the flow.
- Magnetic Reynolds number is assumed to be so small therefore the induced magnetic field is negligible (Sutton (1965)).

Under these assumptions together with Devi and Devi (2011), Khidir (2013), Boussinesq approximations and following Saffman (1962) model of dusty gas the governing equations are:

For the fluid phase:

$$\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0$$

$$p\left(u\frac{\partial u}{\partial r} - \frac{v^2}{r} + w\frac{\partial u}{\partial z}\right) = -\frac{\partial p}{\partial r} + \frac{\partial}{\partial r}\left(\mu\frac{\partial u}{\partial r}\right) + \frac{\partial}{\partial r}\left(\mu\frac{u}{r}\right)$$

$$+ \frac{\partial}{\partial z}\left(\mu\frac{\partial u}{\partial z}\right) - \sigma B_0^2 u + KN(u_p - u)$$

$$\left(\frac{\partial v}{\partial r} + \frac{\partial v}{\partial r}\right) = \partial \left(\frac{\partial v}{\partial r}\right) = \partial \left(\frac{\partial v}{\partial r}\right) = \partial \left(\frac{\partial v}{\partial r}\right)$$

$$(1)$$

$$\rho\left(u\frac{\partial v}{\partial r} + \frac{uv}{r} + w\frac{\partial v}{\partial z}\right) = \frac{\partial}{\partial r}\left(\mu\frac{\partial v}{\partial r}\right) + \frac{\partial}{\partial r}\left(\mu\frac{v}{r}\right) + \frac{\partial}{\partial z}\left(\mu\frac{\partial v}{\partial z}\right) -\sigma B_0^2 v + KN(v_p - v)$$
(3)

$$\rho\left(u\frac{\partial w}{\partial r} + w\frac{\partial w}{\partial z}\right) = -\frac{\partial p}{\partial z} + \frac{\partial}{\partial r}\left(\mu\frac{\partial w}{\partial r}\right) + \frac{1}{r}\frac{\partial}{\partial r}(\mu w) + \frac{\partial}{\partial z}\left(\mu\frac{\partial w}{\partial z}\right) + KN(w_p - w)$$
(4)

$$\rho c_p \left(u \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} \right) = \frac{\partial}{\partial r} \left(\lambda \frac{\partial T}{\partial r} \right) + \frac{\lambda}{r} \frac{\partial T}{\partial r} + \frac{\partial}{\partial z} \left(\lambda \frac{\partial T}{\partial z} \right) - \frac{\partial q_r}{\partial z} + \mu \left[\left(\frac{\partial u}{\partial z} \right)^2 + \left(\frac{\partial v}{\partial z} \right)^2 \right] + \frac{N c_p}{\tau_T} (T_p - T) \quad (5)$$

$$u\frac{\partial C}{\partial r} + w\frac{\partial C}{\partial z} = \frac{1}{r}\frac{\partial}{\partial r}\left(rD_m\frac{\partial C}{\partial r}\right) + \frac{\partial}{\partial z}\left(D_m\frac{\partial C}{\partial z}\right) + \frac{mN}{\rho\tau_c}(C_p - C)$$
(6)

For the dust phase:

$$\frac{1}{r}\frac{\partial}{\partial r}(r\rho_p u_p) + \frac{\partial}{\partial z}(\rho_p w_p) = 0$$
(7)

$$m\left(u_{p}\frac{\partial u_{p}}{\partial r}-\frac{v_{p}^{2}}{r}+w_{p}\frac{\partial u_{p}}{\partial z}\right)=-K(u_{p}-u)$$
(8)

$$m\left(u_p\frac{\partial v_p}{\partial r} + \frac{u_p v_p}{r} + w_p\frac{\partial v_p}{\partial z}\right) = -K(v_p - v)$$
(9)

$$m\left(u_p \frac{\partial w_p}{\partial r} + w_p \frac{\partial w_p}{\partial z}\right) = -K(w_p - w) \tag{10}$$

Frontiers in Heat and Mass Transfer (FHMT), 8, 39 (2017) DOI: 10.5098/hmt.8.39

$$NC_m \left(u_p \frac{\partial T_p}{\partial r} + w_p \frac{\partial T_p}{\partial z} \right) = -\frac{Nc_p}{\tau_T} (T_p - T)$$
(11)

$$u_p \frac{\partial C_p}{\partial r} + w_p \frac{\partial C_p}{\partial z} = -\frac{mN}{\rho \tau_c} (C_p - C)$$
(12)

Appropriate boundary conditions for the problem are:

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At
$$z = 0$$
: $u = 0, v = \Omega_0 r, w = 0, T = T_w, C = C_w,$
As $z \to \infty$: $u = 0, v \to 0, u_p \to 0, v_p \to 0, w_p \to w,$
 $T \to T_{\infty}, T_p \to T_{\infty}, \rho_p \to \alpha\rho, C \to C_{\infty}, C_p \to C_{\infty}$

$$(13)$$

0 7

Using Rosseland approximation for radiation we can write radiative heat flux as (Necati (1973))

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial z}, \qquad (14)$$

where σ^* and k^* are the Stefan-Boltzmann constant and mean absorption coefficient, respectively.

It is assumed that temperature difference within the flow such that the term T^4 can be expressed as a linear function of temperature. This is accomplished by expanding T^4 in a Taylor series about T_{∞} and neglecting the second and higher order terms, we get

$$T^4 \cong 4T_\infty^3 T - 3T_\infty^4 \quad . \tag{15}$$

In order to obtain ordinary differential equations, we introduce the following similarity transformations:

$$\eta = \left(\frac{\Omega_0}{v_{\infty}}\right)^{1/2} z, u = \Omega_0 r f(\eta), v = \Omega_0 r g(\eta),$$
$$w = \left(\Omega_0 v_{\infty}\right)^{1/2} h(\eta), p - p_{\infty} = 2\mu_{\infty}\Omega_0 P(\eta), u_p = \Omega_0 r F(\eta),$$

$$v_p = \Omega_0 r g G(\eta), w_p = (\Omega_0 v_\infty)^{1/2} \mathcal{H}(\eta), \theta = \frac{I - I_\infty}{T_w - T_\infty},$$

$$\theta_p = \frac{T_p - T_\infty}{T_w - T_\infty}, \phi = \frac{C - C_\infty}{C_w - C_w}, \phi_p = \frac{C_p - C_\infty}{C_w - C_w}, \rho_r = \mathcal{H}(\eta)$$
(16)



Fig. 2 Radial velocity profile for different θ_r .

The viscosity of the fluid is assumed to be an inverse linear function of temperature, and it can be expressed as following Lai and Kulacki (1991):

Global Digital Central ISSN: 2151-8629

$$\frac{1}{\mu} = \frac{1}{\mu_{\infty}} \left[1 + \delta \left(T - T_{\infty} \right) \right] \quad \text{or, } \frac{1}{\mu} = \alpha \left(T - T_{r} \right), \tag{17}$$
where $\alpha = \frac{\delta}{\mu_{\infty}}$ and $T_{r} = T_{\infty} - \frac{1}{\delta}$.



Fig. 3 Tangential velocity profile for different θ_r

Moreover, the thermal conductivity of the fluid varies with temperature. Following Choudhury and Hazarika (2013), we assumed thermal conductivity of the fluid as:

$$\frac{1}{\lambda} = \frac{1}{\lambda_{\infty}} \left[1 + \xi \left(T - T_{\infty} \right) \right] \text{ or, } \frac{1}{\lambda} = \zeta \left(T - T_{c} \right),$$
(18)
where $\zeta = \frac{\xi}{\lambda_{\infty}}$ and $T_{c} = T_{\infty} - \frac{1}{\xi}.$

Here α , ξ , ζ , T_r and T_c are constants and their values depend on the reference state and thermal properties of the fluid i.e., v (kinematic viscosity) and λ (thermal conductivity).

Let us introduce two dimensionless parameters:

- $\theta_r = \frac{T_r T_{\infty}}{T_w T_{\infty}}$ the dimensionless reference temperature corresponding
- to viscosity called the viscosity variation parameter, and $T_{z} T$
- $\theta_{c} = \frac{T_{c} T_{\infty}}{T_{w} T_{\infty}}$ the dimensionless reference temperature corresponding

to thermal conductivity called the thermal conductivity variation parameter.

It is also important to note that θ_r and θ_c are negative for liquids and positive for gases (Kuppalapalle *et al.* (2013)).

Using these two parameters in equations (17) and (18) we get dynamic viscosity and thermal conductivity as:

$$\mu = -\frac{\mu_{\infty}\theta_r}{\theta - \theta_r} \text{ and } \lambda = -\frac{\lambda_{\infty}\theta_c}{\theta - \theta_c}.$$
(19)

Substituting equations (14)-(19) into equations (1)-(13), we get the following nonlinear ordinary differential equations:

$$f = -\frac{1}{2}h'$$

$$\frac{\theta_r}{\theta - \theta_r}h''' - \frac{\theta_r}{(\theta - \theta_r)^2}\theta'h'' + hh'' + \frac{1}{2}h'^2 + Mh'$$
(20)

$$+2l\beta_{\mathcal{V}}\mathcal{H}(F+\frac{1}{2}h')+2g^{2}=0$$
(21)

$$\frac{\theta_r}{\theta - \theta_r} g'' - \frac{\theta_r}{\left(\theta - \theta_r\right)^2} \theta' g' + hg' + Mg' - h'g - l\beta_V \mathcal{H}(G - g) = 0$$
(22)

$$\left(\frac{\theta_c}{\theta - \theta_c} - \frac{4}{3R_d}\right) \theta'' - \frac{\theta_c}{\left(\theta - \theta_c\right)^2} {\theta'}^2 + \Pr h\theta' + Ec \Pr \frac{\theta_r}{\theta - \theta_r} \left(\frac{1}{4}{h''}^2 + {g'}^2\right) - \Pr \beta_r a_1(\theta_p - \theta) = 0$$
(23)

$$-\Pr\,\beta_T a_1(\theta_p - \theta) = 0 \tag{2}$$

$$\frac{\theta_r}{\theta - \theta_r} \phi'' - \frac{\theta_r}{\left(\theta - \theta_r\right)^2} \theta' \phi' + Sc h \phi' - Sc l \beta_c \mathcal{H}(\phi_p - \phi) = 0$$
(24)

$$H\mathcal{H}' + H'\mathcal{H} + 2F\mathcal{H} = 0 \tag{25}$$

$$HF' + F^{2} + \beta_{v}(F + \frac{1}{2}h') - G^{2} = 0$$
⁽²⁶⁾

$$HG' + 2FG + \beta_{\mathcal{V}}(G - g) = 0$$
(27)

$$HH' + \beta_{\mathcal{V}}(H-h) = 0 \tag{28}$$

$$H\theta'_p + \gamma \beta_T (\theta_p - \theta) = 0$$
⁽²⁹⁾

$$H\phi'_p + l\beta_c \mathcal{H}(\phi_p - \phi) = 0 \tag{30}$$

Boundary conditions are reduced to:

At
$$\eta = 0$$
: $f = 0, h = 0, h' = 0, g = 1, \theta = 1, \phi = 1$
As $\eta \to \infty$: $f = 0, h = h_w, h' = 0, g = 0, F = 0, G = 0,$
 $\mathcal{H} = \omega, \theta = 0, \theta_p = 0, \phi = 0, \phi_p = 0.$

$$(31)$$

where the dimensionless parameters are defined as follows:

$$M = \frac{\sigma B_0^2}{\Omega_0 \rho}$$
 is the magnetic parameter; $\text{Re} = \frac{\Omega_0 r^2}{v_{\infty}}$ is the Reynolds

number; $R_d = \frac{\lambda_{\infty} k^*}{4\sigma^* T^3}$ is the radiation parameter; $\Pr = \frac{\mu_{\infty} c_p}{\lambda}$ is the

Prandtl number; $S_c = \frac{v}{D_m}$ is the Schmidt number. $\beta_v = \frac{1}{\tau_v \Omega_0}$,

 $\beta_T = \frac{1}{\tau_T \Omega_0}$ and $\beta_c = \frac{1}{\tau_c \Omega_0}$ are the fluid particle interaction

parameters for velocity, temperature and concentration, respectively; $\tau_v = \frac{m}{K}$ is the velocity equilibrium time; $l = \frac{mN}{\rho_n}$ is the mass

concentration; $\rho_r = \rho_p / \rho$ is the relative density; $\gamma = c_p / c_m$ is the ratio of specific heat; $a_1 = \frac{N}{\rho}$ is a constant and a prime (') denotes derivative with respect to similarity variable η .

2.1 Skin friction Coefficient, Nusselt Number and Sherwood Number

Skin friction coefficient in the radial (C_{fr}) and tangential (C_{ft}) directions, Nusselt number (Nu) and Sherwood number(Sh) are the parameters of physical and engineering interest for the present problem, which physically indicates the wall shear stress, rate of heat transfer and rate of mass transfer, respectively.

Skin friction coefficient in the radial and tangential direction are defined as

$$C_{fr} = \left[\frac{\tau_r}{\rho u^2 / 2}\right]_{z=0}, \text{ where } \tau_r = \left[\mu\left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial r}\right)\right] \text{ is the radial shear stress; and}$$

$$C_{ft} = \left[\frac{\tau_t}{\rho v^2 / 2}\right]_{z=0}$$
, where $\tau_t = \left[\mu \frac{\partial v}{\partial z} + \frac{1}{r} \frac{\partial w}{\partial \varphi}\right]$ is the tangential shear stress respectively.

ear stress, respectively.

Using the non-dimensional variables we get the skin friction coefficients as

$$C_{fr} \operatorname{Re}^{1/2} = \frac{\theta_r}{1 - \theta_r} h''(0) \text{ and } \frac{1}{2} C_{ft} \operatorname{Re}^{1/2} = -\frac{\theta_r}{1 - \theta_r} g'(0).$$

The Nusselt number is defined as

$$Nu = \frac{xq_w}{\lambda_{\infty}(T_w - T_{\infty})}, \text{ where } q_w = -\lambda \frac{\partial T}{\partial z} \Big|_{z=0} \text{ is the heat transfer}$$

from surface of the disk.

Using the non-dimensional variables we get

$$Nu / \operatorname{Re}^{1/2} = \frac{\theta_c}{1 - \theta_c} \theta'(0)$$

The Sherwood number which is defined as

$$Sh = \frac{xm_w}{Dm_{\infty}(C_w - C_{\infty})}$$
, where $m_w = -D_m \frac{\partial C}{\partial z} \bigg|_{z=0}$ is the mass flux

at the surface and Dm_{∞} is the diffusion constant at the free stream.

Using the non-dimensional variables we get

$$Sh / \operatorname{Re}^{1/2} = \frac{\theta_r}{1 - \theta_r} \phi'(0) \; .$$

3. METHOD OF SOLUTION

The equations (20)-(30) governing the flow subject to boundary conditions represented by equation (31) are solved numerically using shooting technique with the fourth order Runge-Kutta integration scheme. In this method, all higher order nonlinear ordinary differential equations are converted into a system of linear differential equations of first order and then they are transformed into initial value problem applying shooting technique (Mallikarjuna et al. (2016)). Numerical values are computed by developing suitable codes in MATLAB for the method. From the process of numerical computation, the velocity, temperature and concentration profiles for both the fluid and dust phases are plotted for various flow governing parameters. Further, the skin friction coefficients, Nusselt number and Sherwood number are sorted out and their numerical values are presented in tabular form.

RESULTS AND DISCUSSION 4.

In order to analyze the problem physically, a representative set of numerical results of velocity components, temperature and concentration profiles are shown graphically in Figs. 2-23. The coefficients of skin friction in the radial and tangential directions, Nusselt number and Sherwood number are also calculated and are presented in tabular form. The results are given for different values of the various dimensionless parameters governing the flow, viz., viscosity variation parameter(θ_r), thermal conductivity variation parameter(θ_c), fluid particle interaction parameters ($\beta_v, \beta_T, \beta_c$),

magnetic parameter(M), radiation parameter(R_d) and Eckert number(Ec). Numerical values of the parameters used for simulation are: M=1, Pr=0.71, $\beta_v = \beta_T = \beta_c = 2$, Ec=0.05, R_d=5, Sc=0.22, $\theta_r = 5$ and

 $\theta_c = 3$ unless otherwise stated.

Figures 2-6 demonstrate the influence of viscosity variation parameter (θ_r) on velocity, temperature and concentration profiles of fluid and dust phase. It is seen from Figs. 2-3 that an increase in the strength of θ_r leads to retard the radial and tangential velocity of both the phases. Physically as the values of viscosity variation parameter θ_r .

increases, the resistance to the relative motion of the different layers of a fluid increase due to the increase of viscous force and as a result velocity of the fluid decreases. But Fig. 4 shows a back flow in the axial direction. It is observed from Fig. 5 that temperature of the fluid and dust phase increases when viscosity variation parameter θ_r is increased. Physically an enhancement of θ_r leads to increase flow resistive viscous force and therefore to overcome this force and maintain the flow, the fluid has to do extra work. That energy transformed into thermal energy as a result temperature of the fluid increases. At the same time concentration of both the fluid and dust phases decrease for increasing θ_r (Fig. 6).



Fig. 4 Axial velocity profile for different θ_r



Fig. 5 Temperature profile for different θ_r

From Fig. 7, we have found that both the fluid and dust phase temperature depreciate with an increase in the strength of the thermal conductivity variation parameter θ_C . The reason behind is that thermal conductivity is an inverse linear function of temperature, hence the result.



Fig. 6 Concentration profile for different θ_r



Fig. 8 Radial velocity profile for different M

Figures 8-12 illustrate the effect of magnetic field on velocity, temperature and concentration profiles through the magnetic parameter (M). As the increasing values of magnetic parameter M, radial and tangential components of velocity decrease for both the fluid and dust phase. The presence of transverse magnetic field sets a resistive force, called Lorentz force, which opposes the velocity field. Therefore, as the values of M increase so does the retarding force and hence the velocity decreases (Figs. 8-9). But Fig. 10 shows, axial component of velocity increases with increasing M, because of the fact that it is in the same direction with the applied magnetic field. It is noticed from Figs. 11-12

that an increase in magnetic parameter enhances the temperature as well as concentration profiles for both the phases. This is because of the resistive Lorentz force, which leads to enhancing the friction between adjacent fluid layers, as a result heat is produced and hence temperature and concentration increase.



Fig. 9 Tangential velocity profile for different M



Fig. 10 Axial velocity profile for different M



Fig. 11 Temperature profile for different M

Figure 13 depicts the temperature distribution for various values of radiation parameter R_d . From this figure it is seen that temperature of both the fluid and dust phase is maximum at the surface of the disk and asymptotically decreases to zero as η increases.

Figures 14-18 elucidate the variation of velocity, temperature and concentration fields of fluid and dust phase with fluid particle

interaction parameters. It is observed that, if β_v , β_T and β_c are increased then all the components of fluid phase velocity except axial component, temperature and concentration fields get decrease. But the velocity, temperature and concentration distributions for dust phase are significantly increased. It is also noticed from these graphs that, for very large values of β_v , β_T and β_c both the phases will be same.



Fig. 14 Radial velocity profile for different β_v

The variations of velocity, temperature and concentration profiles for different values of Eckert number (Ec) are depicted in Figs. 19-23. It is found from Figs. 19-21 that, radial and tangential components of

velocity increases with increasing Ec for both the fluid and dust phase. While the axial component of velocity profile significantly decreases with increasing Ec. By analyzing the graphs in Figs. 22-23, we have observed that an enhancement of Ec leads to increase the temperature and concentration distributions of both fluid and dust phase. This is because of the fact that the heat energy is stored in the fluid due to frictional heating.



Fig. 15 Tangential velocity profile for different β_v



Fig. 16 Axial velocity profile for different β_v



Fig. 17 Temperature profile for different β_T





Fig. 21 Axial velocity profile for different Ec



Fig. 22 Temperature profile for different Ec



Fig. 23 Concentration profile for different *Ec*

Table 1 Effects of θ_r , θ_c , M, R_d and Ec on radial skin friction coefficient (C_{fr}), tangential skin friction coefficient (C_{ft}), Nusselt number(Nu) and Sherwood number(Sh)

θ_r	θ_{c}	М	R _d	Ec	C_{ft}	C_{fr}	Nu	Sh
3					-1.53146	0.730836	1.400648	1.525916
5					-1.4804	0.676131	1.393366	1.508651
7	3	1	5	0.05	-1.46009	0.655291	1.390404	1.501648
9					-1.44926	0.644093	1.388867	1.497852
	3				-1.4804	0.676131	1.393366	1.508651
	5				-1.47624	0.674312	1.322758	1.505433
5	7	1	5	0.05	-1.47463	0.673543	1.295707	1.504159
	9				-1.47378	0.673113	1.281369	1.503475
		0.5			-1.2214	0.820624	1.468169	1.555313
		0.7			-1.32831	0.753691	1.433401	1.533553
5	3	0.9	5	0.05	-1.43083	0.699571	1.405288	1.51609
		1.1			-1.52898	0.653797	1.382898	1.501801
			3		-1.48309	0.67694	1.30425	1.510455
			5		-1.4804	0.676131	1.393366	1.508651
5	3	1	7	0.05	-1.4791	0.675733	1.461799	1.507271
			9		-1.47835	0.675498	1.461799	1.507271
				0	-1.47995	0.675953	1.413352	1.508316
				2	-1.49807	0.683085	0.600304	1.522102
5	3	1	5	4	-1.51717	0.690396	-0.24263	1.536703
				6	-1.53729	0.697997	-1.11872	1.552175

The variation of skin friction coefficient, Nusselt number and Sherwood number for various flow governing parameters, viz. θ_r , θ_c , M, R_d and Ec are shown in Table 1. From the table, it is noticed that

magnitude of tangential skin-friction coefficient decreases when viscosity variation parameter (θ_r), thermal conductivity variation parameter (θ_c) and radiation parameter (R_d) increase; however, it increases as the values of Eckert number increase. Also, this table indicates radial skin-friction coefficient decreases for increasing values of θ_r , θ_c and R_d ; while it increases with Ec increases. The Nusselt number i.e., rate of heat transfer at the disk decreases with an increase in θ_r , θ_c and Ec; but we have observed a slight increase with R_d . The Sherwood number i.e., the rate of mass transfer decreases for an enhancement of the parameters θ_r , θ_c and R_d , whereas it increases with Eckert number Ec. All the physical quantities of interest skin-friction coefficient, Nusselt number and Sherwood number decrease as the value of magnetic parameter M increases.

5. CONCLUSIONS

In this paper, an analysis is performed on the effects of viscosity variation parameter, thermal conductivity variation parameter, magnetic parameter, fluid particle interaction parameters, radiation parameter and Eckert number on a conducting dusty fluid flow due to a rotating disk with the influence of magnetic field taking into account.

From the analysis following conclusions were made:

- It is clear that the effects of temperature on viscosity and thermal conductivity are very significant.
- The axial component of the velocity increases with increasing values of viscosity variation parameter and magnetic parameter.
- The effect of the viscosity variation parameter, magnetic parameter and Eckert number is seen to increase the temperature profiles of both the fluid and dust phases.
- An enhancement of radiation parameter has a tendency to decrease the temperature distribution of both the fluid and dust phases.
- An increase in the value of viscosity variation parameter leads to decrease the concentration profile of both the fluid and dust phases; while concentration increases for increasing values of the magnetic parameter and Eckert number.
- It is observed that velocity and temperature profiles of both the fluid and dust phase will be same for very large values of fluid particle interaction parameter.
- The magnitude of skin friction coefficient predicted to be decreased with increase in the value of viscosity variation, thermal conductivity variation and radiation parameters; whereas skin friction coefficient increases with Eckert number increases.
- It is noticed that rate of heat and mass transfer decreases with viscosity variation, thermal conductivity variation and magnetic parameters increase.

ACKNOWLEDGEMENTS

Authors are thankful to the University Grants Commission, New Delhi, India, for the financial support under the scheme of National Fellowship for Students of Other Backward Classes (NFOBC).

NOMENCLATURE

- B_0 axial component of magnetic field strength
- *C* concentration of the fluid
- C_p concentration of dust phase
- **c**_m specific heat of dust particles at constant pressure
- **c**_p specific heat of fluid at constant pressure

Dm	mass diffusivity
<i>f</i> , <i>F</i>	dimensionless radial component of fluid and dust phase
G	velocity, respectively
g, G	dimensionless tangential component of fluid and dust phase
h H	dimensionless axial component of fluid and dust phase
11, 11	velocity, respectively
Κ	Stokes' resistance (drag co-efficient)
l	mass concentration
m	mass of a dust particle
N	number density of the particle phase
р Р	dimensionless pressure
T T	temperature of the fluid inside the boundary layer
T_p	temperature of the dust phase inside the boundary layer
T_{∞}	temperature of the ambient fluid
Greek Sym	bols
θ, θ_p	dimensionless temperature of fluid and dust phase,
	respectively
λ	thermal conductivity
λ_{∞}	thermal conductivity of the ambient fluid
μ	dynamic viscosity
μ_{∞}	dynamic viscosity of the ambient fluid
ϕ, ϕ_p	dimensionless species concentration of fluid and dust
ρ	phase, respectively density of the fluid (kg/m ³)
$\rho_{\rm r}$	density of the dust phase (kg/m ³)
σ	electrical conductivity
τ	relaxation time of the dust narticles i.e. the time required
v	by a dust partials to adjust its valuative to the fluid
	by a dust particle to adjust its velocity to the fluid

- au_T thermal equilibrium time and is the time required by the dust cloud to adjust its temperature relative to the fluid
- solutal equilibrium time i.e., the time required by the τ_{c} dust particle to adjust its concentration relative to the fluid
- kinematic viscosity of the fluid in the free stream v_{∞}
- constant density ratio ω

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